

# Plant Stems with Radial Density Gradients



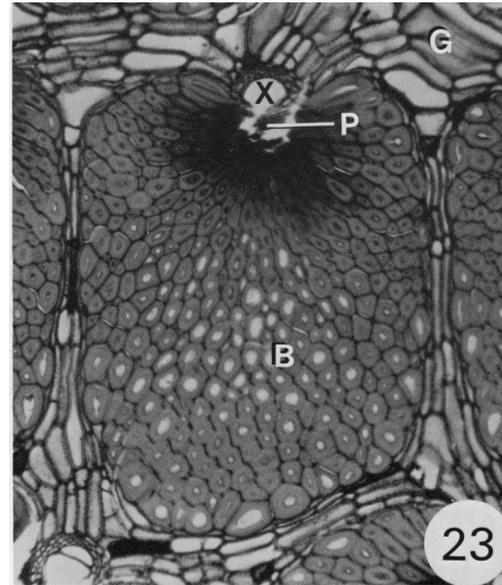
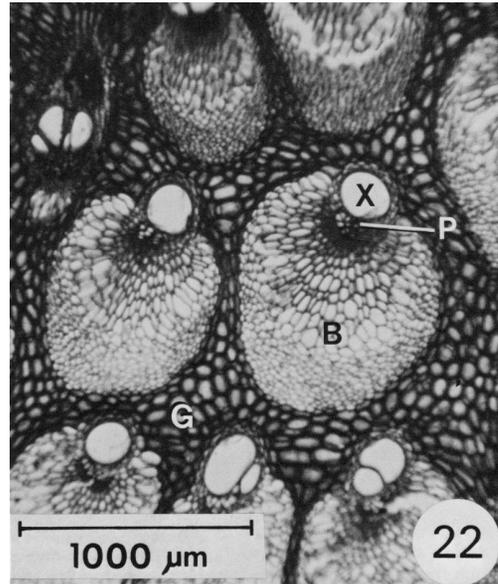
Coconut Palm

