

# Reliability and Availability

This set of notes is a combination of material from Prof. Doug Carmichael's notes for 13.21 and **Chapter 8 of Engineering Statistics Handbook**. NIST/SEMATECH e-Handbook of Statistical Methods, <http://www.itl.nist.gov/div898/handbook/>, 2005.

available free from:

see: **NIST/SEMATECH e-Handbook of Statistical Methods on CD**

Including and improving reliability of propulsion (and other) systems is a challenging goal for system designers. An approach has developed to tackle this challenge:

1. a design and development philosophy
2. a test procedure for components and total systems
3. a modelling procedure based on test results, field tests and probability (statistics)

## ***Design and development philosophy***

recognition that reliability is a product is essentially the absence of failures or substandard performance of all critical systems in the design, followed by an examination of the factors leading to failure.

### ***Causes of failure:***

- a. loading: (inaccurate estimates of) thermal, mechanical or electrical including vibrations
- b. strength: (inaccurate estimates of) the load carrying capacity of the components
- c. environment: presence of dirt, high temperature, shock, corrosion, moisture, etc.
- d. human factors: heavy handed operators ("sailor proof"), wrong decisions (operator error), criminal activities (sabotage), poor design, tools left in critical components, use of incorrect replacements
- e. quality control: or lack thereof; loose control of materials and manufacture, lack of inspection, loose specifications
- f. accident; act of God, freak accidents, collisions
- g. acts of war: terrorism, war damage

designer should recognize these potential causes for failure and try to design devices that will resist failure.

## ***Detailed Design Features***

- a. try to account for all possible situations in the design stage and eliminate possible failures. Delivering maximum loads and minimum strengths
- b. assume that every component can fail, examine the outcome of the failure and try to reduce the risk of damage. Failure Modes and Effects Analysis (FEMA)
- c. institute strict quality control in manufacture and maintenance
- d. have clearly defined specifications (including material specifications and methods of testing)
- e. develop technology to meet new challenges. conduct development testing.
- f. consider possible war damage and ship collision
- g. carry out development testing in arduous conditions

## ***System Design Features***

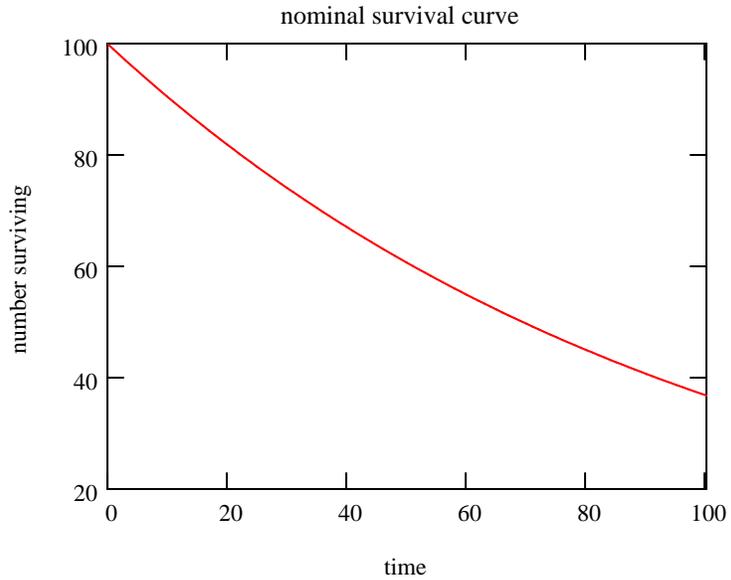
- a. calculate probability of failures. (reliability and availability analysis)
- b. improve system design by standby or redundant systems
- c. analyze failures, note trends
- d. specify clearly all operating procedures (good operating manuals)
- e. require inspection, maintenance and replacement procedures (trend analysis)

## ***Failure testing and analysis***

from field or laboratory tests on components or systems determine number of operating units as a function of time (life):

set up N\_surv

a typical survival curve might look like this:



define the failure rate at time t as

$$\lambda = \frac{\text{proportion failing in } \delta t}{\delta t} = \frac{-\delta N(t)}{N(t)} \cdot \frac{1}{\delta t} = \frac{-1}{N(t)} \cdot \frac{dN(t)}{dt} \quad - \text{ as "rate"} > 0 \text{ consistent with population decline} \quad \text{units are: } \text{time}^{-1}$$

$$-1 \cdot \frac{\frac{d}{dt}N(t)}{N(t)} = \lambda \quad -1 \cdot \frac{dN(t)}{N(t)} = \lambda \cdot dt \quad \ln\left(\frac{N(t)}{N(0)}\right) = -\int_0^t \lambda(\tau) d\tau \quad N(t) = N_I \cdot \exp\left(-\int_0^t \lambda(\tau) d\tau\right)$$

to make some estimates based on this sample:  $\text{fail\_rate}(t, \delta t) := \frac{N(t + \delta t) - N(t)}{N(t) \cdot \delta t}$  calculate for modest  $\delta t = 0.01$  and  $t = 10, 40, 60, 120$

