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2.830J / 6.780J / ESD.63J Control of Manufacturing Processes (SMA 6303)  
Spring 2008

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# Control of Manufacturing Processes

**Subject 2.830/6.780/ESD.63**

**Spring 2008**

**Lecture #16**

**Process Robustness**

**April 10, 2008**

# Outline

- Last Time
  - Optimization Basics
  - Empirical Response Surface Methods
    - Steepest Ascent - Hill Climbing Approach
- Today
  - Process Robustness
    - Minimizing Sensitivity
    - Maximizing Process Capability
  - Variation Modeling
    - Noise Inputs as Random Factors
  - Taguchi Approach
    - Inner - Outer Arrays

# What to Optimize?

- Process Goals
  - Cost (Minimize)
  - Quality (Maximize Cpk or Minimize E(L))
  - Rate (Maximize)
  - Flexibility (N/A for now)

# Simple Problem: Minimum Cost

- Must Hit Target

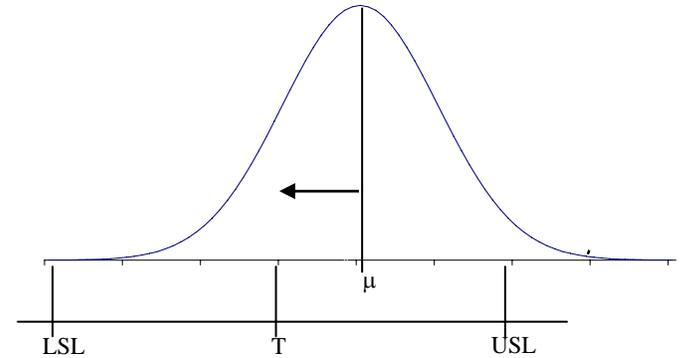
$$\bar{x} = T$$

- Multiple Input Factors

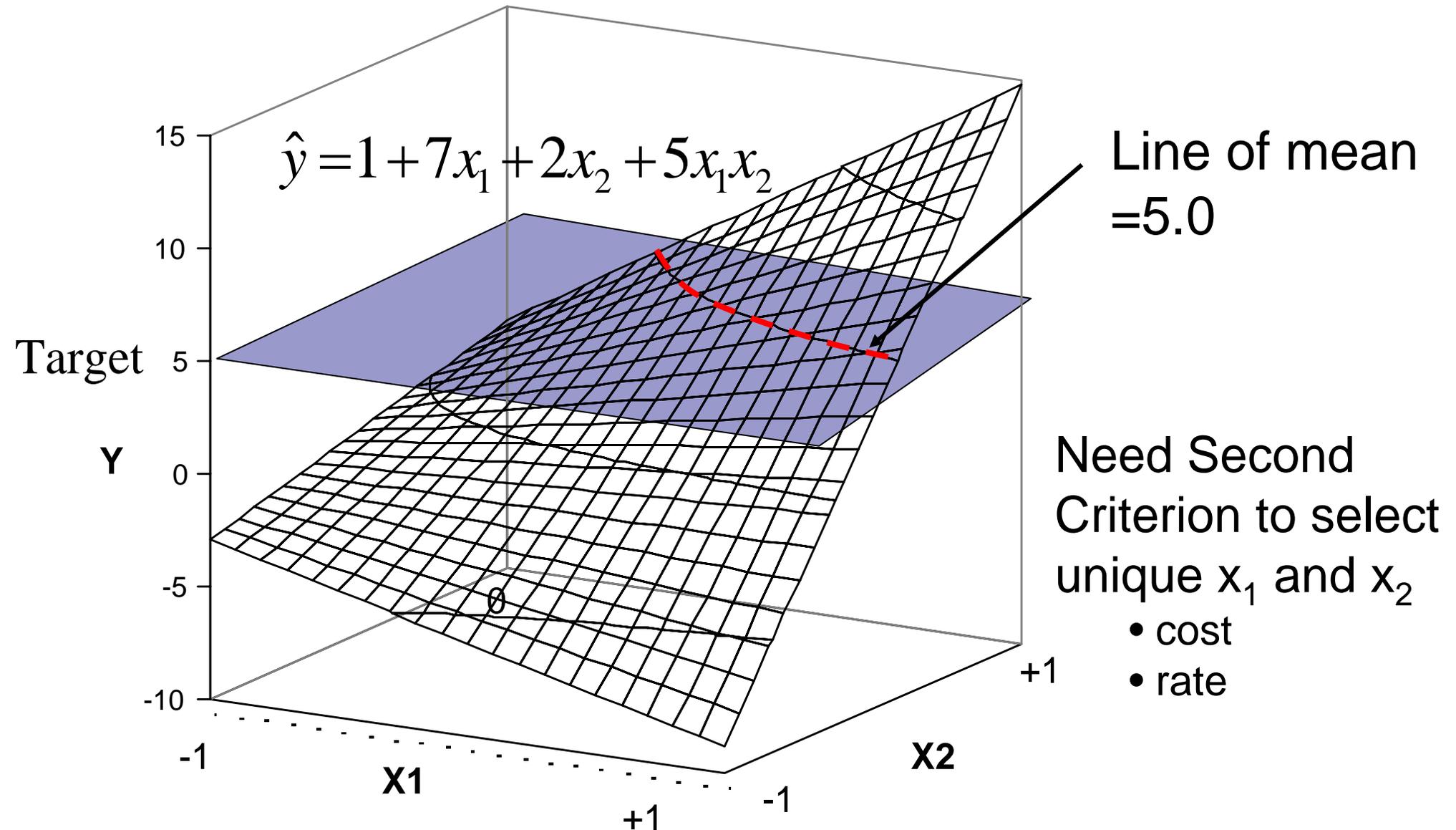
- Contours of constant output
- Match to Target
- Assume constant output variance