<http://en.wikipedia.org/wiki/>  
Image:Palmtree\_Curacao.jpg

# Palm: Density Gradient

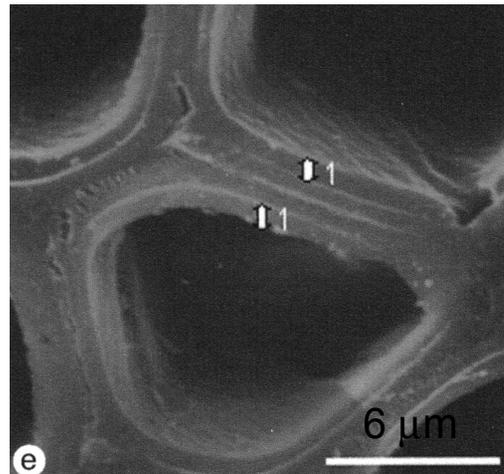
Vascular bundles:  
Honeycomb

Ground tissue  
(Parenchyma):  
Foam

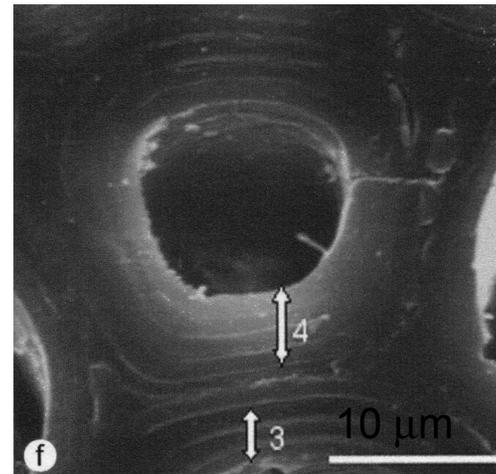


Peripheral  
Stem  
Tissue

Rich, 1987



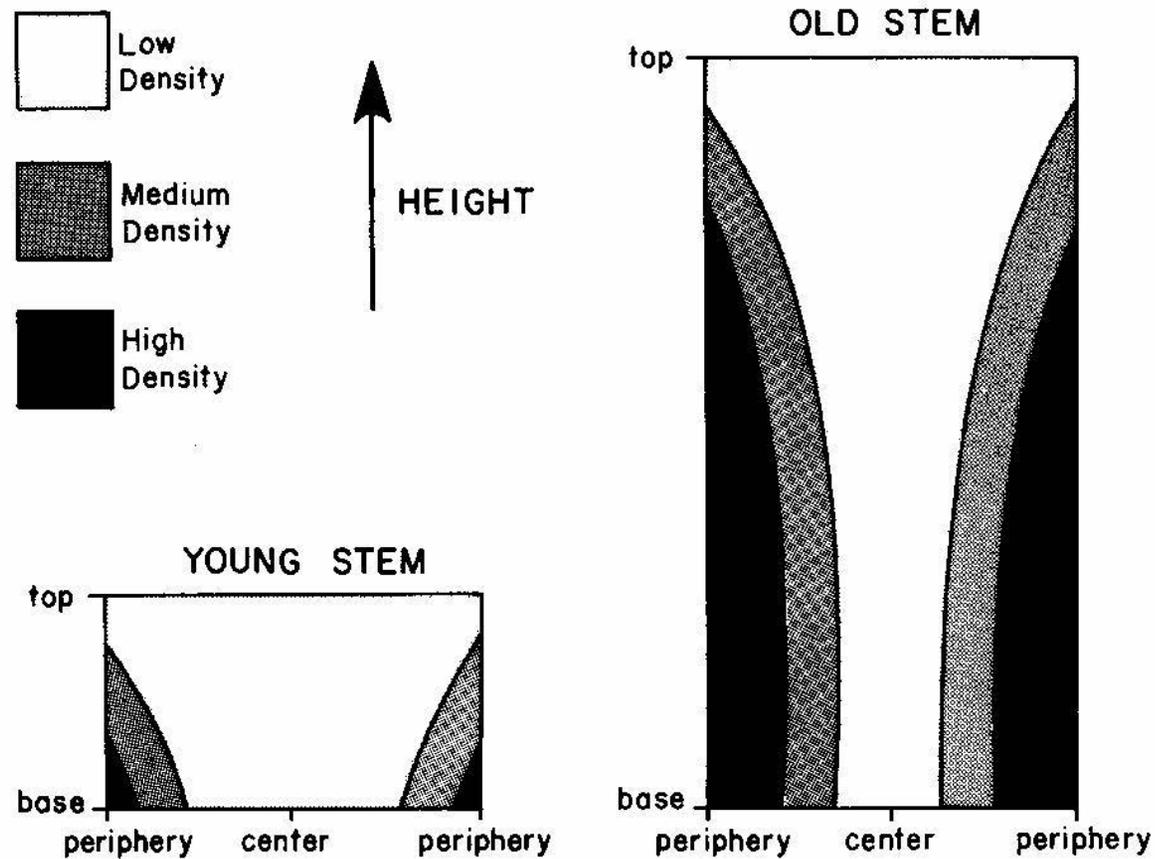