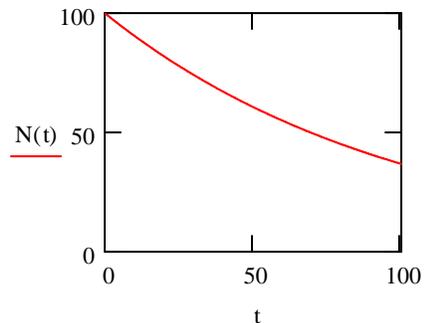
$$\text{fail\_rate}(40, 0.01) = 0.01 \quad \text{fail\_rate}(10, 0.01) = 0.01 \quad \text{fail\_rate}(60, 0.01) = 0.01 \quad \text{fail\_rate}(120, 0.01) = 0.01$$

looks like  $\lambda =$  failure rate is a constant, not unusual

$$\lambda = \frac{-1}{N(t)} \cdot \frac{d}{dt}N(t) = \text{constant}$$

define ...  $N_I = N(t = 0)$   $-1 \cdot \frac{\frac{d}{dt}N(t)}{N(t)} = \lambda$   $-1 \cdot \frac{\frac{d}{dt}N(t)}{N(t)} = \lambda$  integrate from 0 to t  $\ln\left(\frac{N(t)}{N(0)}\right) = -\int_0^t \lambda d\tau$

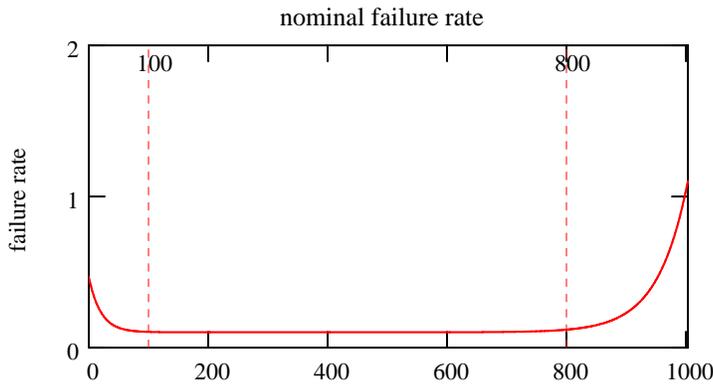
or ...  $N(t) = N_I \cdot \exp\left(-\int_0^t \lambda d\tau\right)$  set ...  $\lambda := 0.01$   $N_I := 100$   
 or ...  $N(t) := N_I \cdot \exp(-\lambda \cdot t)$



N.B. failure rate is not necessarily the same as (but can be related to) (in this case it is) the probability of failure see Engineering Statistics Handbook

an actual failure rate curve might look like this:

 set up bath tub



three regions are evident:

0 - 100 early failure period = infant mortality rate

100 - 800 intrinsic failure period aka stable failure period => intrinsic failure rate

> 800 wearout failure period - materials wear out and degradation failures occur at an ever increasing rate

for most systems, the failure rate is relatively constant except for wear in and wear out. If the failure rate is constant, the component is said to have random failure.

### Reliability

(applies to a particular mission with a defined duration.)

defined as the probability of operating without degraded performance during a specific time period. At time  $t_1$ , the number operating is  $N(t_1)$  and  $N_I$  is the initial number. The reliability is:

$$R(t_1) = \frac{N(t_1)}{N_I} \quad \text{since ...} \quad -1 \cdot \frac{dN(t)}{N(t)} = \lambda \cdot dt \quad \ln\left(\frac{N(t_1)}{N_I}\right) = -\int_0^{t_1} \lambda dt \quad R(t_1) = \frac{N(t_1)}{N_I} = \exp\left(-\int_0^{t_1} \lambda dt\right)$$

$$\text{with } \lambda = \text{constant} \quad R(t_1) = \exp(-\lambda \cdot t_1) \quad \text{and expanding in a series ...} \quad R(t_1) = 1 - \lambda \cdot t_1 + \frac{(\lambda \cdot t_1)^2}{2!} - \frac{(\lambda \cdot t_1)^3}{3!} + \dots$$

$$\text{and if ... } \lambda \cdot t_1 \ll 1, \quad R(t_1) = 1 - \lambda \cdot t_1 \quad \text{e.g. } \lambda t_1 := 0.05 \quad 1 - \lambda t_1 = 0.95 \quad \exp(-\lambda t_1) = 0.951$$

### Mean Time Between (Operational Mission) Failure (MTB(OM)F)

with field testing, data is collected in the form of operating time, failures and repair time.