- Choose Operating Point to

- Minimize Cost (e.g. material usage; tool wear, etc)
- Minimize Cycle Time



# Linear Model with Constraint



# Quality: Minimum Variation

$$\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u$$

- Minimize Sensitivity to  $\Delta \alpha$ 
  - Process Robustness
- Maximize  $C_{pk}$
- Minimize expected quality loss:  $E\{L(x)\}$

# Maximizing Cpk

$$C_{pk} = \min\left(\frac{(USL - \mu)}{3\sigma}, \frac{(LSL - \mu)}{3\sigma}\right)$$

Measure using estimates of response of  $y$  and  $s$ :

$$C_{pk} = \min\left(\frac{(USL - \hat{y})}{3\hat{s}}, \frac{(LSL - \hat{y})}{3\hat{s}}\right)$$

Or create a new response variable from the raw data

$$\eta_j = \min\left(\frac{(USL - \bar{y}_j)}{3s_j}, \frac{(LSL - \bar{y}_j)}{3s_j}\right)$$

- Single variable that combines  $y$  and  $s$
- Could be discontinuous

# Variance Dependence on Operating Point

- We often assume that  $\sigma^2$  is constant throughout the operating space
  - Implicit in simple ANOVA, most regression fits
  - Process optimization might also assume this
    - E.g.  $C_{pk}$ ,  $E(L)$ , sensitivity to  $\alpha$  independent of  $u$
- Reality: process variation may be different at different operating points!
  - Imperfect control of  $u$  implies  $\delta Y/\delta u$  can vary, if model/dependence is nonlinear
  - Presence or sensitivity to noise may depend on  $u$

# Process Output Variance

- We can define the response variable as  $\eta = \sigma_j$  and solve for  $\underline{\eta} = \mathbf{X}\underline{\beta} + \underline{\varepsilon}$

	Input and Levels			Response Replicates			Within Test mean	Within Test std.dev.
Test	x 1	x 2		$\eta_{i1}$	$\eta_{i2}$	$\eta_{i3}$	y bar <sub>i</sub>	$S_i$
1	-	-		$\eta_{11}$	...	...	y bar <sub>1</sub>	$S_1$
2	+	-		...	...	...	y bar <sub>2</sub>	$S_2$
3	-	+		...	...	$\eta_{33}$	y bar <sub>3</sub>	$S_3$
4	+	+				$\eta_{43}$	y bar <sub>4</sub>	$S_4$

