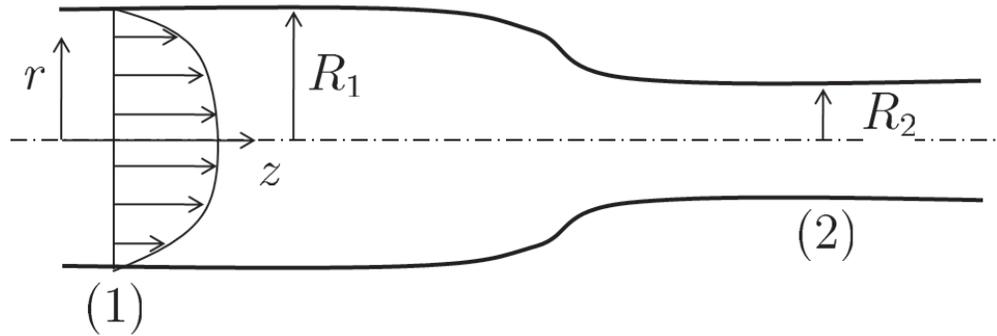


MIT Department of Mechanical Engineering
2.25 Advanced Fluid Mechanics

Problem 10.05

This problem is from "Advanced Fluid Mechanics Problems" by A.H. Shapiro and A.A. Sonin



An inviscid, incompressible fluid flows steadily through a circular pipe with a contraction. At the entrance section, the velocity is purely in the axial direction and is given by :

$$u_1(r) = V_o \left(1 - \left(\frac{r}{R_1} \right)^2 \right)$$

- (a) What does the vorticity field look like at the entrance section?
- (b) What is the velocity profile at the exit?

Solution:

(a) In the cylindrical coordinate, the vorticity is defined as

$$\omega = \nabla \times \mathbf{V} \quad (10.05a)$$

$$\nabla = \frac{\partial}{\partial r} \hat{\mathbf{e}}_r + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{\mathbf{e}}_\theta + \frac{\partial}{\partial z} \hat{\mathbf{e}}_z \quad (10.05b)$$

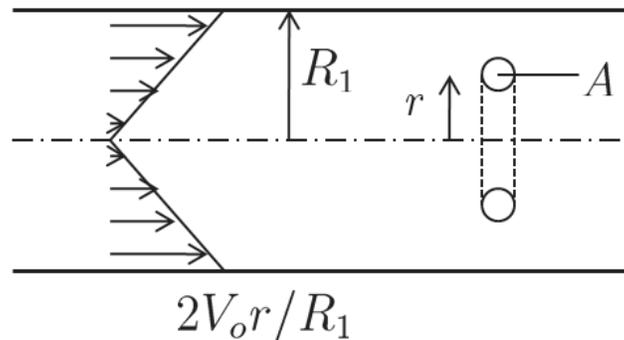
Since the flow is axially symmetric, $v_\theta = \partial/\partial\theta = 0$. And the radial velocity in this problem is zero, i.e., $v_r = 0$. Therefore,

$$\omega = -\frac{\partial v_z}{\partial r} \hat{\mathbf{e}}_\theta, \quad \text{where } v_z = u \quad (10.05c)$$

Substituting the given velocity profile gives

$$\omega = V_o \frac{2r}{R_1^2} \hat{\mathbf{e}}_\theta \quad (10.05d)$$

The vortex distribution looks like as following. The vortex tube looks like a ring.



(b) Kelvin's Circulation Theorem

The Kelvin's theorem represents that the circulation remains at a constant in an inviscid, barotropic flow with conservative body forces.

$$\frac{d\Gamma}{dt} = 0 \Rightarrow \underline{\omega_1 A_1 = \omega_2 A_2 = const} \quad \text{follow same tube} \quad (10.05e)$$

The mass conservation of the tube gives

$$A_1 2\pi r_1 = A_2 2\pi r_2 \Rightarrow \frac{\omega_1}{\omega_2} = \frac{A_2}{A_1} = \frac{r_1}{r_2} \quad (10.05f)$$

Hence, the Kelvin's theorem is

$$\frac{\omega_1}{r_1} = \frac{\omega_2}{r_2} \quad (10.05g)$$

Using the fact above and the $\omega_1 = \omega_\theta$ at section (1), the velocity at section (2) becomes

$$-\frac{\partial u_2}{\partial r} = \frac{2V_o r}{R_1^2} \Rightarrow u_2(r) = -\frac{V_o r^2}{R_1^2} + c \quad (10.05h)$$

Let's obtain the constant c by mass conservation between section (1) and (2).

$$\int_0^{R_1} V_o \left(1 - \left(\frac{r}{R_1}\right)^2\right) 2\pi r \, dr = \int_0^{R_2} \left(-\frac{V_o r^2}{R_1^2} + c\right) 2\pi r \, dr \quad (10.05i)$$

$$\frac{\pi V_o}{2} R_1^2 = 2\pi \left(-\frac{V_o R_2^4}{4R_1^2} + \frac{1}{2} c R_2^2\right) \quad (10.05j)$$

Then the constant c and the velocity profile at section (2) are

$$c = \frac{1}{2} V_o \frac{R_1^2}{R_2^2} + \frac{1}{2} V_o \frac{R_2^2}{R_1^2} \quad (10.05k)$$

$$\Rightarrow u_2(r) = -\frac{V_o}{R_1} r^2 + \frac{V_o}{2} \left(\frac{R_1}{R_2}\right)^2 \left\{1 + \left(\frac{R_2}{R_1}\right)^2\right\} \quad (10.05l)$$

□

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