

Figure 1: Smallest- $|\lambda|$ eigenfunctions of $\hat{A} = \frac{d}{dx} [c(x)\frac{d}{dx}]$ for $c(x) = e^{3x}$.

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dx = L / (M+1)
x = dx*0.5:dx:L # sequence of x values from 0.5*dx to <= L in steps of dx
c(x) = exp(3x)
C = diagm(c(x))
A = -D' * C * D / dx^2

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You can now get the eigenvalues and eigenvectors by λ , $U = \text{eig}(A)$, where λ is an array of eigenvalues and U is a matrix whose columns are the corresponding eigenvectors (notice that all the λ are < 0 since A is negative-definite).

- (i) The plot is shown in Figure 1. The eigenfunctions look vaguely “sine-like”—they have the same number of oscillations as $\sin(n\pi x/L)$ for $n = 1, 2, 3, 4$ —but are “squeezed” to the left-hand side.
- (ii) We find that the dot product is $\approx 4.3 \times 10^{-16}$, which is zero up to roundoff errors (your exact value may differ, but should be of the same order of magnitude).
- (iii) In the posted IJulia notebook for the solutions, we show a plot of $|\lambda_{2M} - \lambda_M|$ as a function of M on a log–log scale, and verify that it indeed decreases $\sim 1/M^2$. You can also just look at the numbers instead of plotting, and we find that this difference decreases by a factor of ≈ 3.95 from $M = 100$ to $M = 200$ and by a factor of ≈ 3.98 from $M = 200$ to $M = 400$, almost exactly the expected factor of 4. (For fun, in the solutions I went to $M = 1600$, but you only needed to go to $M = 800$.)
- (d) In general, the eigenfunctions have the same number of nodes (sign oscillations) as $\sin(n\pi x/L)$, but the oscillations are pushed towards the region of high $c(x)$. This is even more dramatic if we increase the $c(x)$ contrast. In Figure xxx, we show two examples. First, $c(x) = e^{20x}$, in which all of the functions are squished to the left where c is small. Second $c(x) = 1$ for $x < 0.3$ and 100 otherwise—in this case, the oscillations are at the left 1/3 where c is small, but the function is not zero in the right 2/3. Instead, the function is nearly constant where c is large. The reason for this has to do with the continuity of u : it is easy to see from the operator that cu' must be continuous for $(cu)'$ to exist, and hence the slope u' must decrease by a factor of

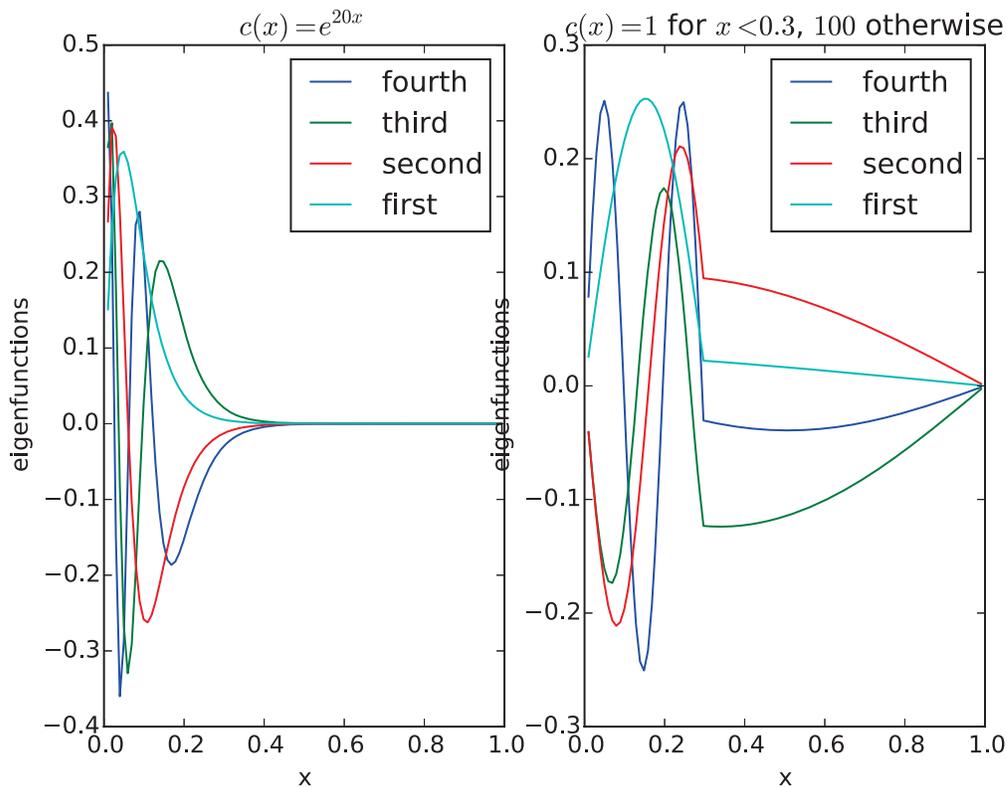


Figure 2: First four eigenfunctions of $\hat{A}u = (cu)'$ for two different choices of $c(x)$.

