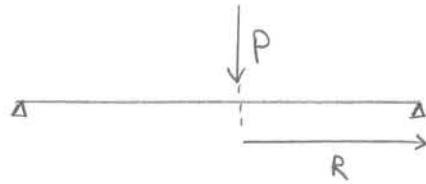


## Recitation 6: Energy Methods

### Example 1

A circular plate simply supported at its periphery is loaded in the center with point force,  $P$ .



Find the center deflection,  $w_0$ .

$$\textcircled{1} \text{ Assume a deflection shape: } w(r) = w_0 \left[ 1 - \left( \frac{r}{R} \right)^2 \right]$$



$$\textcircled{2} \text{ Calculate } U: U = \int_S \tilde{U} dA$$

For a plate,  $\tilde{U}_b = \frac{D}{2} [(\kappa_{11} + \kappa_{22})^2 - 2(1-\nu)(\kappa_{11}\kappa_{22} - \kappa_{12}^2)]$  (eqn. 4.112)

In our case,

$$\kappa_{11} = \kappa_r = -\frac{\partial^2 w}{\partial r^2} \quad (6.1)$$

$$\kappa_{22} = \kappa_\theta = -\frac{1}{r} \frac{\partial w}{\partial r} \quad (6.2)$$

$$\kappa_{12} = \kappa_{r\theta} = 0 \quad (6.3)$$

$$\frac{\partial w}{\partial r} = -2w_0 \frac{r}{R^2}, \quad \frac{\partial^2 w}{\partial r^2} = -\frac{2w_0}{R^2} \quad (6.4)$$

So

$$\left. \begin{aligned} \kappa_r &= -\frac{\partial^2 w}{\partial r^2} = \frac{2w_0}{R^2} \\ \kappa_\theta &= -\frac{1}{r} \frac{\partial w}{\partial r} = \frac{2w_0}{R^2} \end{aligned} \right\} \kappa_r = \kappa_\theta \quad (6.5)$$

$$\begin{aligned} \tilde{U}_b &= \frac{D}{2} [(\kappa_r + \kappa_\theta)^2 - 2(1-\nu)\kappa_r\kappa_\theta] \\ &= \frac{D}{2} [4\kappa_r^2 - 2(1-\nu)\kappa_r^2] = D(1+\nu)\kappa_r^2 = 40(1+\nu) \frac{w_0^2}{R^4} \end{aligned} \quad (6.6)$$

$$\begin{aligned} U &= \int_S \tilde{U}_b dA = \int_0^{2\pi} \int_0^R 4D(1+\nu) \frac{w_0^2}{R^4} r dr d\theta \\ &= 4D(1+\nu) \frac{w_0^2}{R^4} \cdot 2\pi \frac{R^2}{2} = 4\pi D(1+\nu) \frac{w_0^2}{R^2} \end{aligned} \quad (6.7)$$

③ Calculate work of external forces,  $W$

$$W = Pw_0 \quad (6.8)$$

$$\textcircled{4} \text{ Calculate } \Pi = U - W: \Pi = 4\pi D(1+\nu) \frac{w_0^2}{R^2} - Pw_0$$

$$\textcircled{5} \text{ Find } w_0(P) \text{ by setting } \frac{\partial \Pi}{\partial w_0} = 0:$$

$$8\pi D(1+\nu) \frac{w_0}{R^2} - P = 0 \quad (6.9)$$

$$\rightarrow \boxed{w_0 = \frac{PR^2}{8\pi D(1+\nu)}} \quad (6.10)$$

### Example 2

Same plate as Example 1, but with uniform pressure load,  $p$ . Find center deflection, and compare to the exact solution in Lecture 7.