New Response Variable

# Process Output Variance

- Solve for  $\underline{\eta} = \mathbf{X}\underline{\beta} + \underline{\varepsilon}$  using the same  $\mathbf{X}$  matrix as with  $y$ .
- This will yield a “variance response surface”
- Linear model: minimum at the boundary

# Combining Mean and Variance:

- Find the line (or general function) defining minimum error from the  $y$  response surface
- Find the minimum variance using those constrained  $x_1$  and  $x_2$  values

# Combining Mean and Variance: Direct Method

$$\hat{y} = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2$$

y surface

$$y^* = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 = \text{target}$$

solve for  $x_1$

$$x_1 = \frac{(y^* - \beta_0 - \beta_1 x_2)}{\beta_1 + \beta_{12} x_2} x_2$$

(line on surface)

$$\hat{s} = \beta'_0 + \beta'_1 x_1 + \beta'_2 x_2 + \beta'_{12} x_1 x_2$$

s surface

# Combining Mean and Variance: Direct Method

Substitute for  $x_1$  in the  $s$  equation and find minimum

$$x_1 = \frac{(y^* - \beta_0 - \beta_1 x_2)}{\beta_1 + \beta_{12} x_2} x_2$$



$$\hat{s} = 1 + \beta'_1 x_1 + \beta'_2 x_2 + \beta'_{12} x_1 x_2$$

s surface

$\hat{s} = f(x_2)$  it will be non – linear in general

$$\frac{\partial \hat{s}}{\partial x_2} = 0 \quad \text{solve for } x_2$$

# Minimizing E(L)

$$E\{L(x)\} = k\sigma_x^2 + k(\mu_x - x^*)^2$$

define a new response variable:

$$\eta_j = ks_{\bar{y}_j}^2 + k(\bar{y}_j - y^*)^2$$

and find  $\min(\eta)$

NOTE: Since the response variable is *quadratic* in  $y$  and  $s$ , the new estimation model should be *quadratic* as well

# Problems?

- With Variance Varying?
- What Caused Non-Constant Variance?
- Can We Assess “Robustness”?