Young



Old

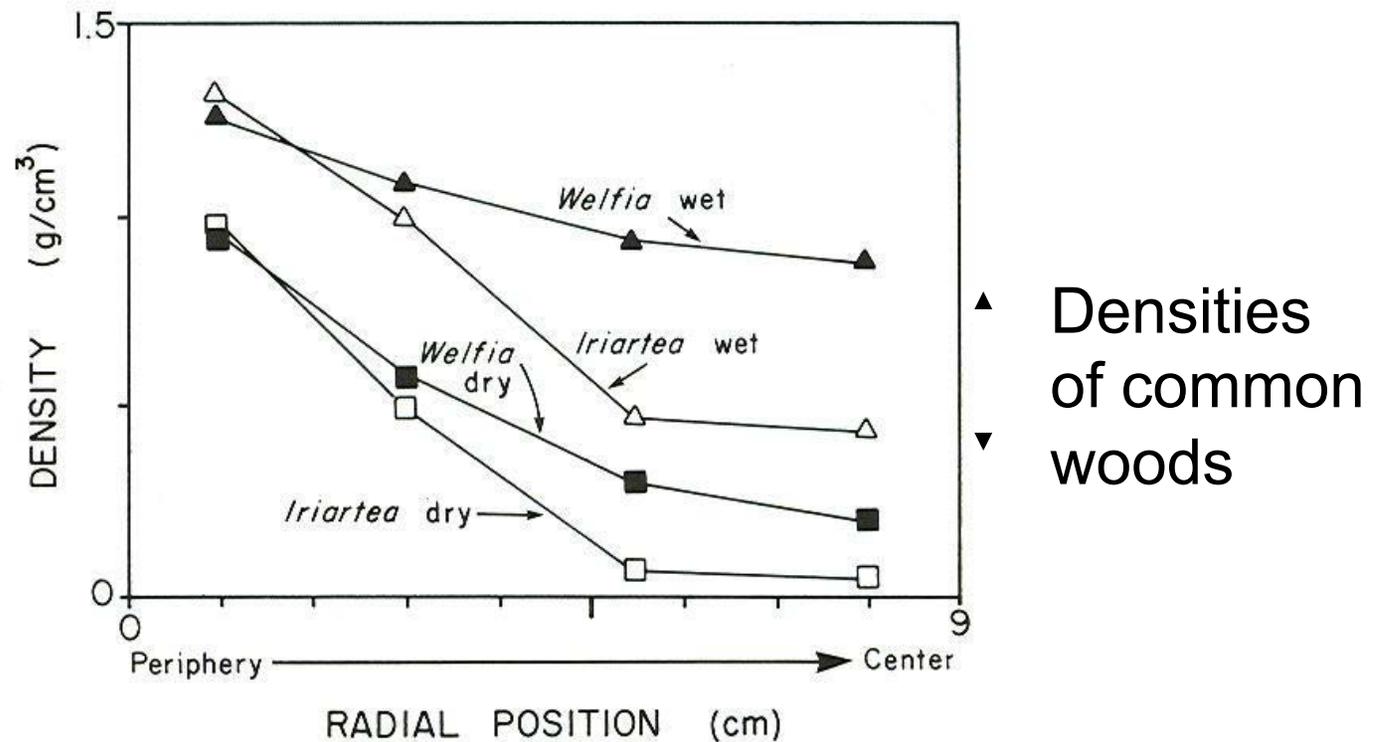
Kuo-Huang  
et al., 2004

# Palm Stem: Density Gradient



Rich, PM (1987) Bot.Gazette 148, 42-50.

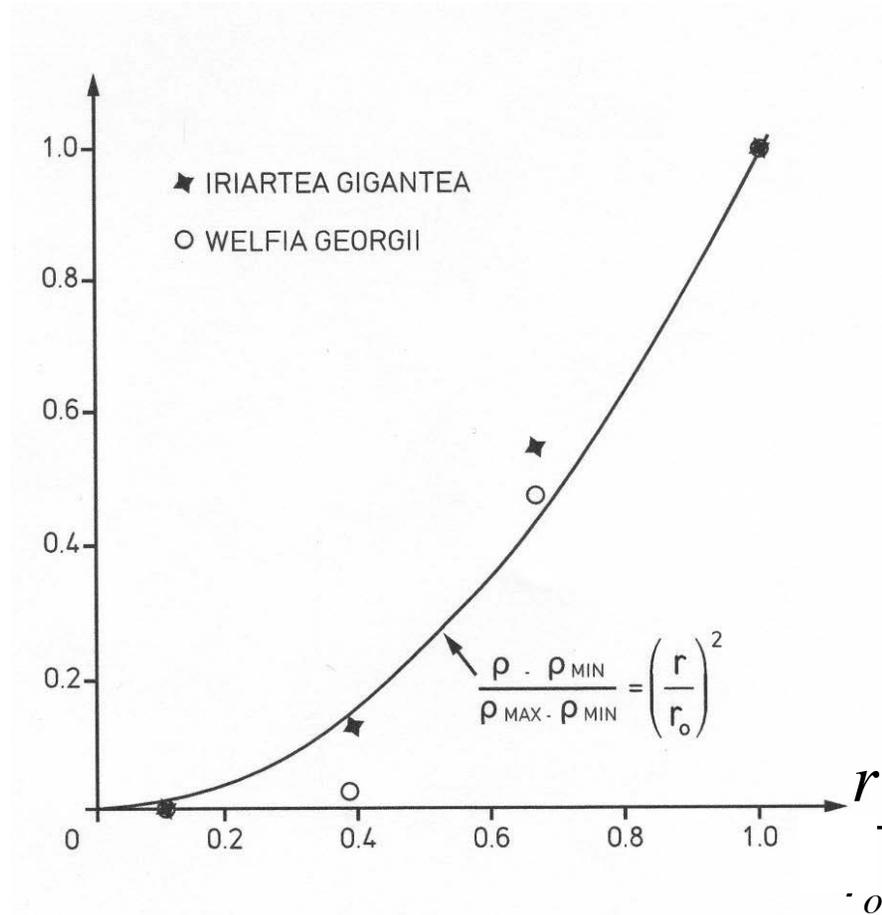
# Palm Stem: Density at Breast Height



A single mature palm has a similar range of density as nearly all species of wood combined

