

d. EHP

$$PE := \text{Thrust} \cdot (1 - t) \cdot \frac{V_s}{550 \frac{\text{lb} \cdot \frac{\text{ft}}{\text{sec}}}{\text{hp}}}$$

$$PE = 1.433 \times 10^3 \text{ hp}$$

e. Quasi Efficiency

$$\eta_D := \frac{PE}{PD}$$

$$\eta_D = 0.74$$

f. Propeller rpm and thrust at 50,000.

$$\text{Advance_velocity} := 0$$

$$\text{Torque}_{\text{max}} := 50000 \text{ lb-ft}$$

$$n_o := \sqrt{\frac{\text{Torque}_{\text{max}}}{\rho \cdot K_Q \cdot d^5 \cdot \eta_R}}$$

$$n_o = 3.305 \frac{1}{\text{s}}$$

$$n_q := n_o \cdot 60 \cdot \text{sec}$$

$$n_q = 198.286$$

$$\text{Thrust}_q := K_T \cdot \rho \cdot n_q^2 \cdot d^4$$

$$\text{Thrust}_q = 9.391 \times 10^7 \text{ s}^2 \text{ lb}$$

2. A propeller is to be selected for a single-screw container ship with the following features:

EHP = 80000 HP, ship speed = 25 kts, maximum propeller diameter = 34 ft, $w = 0.249$, $t = 0.18$, $\eta_R = 1.0$, centerline depth, $h = 25$ ft

a. Using the maximum prop diameter, determine the optimum B 5-90 design. Use the metrics below to confirm your design.

- a. P/D
- b. K_T (optimum)
- c. K_Q (optimum)
- d. η_o (optimum)
- e. J
- f. Developed HP
- g. The (Quasi) PC or η_D
- h. RPM

From the consideration of cavitation, determine:

- i. The predicted cavitation (%) using the Burrill correlation
- j. The expanded area ratio (EAR) to provide 5% cavitation for a commercial ship.

Assume the operating conditions are similar to the B 5-90 propeller.

Given $V_2 := 25\text{-knot}$ $EHP := 80000\text{hp}$ $d_2 := 34\text{-ft}$ $w_2 := .249$ $t_2 := .18$ $\eta_R := 1$ $h := 25$

First we must combine a couple of equations in order to get all the information we know in terms of K_T and J.

$$R_2 := \left(550 \frac{\text{lb} \cdot \frac{\text{ft}}{\text{sec}}}{\text{hp}} \right) \cdot \frac{\text{EHP}}{V_2} \quad T_2 := \frac{R_2}{1 - t_2} \quad K_t := \frac{T_2}{\rho \cdot n_2^2 \cdot d_2^4} \quad J_2 := \frac{V_2}{n_2 \cdot d_2}$$

$$\frac{K_t}{J_2^2} \rightarrow \frac{\left(550 \frac{\text{lb} \cdot \frac{\text{ft}}{\text{sec}}}{\text{hp}} \right) \cdot (\text{EHP})}{\rho \cdot V_2^3 \cdot d_2^2 \cdot (1 - t_2) \cdot (1 - w_2)^2} = 0.55$$

Now we can plot the function $K_T = 0.55 \cdot J^2$ on the B 5-90 curve graph. Drawing a verticle line where the function plot and each $K_T - P/D$ intersect will provide a value for K_T and η_0 . Starting with a logical P/D (.5 for example), step though P/D values, recording K_T and η_0 . Take note at the peak value for η_0 , That will determine optimal values. Using the curves posted on the web, I found:

$P/D = 1.2 \quad K_T = .29 \quad \eta_0 = .6$

a. $P/D = 1.2$

$K_t := .29$

b. $K_T(\text{opt}) = .29$

$J_2 := \sqrt{\frac{K_t}{.55}}$

$K_q := .055$

c. $K_Q(\text{opt}) = .055$

$\eta_{o2} := .6$

d. $\eta_0 = .6$

$Q_2 := K_q \cdot \rho \cdot n^2 \cdot d^5$

e. $J = 0.726$

$J_2 = 0.726$

$PC := \eta_{o2} \cdot \left(\frac{1 - t}{1 - w} \right) \cdot \eta_R$

f. $HP = 124200 \text{ HP}$

$PD_2 := \frac{\text{EHP}}{\text{PC}}$

$PD_2 = 1.242 \times 10^5 \text{ hp}$

g. $PC = .644$

$n_2 := V_2 \cdot \frac{1 - w_2}{J_2 \cdot d_2}$

$n_2 = 1.284 \frac{1}{s}$

$PC = 0.644$

h. $RPM = 77.012$

$N_2 := n_2 \cdot 60 \cdot s$

$N_2 = 77.012$

Cavitation Calculations

$\text{EAR} := 90 \quad P_{\text{over}_D_{\text{ans}}} := 1.2$

$h_{\text{max}} := 25\text{ft}$

$A_E := \text{EAR} \cdot \frac{\pi \cdot d_2^2}{4}$

assume $A_D \sim A_E$

$$A_P := A_E \cdot [1.067 - 0.229(P_{\text{over_D_ans}})]$$

$$V_R := \left[\left[V_2 \cdot (1 - w_2) \right]^2 + \left(0.7\pi \cdot n \cdot d_2 \right)^2 \right]^{\frac{1}{2}}$$

$$\tau_C := \frac{\frac{T}{A_P}}{\frac{1}{2} \cdot \rho \cdot V_R^2} \quad A_E = 7.591 \times 10^3 \text{ m}^2 \quad \tau_C = 5.421 \times 10^{-10} \frac{1}{\text{A} \cdot \text{s}^2}$$

$$\sigma_{0.7R} := \frac{2026 \frac{\text{ft}^4}{\text{sec}^4} + 64.4 \frac{\text{ft}^3}{\text{sec}^4} \cdot h}{V_R^2 + 4.836 \left(N_2 \cdot \frac{1}{s} \right)^2 \cdot d_2^2 \text{ ft}^2} \cdot \text{sec}^2 \quad \sigma_{0.7R} = 1.095 \times 10^{-4}$$

$$C_{\text{ww}} := \frac{\tau_C \cdot A \cdot \text{s}^2 + 0.3064 - 0.523 \sigma_{0.7R}^{0.2}}{0.0305 \sigma_{0.7R}^{0.2} - 0.0174} \quad C = -17.791 \quad \% \text{ cavitation}$$

Negative cavitation indicates that it is not a problem with at this speed

i. Cavitation = - 17.8%

$$\tau_{Cn} := C \cdot \left[.0305 \left(\sigma_{0.7R}^{0.2} \right) - . \times 0174 \right] - .3064 + .523 \sigma_{0.7R}^{0.2}$$

$$A_{pn} := \frac{T}{\left(.5 \cdot \rho \cdot \tau_{Cn} \cdot V_R^2 \right)} \quad EAR_n := \frac{A_{pn}}{\left[1.067 - .229 \cdot 1.2 \cdot \pi \cdot \frac{(34^2)}{4} \right]}$$

j. = EAR is much less than one, Changing to meet these requirements would not be necessary. (This will be considered extra credit)

3. List the advantages and disadvantages of the fixed pitch propeller, controllable pitch propeller, and waterjet propulsion systems. List the best applications (or platform(s)) for each propulsor and supporting reasons considering the mission of the platform. (expectation: half a page of concise thought).

For full credit - A brief discussion similar to that in chapter 6 of the text, At least 2 advantages and 2 disadvantages of each and an example of where each has been used successfully.