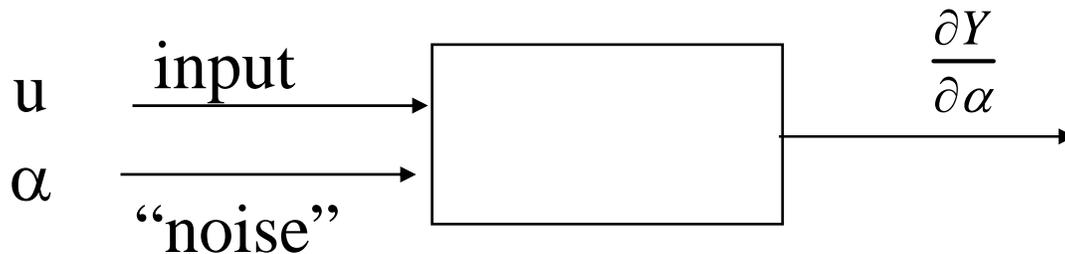
# Use of the Variation Model

Recall: 
$$\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u$$

$$\frac{\partial Y}{\partial \alpha} = f(u, \alpha)$$

Disturbance  
Sensitivity

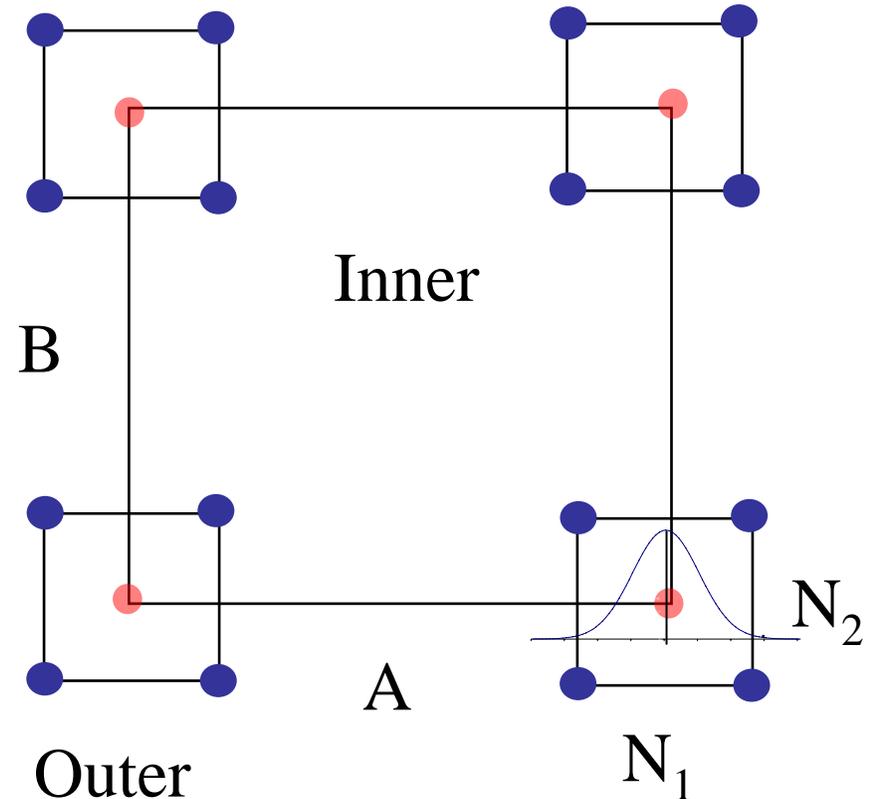
How would we minimize  $\frac{\partial Y}{\partial \alpha}$  ?



# Robustness to Noise Factors – Inner and Outer Factors

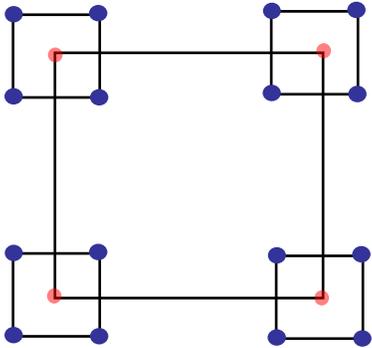
- Find Control Factors that Minimize Effect of Noise
- Taguchi Approach: Varying Noise Factors at Each Level of Control Factors

$k_n = \#$  noise factors  
 $k_c = \#$  control factors



Each corner gives a measure of  $\frac{\partial Y}{\partial \alpha}$

# Robustness to Noise Factors



## Crossed Array Design

### Outer Array

N1	-1	1	-1	1
N2	-1	-1	1	1

Variance caused by Outer array variations

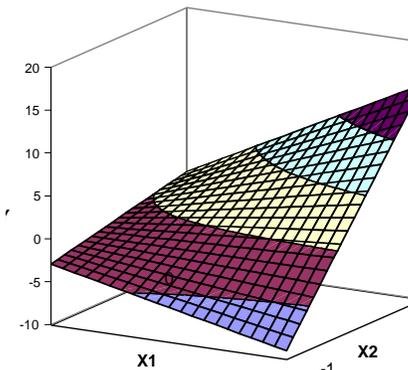
Number of Tests?

Inner Array

A	B					Average	Variance
-1	-1	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Ybar1	s21
1	-1	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Ybar2	s22
-1	1	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Ybar3	s23
1	1	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Y <sub>ij</sub>	Ybar4	s24

$$\text{Taguchi S/N} = -10 \log \frac{\bar{y}_i^2}{S_i^2}$$

S/N
SN1
SN2
SN3
SN4



# Taguchi – Signal-to-Noise Ratios

- Nominal the best:

$$SN_N = 10 \log(\bar{y}/s)$$

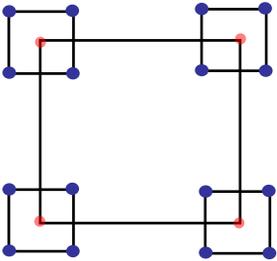
- Larger the better:

$$SN_L = -10 \log\left(\frac{1}{n} \sum_{i=1}^n \frac{1}{y_i^2}\right)$$

- Smaller the better:

$$SN_S = -10 \log\left(\frac{1}{n} \sum_{i=1}^n y_i^2\right)$$

# Crossed Array Method



- Number of tests
  - Control Factor tests \* Noise Factor tests
  - Linear model leads to linear response surface for S/N
  - True Optimum requires Quadratic test on inner array
    - # Tests =  $3^{kc} 2^{kn}$  unless interaction ignored
    - $3^{kc}$  requirement can be reduced with use of central composite or related designs