# Palm Stem: Density Gradient

$$\frac{\rho - \rho_{\min}}{\rho_{\max} - \rho_{\min}}$$

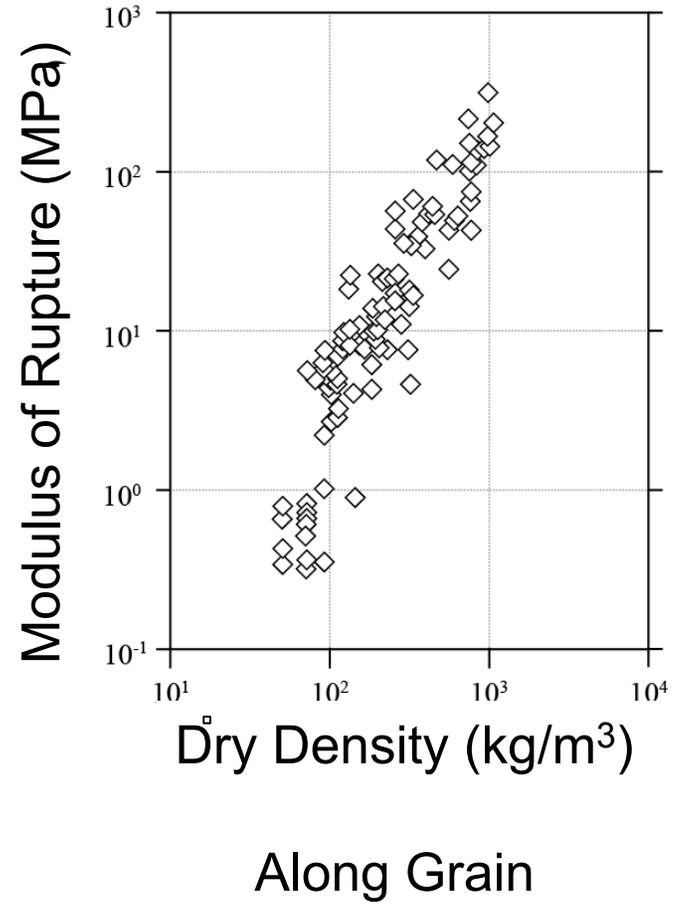
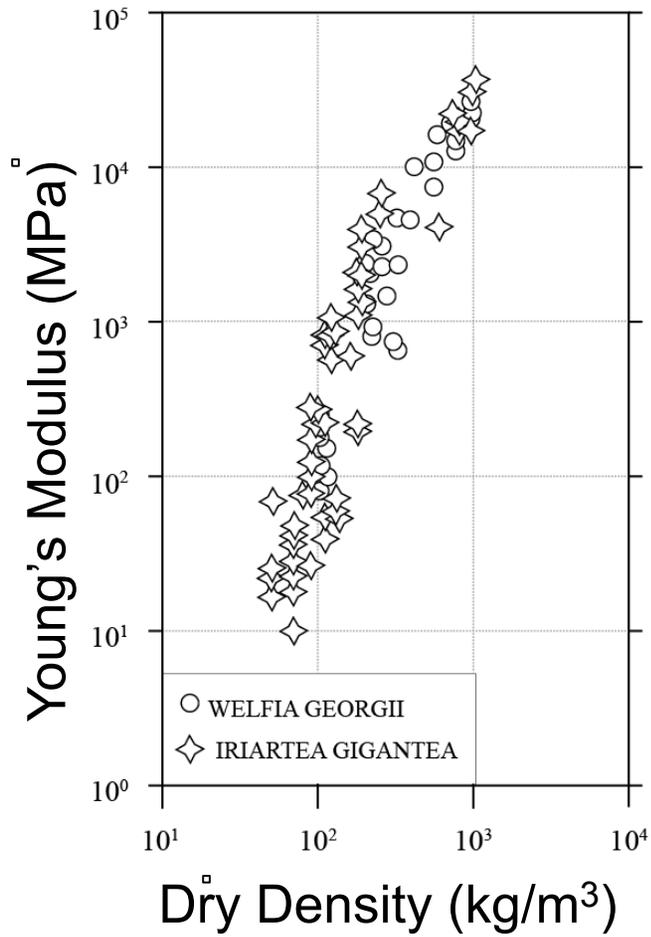