100 for $x > 0.3$, leading to a u that is nearly constant. (We will explore some of these issues further later in the semester.)

Problem 3: (5+5+5+5+5+5 points)

- (a) The heat capacity equation tells us that $\frac{dT_n}{dt} = \frac{1}{c\rho a\Delta x} \frac{dQ_n}{dt}$, where dQ_n/dt is the rate of change of the heat in the n -th piece. The thermal conductivity equation tells us that dQ_n/dt , in turn, is equal to the sum of the rates q at which heat flows from $n+1$ and $n-1$ into n :

$$\frac{dT_n}{dt} = \frac{1}{c\rho a\Delta x} \frac{dQ_n}{dt} = \frac{1}{c\rho a\Delta x} \frac{\kappa a}{\Delta x} [(T_{n+1} - T_n) + (T_{n-1} - T_n)] = \alpha(T_{n+1} - T_n) + \alpha(T_{n-1} - T_n)$$

where $\alpha = \frac{\kappa}{c\rho(\Delta x)^2}$. The only difference for T_1 and T_N is that they have no heat flow $n-1$ and $n+1$, respectively, since the ends are insulated: $\frac{dT_1}{dt} = \alpha(T_2 - T_1)$ and $\frac{dT_N}{dt} = \alpha(T_{N-1} - T_N)$.

- (b) We can obtain A in two ways. First, we can simply look directly at our equations above, which give $\frac{dT_n}{dt} = \alpha(T_{n+1} - 2T_n + T_{n-1})$ for every n except T_1 and T_N , and read off the

for $n = 1, \dots, N$, where we let $T'_{0.5} = T'_{N+0.5} = 0$ ($D\mathbf{T}'$ using the D from above). This gives $T''_1 = \frac{T'_{1.5} - 0}{\Delta x} = \frac{T_2 - T_1}{\Delta x^2}$, $T''_N = \frac{0 - T'_{N-0.5}}{\Delta x} = \frac{-T_N + T_{N-1}}{\Delta x^2}$ at the endpoints, and $T''_n = \frac{(T_{n+1} - T_n) - (T_n - T_{n-1})}{\Delta x^2} = \frac{T_{n+1} - 2T_n + T_{n-1}}{\Delta x^2}$ for $1 < n < N$, which are precisely the rows of our A matrix above.

- (e) If $\kappa(x)$, then we get a different κ and α factor for each $T_{n+1} - T_n$ difference:

$$\frac{dT_n}{dt} = \alpha_{n+1/2}(T_{n+1} - T_n) + \alpha_{n-1/2}(T_{n-1} - T_n),$$

where $\alpha_{n+1/2} = \frac{\kappa_{n+1/2}}{c\rho(\Delta x)^2}$ and $\kappa_{n+1/2} = \kappa([n + 1/2]\Delta x)$. In the $N \rightarrow \infty$ limit, this gives

$\hat{A} = \frac{1}{c\rho} \frac{\partial}{\partial x} \kappa \frac{\partial}{\partial x}$: we differentiated, multiplied by κ , differentiated again, and then divided by $c\rho$. (You weren't asked to handle the case where $c\rho$ is not a constant, so it's okay if you commuted $c\rho$ with the derivatives.)

- (f) If we discretize to $T_{m,n} = T(m\Delta x, n\Delta y)$, the steps are basically the same except that we have to consider the heat flow in both the x and y directions, and hence we have to take differences in both x and y . In particular, suppose the thickness of the block is h . In this case, heat will flow from $T_{m,n}$ to $T_{m+1,n}$ at a rate $\frac{\kappa h \Delta y}{\Delta x} (T_{m,n} - T_{m+1,n})$ where $h\Delta y$ is the area of the interface between the two blocks. Then, to convert into a rate of temperature change, we will divide by $c\rho h \Delta x \Delta y$, where $h\Delta x \Delta y$ is the volume of the block. Putting this all together, we obtain:

$$\frac{dT_{m,n}}{dt} = \frac{\kappa}{c\rho} \left[\frac{T_{m+1,n} - 2T_{m,n} + T_{m-1,n}}{\Delta x^2} + \frac{T_{m,n+1} - 2T_{m,n} + T_{m,n-1}}{\Delta y^2} \right],$$

where the thing in $[\dots]$ is precisely the five-point stencil approximation for ∇^2 from class. Hence, we obtain

$$\hat{A} = \frac{1}{c\rho} \nabla \cdot \kappa \nabla,$$

where for fun I have put the κ in the middle, which is the right place if κ is not a constant (you were not required to do this).

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