# Robustness Using Noise Response

$$\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u$$

$u$ : • control factors

$\alpha$ : • some can be manipulated if desired (Noise Factors)  
• some cannot (Pure error)

Treat *control and noise* as factors for experiments:

$$\hat{y} = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \gamma_1 z_1 + \delta_{11} x_1 z_1 + \delta_{21} x_2 z_1$$

$x_i$  are control factors,  $z_j$  are noise factors

# Noise Response Surface Approach

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \gamma_1 z_1 + \delta_{11} x_1 z_1 + \delta_{21} x_2 z_1 + \varepsilon$$

Assume  $z_1 : N(0, \sigma_z)$

$\varepsilon : N(0, \sigma)$

Full factorial in  $x_1$  and  $x_2$  (Control Factors)

Interaction terms for  $z_1$  (Noise Factors)

- Why are they vital?

# Noise Response Models

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \gamma_1 z_1 + \delta_{11} x_1 z_1 + \delta_{21} x_2 z_1 + \varepsilon$$

Assume  $z_1 : N(0, \sigma_z)$

$\varepsilon : N(0, \sigma)$

Mean of Response:

$$E(y) = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2$$

Variance of Response:

$$V(y) = (\gamma_1 + \delta_{11} x_1 + \delta_{21} x_2)^2 \sigma_z^2 + \sigma^2$$

Now variance is a function of control factors

# Variance Models

$$V(y) = (\gamma_1 + \delta_{11}x_1 + \delta_{21}x_2)^2 \sigma_z^2 + \sigma^2$$

$$V(x_1, x_2) = (\gamma_1^2 + 2\gamma_1\delta_{12}x_1 + 2\gamma_1\delta_{21}x_2 + \delta_{12}^2x_1^2 + \delta_{21}^2x_2^2 + 2\delta_{12}\delta_{21}x_1x_2)\sigma_z^2$$

Quadratic in  $x_1, x_2$

# Example: Robust Bending

- Control Factors
  - Depth of Punch  $x_1$
  - Width of Die  $x_2$
- Noise Factors
  - Yield Point of Material  $z_1$
  - Thickness of Material  $z_2$

