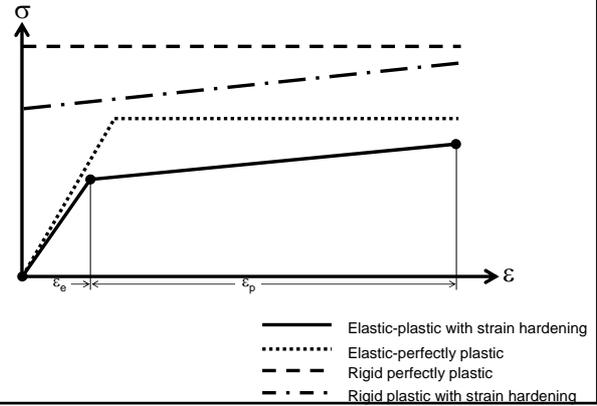


DEFORMING

Stress strain behavior of ductile materials



Topics for today's lecture

Deformation processes

- Deforming process characteristics
- Deforming physics
- Common deforming processes
- DFM

Process characteristics

Material/continuum changes during processing

- Machining = Local, concentrated
- Deforming = Over large volume

Force

- Machining: ~10s - 100s of lbs
- Stamping: ~10s - 100s of tons

Materials - Virtually all ductile materials

Shapes - Limited by strain/flow

Size - Limited by force/equipment

Advantages and disadvantages

Advantages

- Parallel process: rapid bulk formation
- Overall material properties improved

Disadvantages

- Cost of equipment and dies
- Limited flexibility in shapes and sizes (i.e. compared to machining)
- Accuracy
- Repeatability

Important physics

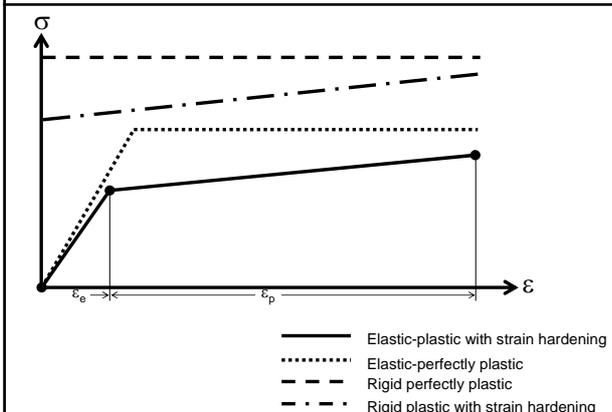
Stress/strain

- Affect CQFR
- Affect deforming force -> equipment & energy requirements

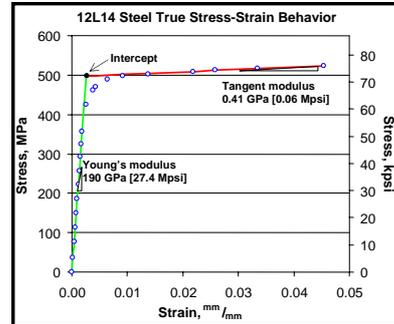
Friction

- Affect on deforming force -> equipment & energy requirements
- Why lubrication is needed and can help
- Friction is not repeatable... quality....

Stress strain behavior of ductile materials

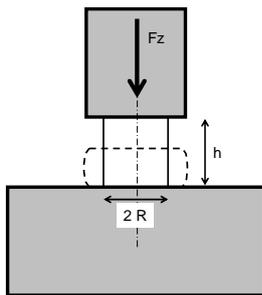


Example: 12L14 Steel in Duratec



Forging force and friction

Axisymmetric upsetting



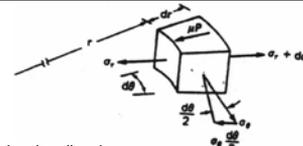
Purpose

- Find $F_z(\mu)$
- Sensitivity

Assumptions:

- Tresca flow
- Constant friction coefficient
- Plastic deformation

Forging force and friction



Eqxn: A – Equilibrium in r direction

$$\Sigma dF_r = 0 = \underbrace{dF_{\text{inner arc}}}_{d\sigma_r \cdot h \cdot r \cdot d\theta} - \underbrace{dF_{\text{friction top \& bottom}}}_{2 \cdot \mu \cdot p \cdot r \cdot d\theta} - \underbrace{dF_{\text{hoop}}}_{2 \cdot \sigma_\theta \cdot h \cdot dr} + \underbrace{dF_{\text{outer arc}}}_{(\sigma_r + d\sigma_r) \cdot (r + dr) \cdot h \cdot d\theta}$$

$$\frac{d\sigma_r}{dr} = \frac{2 \cdot \mu \cdot p}{h} = -\frac{2 \cdot \mu \cdot \sigma_r}{h}$$

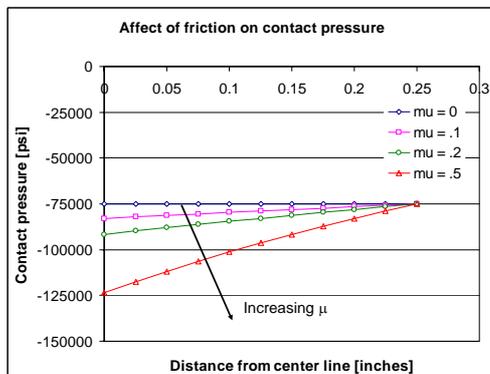
Eqxn: B - Tresca Yield Criterion

$$\sigma_r - \sigma_z = Y$$

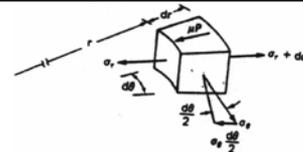
$$\sigma_z = -Y \cdot \exp\left[\frac{2\mu}{h}(R-r)\right]$$

Forging force and friction

Y=75000 psi
h = 1/2 inch



Forging force and friction cont.



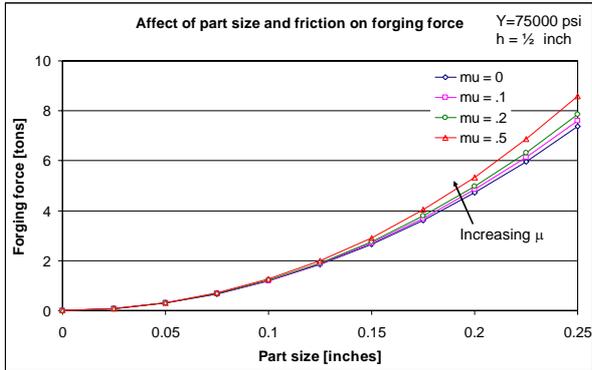
$$F_z = \int_0^R \sigma_z \cdot 2 \cdot \pi \cdot r \cdot dr = (\pi \cdot R^2) \cdot \frac{1}{2} \cdot \left(\frac{h}{\mu \cdot R}\right)^2 \cdot Y \cdot \left[\exp\left(\frac{2 \cdot \mu \cdot R}{h}\right) - \left(\frac{2 \cdot \mu \cdot R}{h}\right) - 1 \right]$$

Now use Taylor's series expansion (3 terms) to approximate the exponential function

Expand about 0, makes this approximation valid for small values of $2\mu R/h$

$$|F_z| = (\pi \cdot R^2) \cdot Y \cdot \left[1 + \left(\frac{2}{3} \cdot \frac{\mu \cdot R}{h}\right) \right]$$