$$\textcircled{1} \text{ Deflected shape should be the same: } w(r) = w_0 \left[ 1 - \left( \frac{r}{R} \right)^2 \right]$$

$$\textcircled{2} \text{ } U = 4\pi D(1+\nu) \frac{w_0^2}{R^2}$$

$$\begin{aligned} \textcircled{3} \text{ } W &= \int_S p w dA \\ &= \int_0^{2\pi} \int_0^R p w_0 \left[ 1 - \left( \frac{r}{R} \right)^2 \right] r dr d\theta \\ &= 2\pi p w_0 \left( \frac{r^2}{2} - \frac{r^4}{4R^2} \right) \Big|_0^R = 2\pi p w_0 \left( \frac{R^2}{2} - \frac{R^2}{4} \right) = \frac{\pi}{2} p w_0 R^2 \end{aligned}$$

$$\textcircled{4} \text{ } \Pi = U - W = 4\pi D(1+\nu) \frac{w_0^2}{R^2} - \frac{\pi}{2} p w_0 R^2$$

$$\textcircled{5} \text{ } \frac{\partial \Pi}{\partial w_0} = 0 \rightarrow 8\pi D(1+\nu) \frac{w_0}{R^2} - \frac{\pi}{2} p R^2 = 0 \rightarrow \boxed{w_0 = \frac{p R^4}{16D(1+\nu)}}$$

Exact soln:

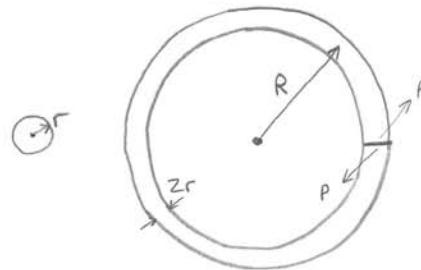
$$w(r) = \frac{pR^2}{64D} \left[ \left( \frac{r}{R} \right)^4 - 2 \left( \frac{r}{R} \right)^2 \frac{3+\nu}{1+\nu} + \frac{5+\nu}{1+\nu} \right] \quad (\text{eqn. 7.28}) \quad (6.11)$$

$$w_0 = w(r=0) = \frac{pR^4}{64D} \left( \frac{5+\nu}{1+\nu} \right) \quad (6.12)$$

$$\frac{w_{0,\text{approx.}}}{w_{0,\text{exact}}} = \frac{\left( \frac{pR^4}{16D(1+\nu)} \right)}{\left( \frac{pR^4(5+\nu)}{64D(1+\nu)} \right)} = \frac{64}{16(5+\nu)} = \underbrace{\frac{4}{5.3}}_{\nu=0.3} \simeq [0.75] \quad (6.13)$$

### Example 3

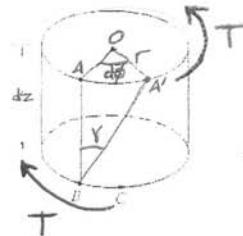
Find the out-of-plane force required to open a keyring.



Compare to the required in-plane force for the same opening.

This is a combined *bending-torsion* problem.

### Introduction to torsion



— Torque,  $T$ , causes rotation  $d\Phi$

$$\alpha \stackrel{\text{def}}{=} \frac{d\Phi}{dz} \quad (\text{like } \kappa = \frac{d\theta}{dx}) \quad (6.14)$$

Shear modulus,

$$G = \frac{E}{2(1 + \nu)} \quad (6.15)$$

Polar moment of inertia,

$$J = I_p \stackrel{\text{def}}{=} \int_A r^2 dA \quad (6.16)$$

For a solid circle,  $J = \frac{\pi r^4}{2}$

$$T = GJ\alpha \quad (\text{like bending, } M = EI\kappa) \quad (6.17)$$

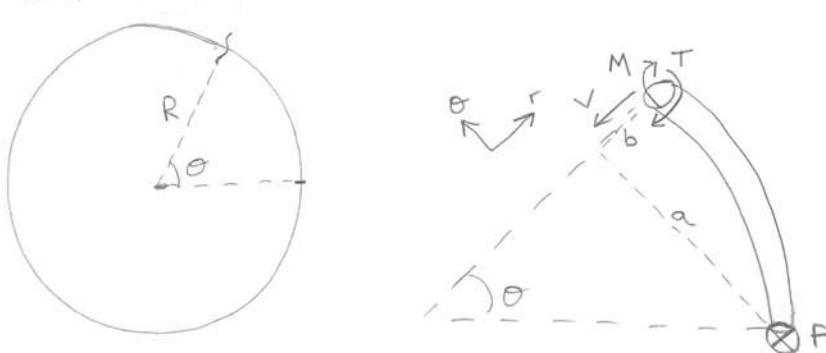
Strain energy,

$$U = \int_L \frac{1}{2} T \alpha dz \quad (\text{like } U = \int_L \frac{1}{2} M \kappa dx) \quad (6.18)$$