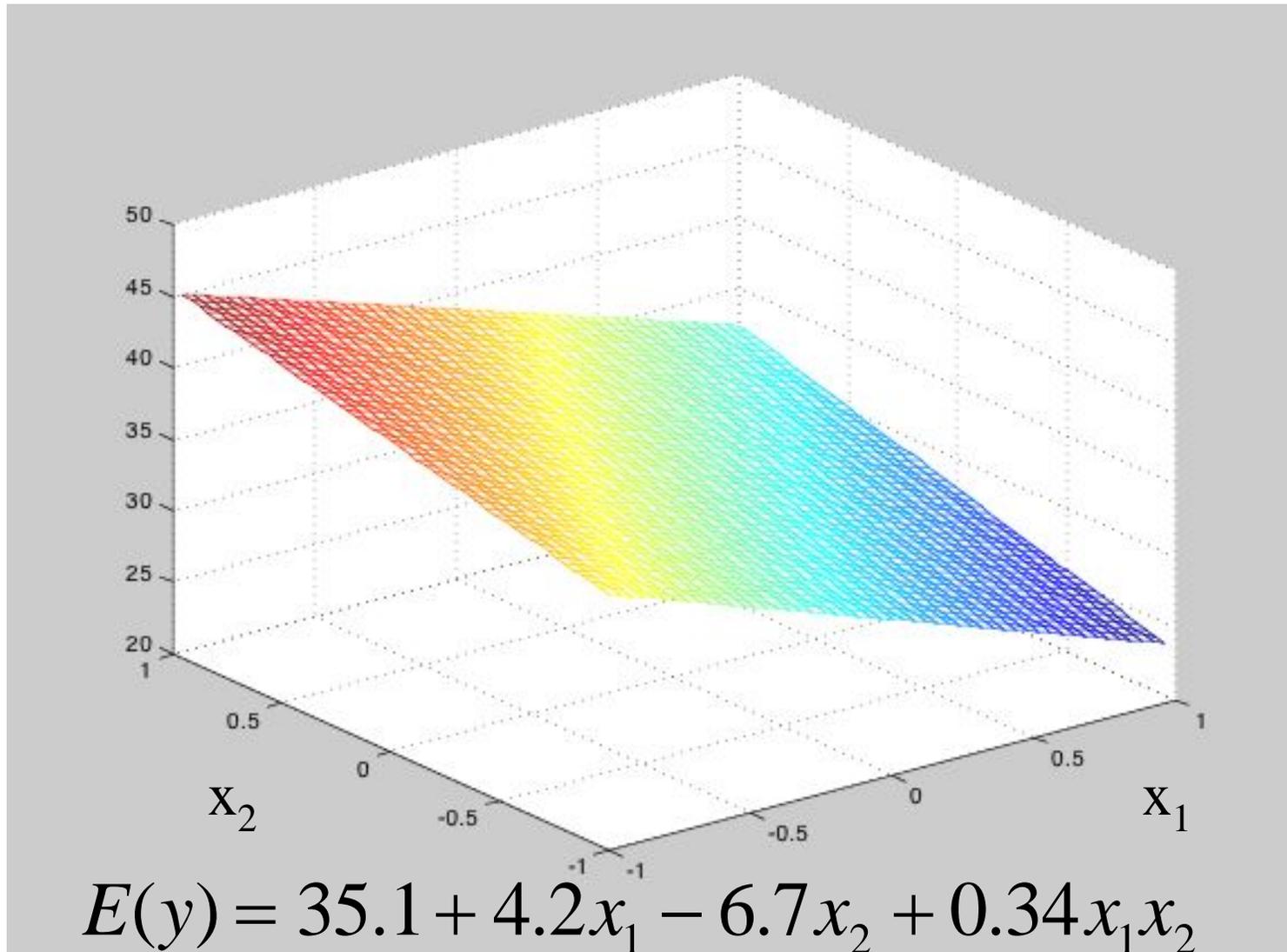
# Example: Robust Bending

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 + \gamma_1 z_1 + \delta_{11} x_1 z_1 + \delta_{21} x_2 z_1 + \varepsilon$$

