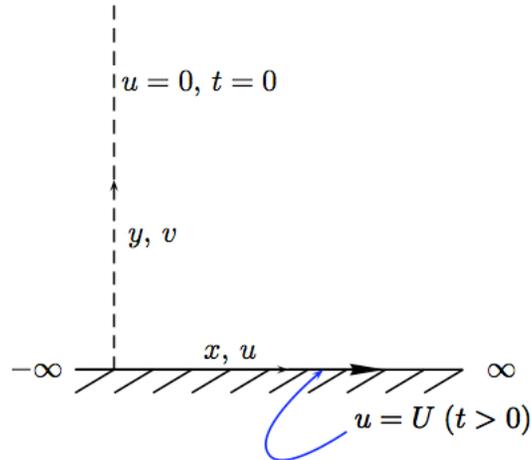


MIT Department of Mechanical Engineering
2.25 Advanced Fluid Mechanics

Stokes First Problem ATP



Consider Stokes' First Problem: impulsive start of a flat plate beneath a semi-infinite layer of initially quiescent incompressible fluid. The governing equations (presuming parallel flow — no instabilities) for $u(y, t)$ are:

$$\rho \frac{\partial u}{\partial t} = \mu \frac{\partial^2 u}{\partial y^2}, \quad 0 < y < \infty, \quad (1)$$

$$u(y = 0, t) = U, \quad (2)$$

$$u(y \rightarrow \infty, t) \rightarrow 0, \quad (3)$$

$$u(y, t = 0) = 0. \quad (4)$$

The shear stress at the wall is then given by

$$\tau_W(t) = \mu \left. \frac{\partial u}{\partial y} \right|_{y=0}. \quad (5)$$

Here ρ is the density and μ is the dynamic viscosity. The shear stress at the wall will be of the form

$$\tau_W = CU^{\alpha_1} \rho^{\alpha_2} \mu^{\alpha_3} t^{\alpha_4}, \quad (6)$$

where C is a non-dimensional constant. Find the exponents α_1 , α_2 , α_3 , and α_4 by dimensional analysis.

Hint (one approach): Write the equations in terms of u/U ; apply Buckingham Pi with as few variables as possible; apply the chain rule.

Solution:

$$\tilde{u} = fcn(y, t, \nu)$$

ϕ (dimensionless) L^* T^* $L^2 T^{-1}$

where \tilde{u} is dimensionless; y has units of length, \mathcal{L} ; t has units of time, \mathcal{T} , and ν is given in $\mathcal{L}^2 \mathcal{T}^{-1}$. Then, there are three remaining variables and two remaining dimensions; therefore there is one more dimensional group.

So, $\Pi_1 = \tilde{u}$ (or any multiple), and $\Pi_2 = \nu y^{\alpha_2} t^{\beta_2}$. Now, choosing α_2, β_2 such that,

$$2 + \alpha_2 = 0, \quad (7)$$

$$-1 + \beta_2 = 0, \quad (8)$$

$$\alpha_2 = -2, \quad \beta_2 = 1, \quad (9)$$

Then,

$$\Pi_2 = \nu t / y^2 \quad (10)$$

or

$$\Pi_1 = fcn_*(\Pi_2^0) \quad (11)$$

where Π_2^0 can be replaced with any function of Π_2 ; choose (convention) $\Pi_2 = (\Pi_2^0)^{-1/2} = y / \sqrt{\nu t}$

$$\Pi_1 = fcn_*(\Pi_2), \quad (12)$$

or

$$\frac{u}{U} = fcn_*(y / \sqrt{\nu t}) = f_I(y / \sqrt{\nu t}) \quad (13)$$

furthermore, using the chain rule,

$$\tau_W = -\mu \frac{\partial u}{\partial y} \Big|_{y=0} = -\mu f_I'(0) \frac{U}{\sqrt{\nu t}}, \quad (14)$$

where $f_I'(0)$ is a 'universal constant'.

Now, if we define

$$\delta_\epsilon = y \quad \text{such that} \quad \frac{u(\delta_\epsilon)}{U} = \epsilon, \quad (15)$$

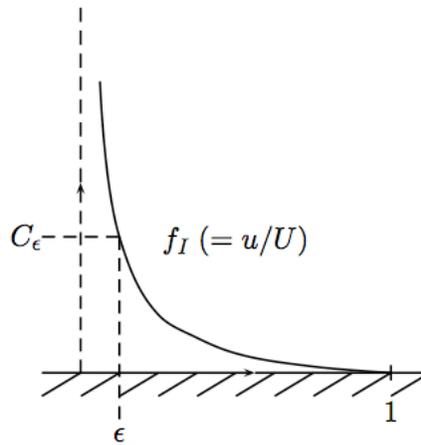
then,

$$f_I\left(\frac{\delta_\epsilon}{\sqrt{\nu t}}\right) = \epsilon \quad (16)$$

$$\frac{\delta_\epsilon}{\sqrt{\nu t}} = C_\epsilon, \quad (17)$$

$$\delta_\epsilon = C_\epsilon \sqrt{\nu t}. \quad (18)$$

Then, the effect of the wall penetrates as $\sqrt{\nu t}$ (shear accelerates fluid, decreases stress, ...).



□

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Fall 2013

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