Forging force and friction



Common processes

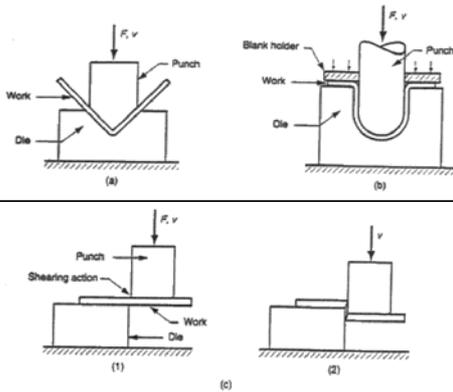
Sheet metal

Forging

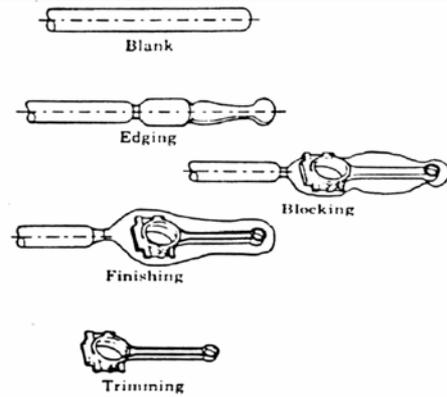
Extrusion

Rolling

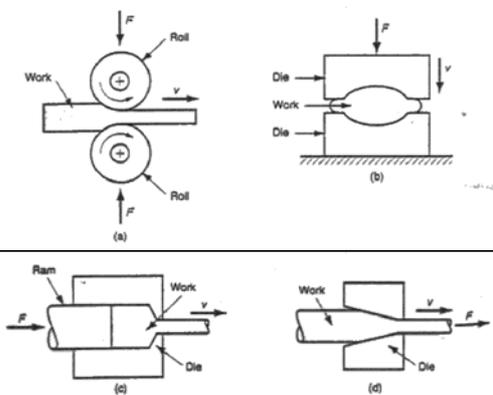
Bending and shearing



Forging



Rolling and extrusion



Affect of grain size

Properties affected by grain size

- Strength
- Hardness
- Ductility
- For example (Ferrite)

$$\sigma_y = \sigma_0 + \frac{k_y}{\sqrt{d_{\text{grain}}}}$$

We desire smaller grains for better properties

Recrystallization

Recrystallization and Grain Growth in Brass

Figure 7.21 Callister



Cold-worked (33% CW)



3s at 580 C: initial recrystallization



4s at 580 C: partial replacement



8s at 580 C: complete recrystallization



15 min at 580 C: grain growth



10 min at 700 C: grain growth

<http://www.mmat.ubc.ca/other/courses/apsc278/lecture11.pdf>

DFM for deforming processes

Parting line and flash

Draft angle

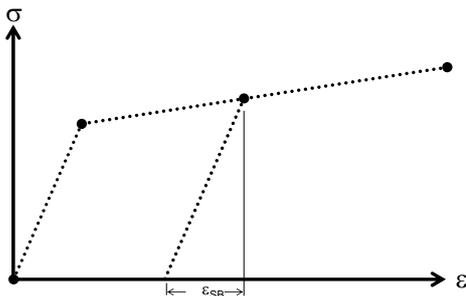
Radii

Lubrication

Mechanics of spring back

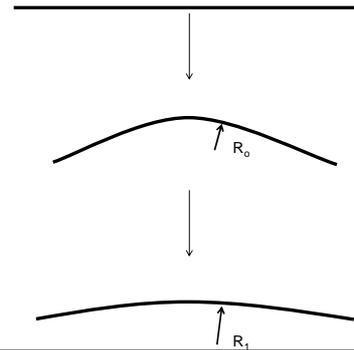
Q: Why do we see spring back?

A: Elastic recover of material



Example: Elastic spring back

Example: Bending wire



$$R_o < R_f \Rightarrow \frac{1}{R_o} > \frac{1}{R_f}$$

Quantifying elastic spring back

Elastic recovery of material leads to spring back

○ Y = Yield stress E = Young's Modulus t = thickness

$$\circ \frac{R_f}{R_o} = 4 \left(\frac{R_o Y}{t E} \right)^3 - 3 \left(\frac{R_o Y}{t E} \right) + 1 \longrightarrow \frac{1}{R_f} - \frac{1}{R_o} = \frac{3}{t} \left(\frac{Y}{E} \right) - \frac{4 R_o^2}{t^3} \left(\frac{Y}{E} \right)^3$$

○ With increase in R_o/t or Y OR decrease in E spring back increases