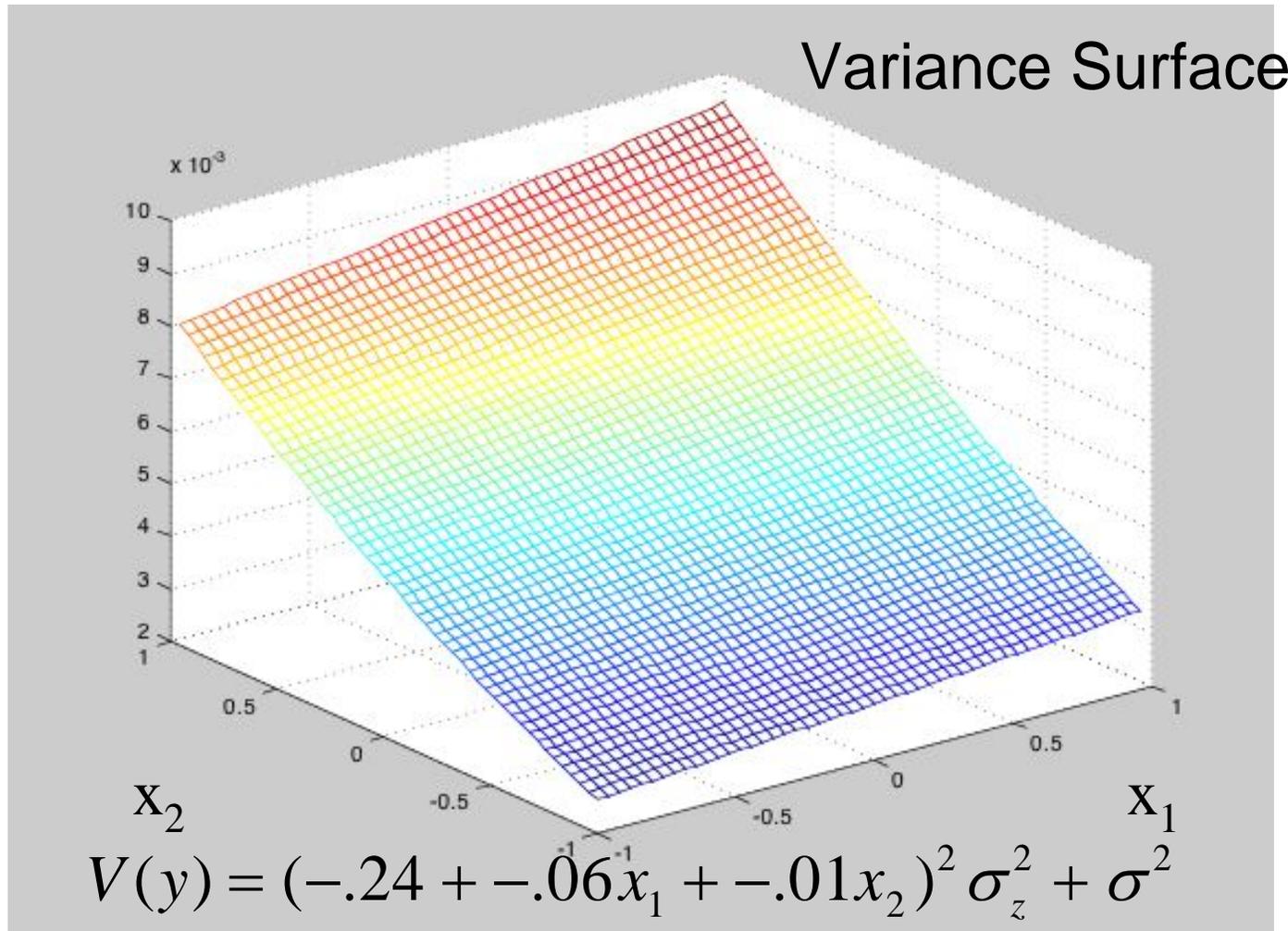
yp	w	sigma	Mean		
x1	x2	z	Angle		
-1	-1	-1	38.1	$\beta_0$	35.09
1	-1	-1	45.9	$\beta_1$	4.16
-1	1	-1	24.1	$\beta_2$	-6.69
1	1	-1	33.2	$\gamma_1$	-0.24
-1	-1	1	37.8	$\beta_{12}$	0.34
1	-1	1	45.3	$\delta_{11}$	-0.06
-1	1	1	23.7	$\delta_{21}$	-0.01
1	1	1	32.6	$\beta_{123}$	0.01

$$y = 35.1 + 4.2x_1 - 6.7x_2 + 0.34x_1x_2 - .24z_1 - .06x_1z_1 + -0.013x_2z_1 + \varepsilon$$

