

2.094

FINITE ELEMENT ANALYSIS OF SOLIDS AND FLUIDS SPRING 2008

Homework 7 - Solution

Instructor:	Prof. K. J. Bathe	Assigned:	04/03/2008
		Due:	04/10/2008

Problem 1 (20 points):

(a)

$${}^0\underline{X} = {}^0\underline{R} {}^0\underline{U} = \begin{bmatrix} \cos 45^\circ & -\sin 45^\circ \\ \sin 45^\circ & \cos 45^\circ \end{bmatrix} \begin{bmatrix} \frac{1}{2} & 0 \\ 0 & \frac{3}{4} \end{bmatrix} = \frac{1}{\sqrt{2}} \begin{bmatrix} \frac{1}{2} & -\frac{3}{4} \\ \frac{1}{2} & \frac{3}{4} \end{bmatrix}$$

$${}^t\underline{X} = ({}^0\underline{X})^{-1} = \begin{bmatrix} \sqrt{2} & \sqrt{2} \\ -\frac{2\sqrt{2}}{3} & \frac{2\sqrt{2}}{3} \end{bmatrix}$$

(b)

$${}^t\uunderline{\varepsilon} = \frac{1}{2} ({}^t\underline{X}^T {}^0\underline{X} - \underline{I}) = \begin{bmatrix} \frac{17}{18} & \frac{5}{9} \\ \frac{5}{9} & \frac{17}{18} \end{bmatrix}$$

$${}^t\underline{S} = \begin{bmatrix} 11 & 7 & 0 \\ 7 & 11 & 0 \\ 0 & 0 & 9 \end{bmatrix} \begin{bmatrix} \frac{17}{18} \\ \frac{17}{18} \\ \frac{5}{9} \end{bmatrix} = \begin{bmatrix} 17 \\ 17 \\ 5 \end{bmatrix}$$

$$\frac{{}^t\rho}{{}^0\rho} = \frac{{}^0V}{{}^tV} = \frac{(1.5)(1)(thickness)}{(2)(2)(thickness)} = \frac{3}{8}$$

Therefore,

$${}^t\tau = \frac{{}^t\rho}{{}^0\rho} {}^tX {}^0S {}^tX^T = \begin{bmatrix} 33 & 0 \\ 0 & 8 \end{bmatrix}$$

$${}^t\tau_{11} = 33, \quad {}^t\tau_{22} = 8, \quad {}^t\tau_{12} = 0$$

Hence the Cauchy stress ${}^t\tau$ given by the program is not correct.

We can identify the program error by noting that $\frac{33+8}{2} = 20.5$, $20.5 + 12.5 = 33$ and $20.5 - 12.5 = 8$. Hence a

rotation of 45° was wrongly applied. Therefore,

$${}^t\tau|_{\text{program}} = R {}^t\tau|_{\text{above}} R^T \text{ where } R = \begin{bmatrix} \cos 45^\circ & -\sin 45^\circ \\ \sin 45^\circ & \cos 45^\circ \end{bmatrix}$$

Problem 2 (10 points):

Since $H, h \ll b$, we only consider the displacement u_r in the x_1 -direction with the plane stress assumption.

Total Lagrangian formulation

$${}^t f^B = {}^t\rho {}^t r \omega^2$$

$${}^0 t = H \left(\frac{r-b}{a-b} \right) + h \left(\frac{r-a}{b-a} \right), \quad {}^t t = H \left(\frac{r-{}^t b}{{}^t a - {}^t b} \right) + h \left(\frac{r-{}^t a}{{}^t b - {}^t a} \right) \text{ (Thickness)}$$

$${}_0 e_{rr} = \frac{\partial u_r}{\partial {}^0 r} + \frac{\partial {}^t u_r}{\partial {}^0 r} \frac{\partial u_r}{\partial {}^0 r}, \quad {}_0 \eta_{rr} = \frac{1}{2} \left(\frac{\partial u_r}{\partial {}^0 r} \right)^2$$

$${}_0 e_{\theta\theta} = \frac{u_r}{{}^0 r} + \frac{{}^t u_r u_r}{{}^0 r^2}, \quad {}_0 \eta_{\theta\theta} = \frac{1}{2} \left(\frac{u_r}{{}^0 r} \right)^2$$

Therefore,

$$\begin{aligned} & \int_a^b {}_0C_{ijrs} e_{rs} \delta_0 e_{ij}^0 r^0 t dr + \int_a^b {}_0^t S_{ij} \delta_0 \eta_{ij}^0 r^0 t dr \\ &= \int_{t+\Delta t}^{t+\Delta t+b} \rho^t r \omega^2 r^t t \delta u_r dr - \int_a^b {}_0^t S_{ij} \delta_0 e_{ij}^0 r^0 t dr \end{aligned}$$

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Spring 2011

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