During the field operation of a component or a system, there is a total number of operating hours and a total number of failures. MTB(OM)F is defined

$$\text{MTB(OM)F} = \frac{\text{accumulated\_life}}{\text{number\_of\_failures}}$$

$$\text{For random failures, the failure rate } \lambda = \frac{\text{number\_of\_failures}}{\text{accumulated\_life}} = \frac{1}{\text{MTB(OM)F}}$$

$$\text{if ... } \frac{t_1}{\text{MTB(OM)F}} < 1 \quad R(t_1) = 1 - \lambda \cdot t_1 = 1 - \frac{t_1}{\text{MTB(OM)F}}$$



## R out of N

see Handbook of Statistical Methods section 8.1.8.4.R out of N model

If a system has n components and requires any r to be operational; assuming

all components have the same reliability  $R_i$

all components operate independent of one another (as far as failure is concerned)

the system can survive any (n - r) components failing, but fails at the instant the (n - r + 1)th component fails

System reliability is given by the probability of exactly r components surviving to time t + the probability of exactly (r + 1) components surviving to time t ... up to all n surviving. These are binomial probabilities:

$$R_s(t) = \sum_{i=r}^n \left[ \binom{n}{i} \cdot R_i^i \cdot (1 - R_i)^{n-i} \right]$$

for example (where  $R_i$  are not necessarily equal ...  $n = 4$   $r = 2$  i.e. four components of which two are required for operation

2 components  $R_1 \cdot R_2 \cdot Q_3 \cdot Q_4 + R_1 \cdot R_3 \cdot Q_2 \cdot Q_4 + R_1 \cdot R_4 \cdot Q_2 \cdot Q_3 + R_2 \cdot R_3 \cdot Q_1 \cdot Q_4 + R_2 \cdot R_4 \cdot Q_1 \cdot Q_3 + R_3 \cdot R_4 \cdot Q_1 \cdot Q_2$

3 components  $R_1 \cdot R_2 \cdot R_3 \cdot Q_4 + R_1 \cdot R_3 \cdot R_4 \cdot Q_2 + R_1 \cdot R_2 \cdot R_4 \cdot Q_3 + R_2 \cdot R_3 \cdot R_4 \cdot Q_1$

n = 4 components  $R_1 \cdot R_2 \cdot R_3 \cdot R_4$

sum all these for  $R_s$

$$R_s = R_1 \cdot R_2 \cdot Q_3 \cdot Q_4 + R_1 \cdot R_3 \cdot Q_2 \cdot Q_4 + R_1 \cdot R_4 \cdot Q_2 \cdot Q_3 + R_2 \cdot R_3 \cdot Q_1 \cdot Q_4 + R_2 \cdot R_4 \cdot Q_1 \cdot Q_3 + R_3 \cdot R_4 \cdot Q_1 \cdot Q_2 \dots$$

$$+ R_1 \cdot R_2 \cdot R_3 \cdot Q_4 + R_1 \cdot R_3 \cdot R_4 \cdot Q_2 + R_1 \cdot R_2 \cdot R_4 \cdot Q_3 + R_2 \cdot R_3 \cdot R_4 \cdot Q_1 \dots$$

$$+ R_1 \cdot R_2 \cdot R_3 \cdot R_4$$

N.B. a series system is one with  $r = n$  i.e. all components must operate. a parallel system is one with  $r = 1$

## Standby Systems

Standby scenario will be more reliable than parallel as seen in Handbook of Statistical Methods section 8.1.8.5.Standby model

## Availability

Availability is the probability that a component is operational, i.e. it is not being repaired

$$MTTR = \text{mean\_time\_to\_repair} = \frac{\text{total\_time\_for\_repairs}}{\text{number\_of\_repairs}}$$

For every failure there should be a repair, so that the average component is repaired for the average time after it has operated for the average time between failures. Average time between failures is MTBF and for repair MTTR, so assuming component is either operating or being repaired ...

$$\text{availability} = A = \frac{\text{operating\_time}}{\text{operating\_time} + \text{repair\_time}} = \frac{\text{MTBF}}{\text{MTBF} + \text{MTTR}}$$

if ...  $\text{MTBF} > \text{MTTR}$  ( $\ll$ ) which it should be ...

$$A = \frac{MTBF}{MTBF + MTTR} = 1 - \frac{MTTR}{MTBF} \quad \frac{1}{1+a} = (1+a)^{-1} = 1-a \quad a < 1 \quad (<<)$$

probability that it is being repaired is ...  $Q_A$        $Q_A = 1 - A = \frac{MTTR}{MTBF}$

and as above, availability for series systems would be ..  $A_{series} = A_1 \cdot A_2 \cdot A_3 \dots A_n = \prod_n A_i$

and parallel ...  $A_{parallel} = 1 - Q_1 \cdot Q_2 \cdot Q_3 \dots Q_n = 1 - \prod_n Q_i$