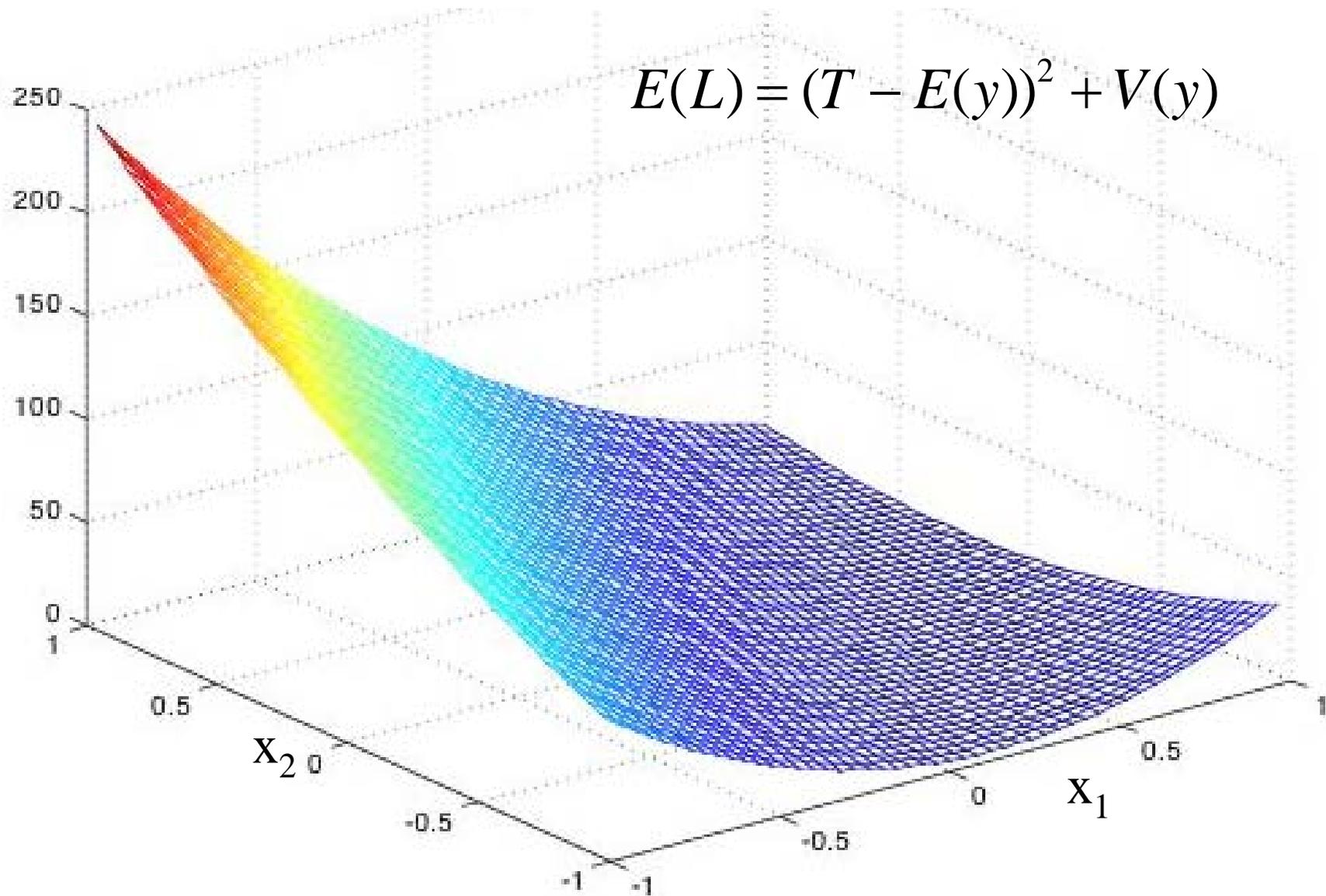
# Example: Robust Bending



# Example: Robust Bending



# Example: Robust Bending



# Response Model Method

- Define Control and Noise Factors
- Perform Appropriate Linear Experiment
- If possible scale noise factor changes to  $\pm 1 \sigma_z$ 
  - (Assumes we know noise factor statistics)
- Define Response Surface for V
- Optimize V, Subject to desired E(y)
- Number of Tests?
  - Full factorial with center point:  $(2^{kc}+1)(2^{kn})$
  - Quadratic in control:  $3^{kc} 2^{kn}$
  - RSM, full factorial with center point:  $(2^{kc+kn} + 1)$
  - RSM, central composite:  $2^{kc+kn}+2(kc+kn)+1$
- Taguchi orthogonal arrays: fractional factorials ignoring noise factor interactions

# Comparison

Control Factors	Noise Factors	Crossed Array Lin.	Crossed Array (quad)	Response Surface
2	1	8	18	6
2	2	16	36	13
3	3	64	216	60
4	3	128	648	124

- Crossed array with S/N does not adjust mean
- Size of Experiments is Large vs. RSM
- Forces use of Fractional Factorial DOE
  - Assumes little or no Interaction

# Conclusions: Process Optimization

- Cost, Rate, Quality
- Quality:
  - Min E(L)
  - Max  $C_{pk}$
  - Max S/N
- All depend on variation equation:

$$\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u \quad \longrightarrow \quad \frac{\partial Y}{\partial \alpha} = f(u, \alpha)$$