$$\alpha = \frac{T}{GJ} \Rightarrow U = \int_L \frac{T^2}{2GJ} dz \quad (6.19)$$


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In our keyring problem:



$$a = R \sin \theta \\ b = R(1 - \cos \theta)$$

$$M_\theta = T = Pb = PR(1 - \cos \theta) \\ M_r = M_b = Pa = PR \sin \theta \quad (6.20)$$

$$U = \int_L \frac{T^2}{2GJ} ds + \int_L \frac{M_b^2}{2EI} ds \quad (ds = Rd\theta) \\ = \int_0^{2\pi} \left( \frac{T^2}{2GJ} + \frac{M_b^2}{2EI} \right) Rd\theta \\ = \frac{P^2 R^3}{2} \int_0^{2\pi} \left[ \frac{(1 - \cos \theta)^2}{GJ} + \frac{\sin^2 \theta}{EI} \right] d\theta \\ = \frac{P^2 R^3}{2} \int_0^{2\pi} \left( \frac{1 - 2 \cos \theta + \cos^2 \theta}{GJ} + \frac{\sin^2 \theta}{EI} \right) d\theta \quad (6.21) \\ = \frac{P^2 R^3}{2} \left( \frac{2\pi}{GJ} + \frac{\pi}{GJ} + \frac{\pi}{EI} \right) = \frac{\pi P^2 R^3}{2} \left( \underbrace{\frac{3}{GJ}}_{\text{Torsion}} + \underbrace{\frac{1}{EI}}_{\text{Bending}} \right)$$

Which contribution is larger?

$$G = \frac{E}{2(1+\nu)} = \frac{E}{2.6} \quad (6.22)$$

$$J = \frac{\pi r^4}{2}, \quad I = \frac{\pi r^4}{4} \quad \rightarrow \quad J = 2I \quad (6.23)$$

So  $\frac{3}{GJ} = \frac{3(2.6)}{E(2I)} \simeq \frac{4}{EI}$  ⇒ torsion is ~4x bending

CAstigliano:

$$w_0 = \frac{\partial U}{\partial P} = \pi PR^3 \left[ \frac{3(2.6)}{2EI} + \frac{1}{EI} \right] \quad (6.24)$$

$$\rightarrow \boxed{P = \frac{EIw_0}{4.9\pi R^3}} \quad (6.25)$$

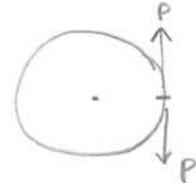

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In-plane force:

Bending only:

$$M_b = PR(1 - \cos \theta)$$

$$\begin{aligned} U &= \int_0^{2\pi} \frac{M_b^2}{2EI} R d\theta \\ &= \frac{P^2 R^3}{2EI} \int_0^{2\pi} (1 - 2\cos \theta + \cos^2 \theta) d\theta = \frac{P^2 R^3}{2EI} (2\pi + \pi) = \frac{3\pi P^2 R^3}{2EI} \end{aligned}$$



$$w_0 = \frac{\partial U}{\partial P} = \frac{3\pi PR^3}{EI} \quad (6.26)$$

$$\rightarrow \boxed{P = \frac{EIw_0}{3\pi R^3}} \quad (6.27)$$

Compare:

$$\frac{P_{\text{out-of-plane}}}{P_{\text{in-plane}}} = \frac{\left(\frac{EIw_o}{4.9\pi R^3}\right)}{\left(\frac{EIw_o}{3\pi R^3}\right)} = \frac{3}{4.9} \simeq \boxed{0.6} \quad (6.28)$$

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