$r_o$  is the outer radius

*Iriartea gigantea:*

$$\rho_{\min} \approx 0$$

$$\frac{\rho^*}{\rho_{\max}} = \left(\frac{r}{r_o}\right)^2$$



*Iriarteia gigantea*

$$E^* = C \left( \frac{\rho^*}{\rho_{\max}} \right)^{2.5}$$

$$\sigma^* = C \left( \frac{\rho^*}{\rho_{\max}} \right)^2$$

Rich, PM (1987) Bot.Gazette 148, 42-50.

# Palm Properties

- Prismatic cells in palm deform axially (like wood loaded along the grain)
- If  $E_s$  was constant, would expect:  $E^* = E_s (\rho^* / \rho_s)$
- But measure:  $E^* = C (\rho^* / \rho_{\max})^{2.5}$
- Similarly with strength

# Palm Properties

- $E_s = 0.1\text{-}3.0$  GPa in low density palm tissue from *Washingtonia robusta* (Rueggeberg et al., 2008)
- Estimate in dense tissue ( $E^* = 30$  GPa;  $\rho^* = 1000$  kg/m<sup>3</sup>)  $E_s = 45$  GPa
- Large variation in  $E_s$  due to additional secondary layers in cell walls of denser tissue and increased alignment of cellulose microfibrils in those layers

# Palm: Mechanical Efficiency

## Bending Stiffness

$$\rho = \left(\frac{r}{r_o}\right)^n \rho_{\max} \quad (EI)_{\text{gradient}} = \frac{C\pi r_o^4}{mn + 4}$$

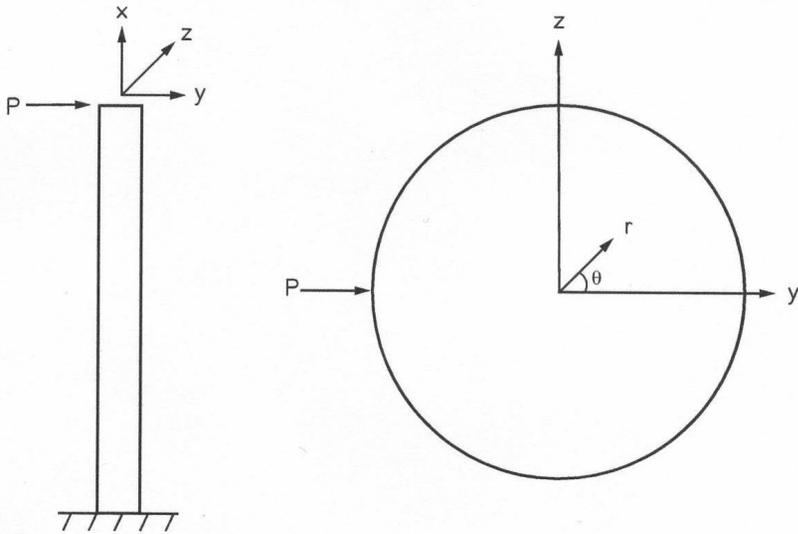
$$E = C \left(\frac{\rho}{\rho_{\max}}\right)^m = C \left(\frac{r}{r_o}\right)^{mn} \quad \frac{(EI)_{\text{gradient}}}{(EI)_{\text{uniform}}} = \frac{4}{mn + 4} \left(\frac{n + 2}{2}\right)^m$$

*Iriarteia gigantea*:  $n = 2$ ,  $m = 2.5$

$$(EI)_{\text{gradient}} / (EI)_{\text{uniform}} = 2.5$$

# Palm: Mechanical Efficiency

## Bending *Stress* Distribution



$$\sigma(y) = E\varepsilon = E\kappa y$$

$$\sigma(r, \theta) = C \left( \frac{r}{r_o} \right)^{mn} \kappa r \cos \theta \propto r^{mn+1}$$

*I. gigantea*:  $n = 2$ ,  $m = 2.5$

$$\sigma \propto r^6$$

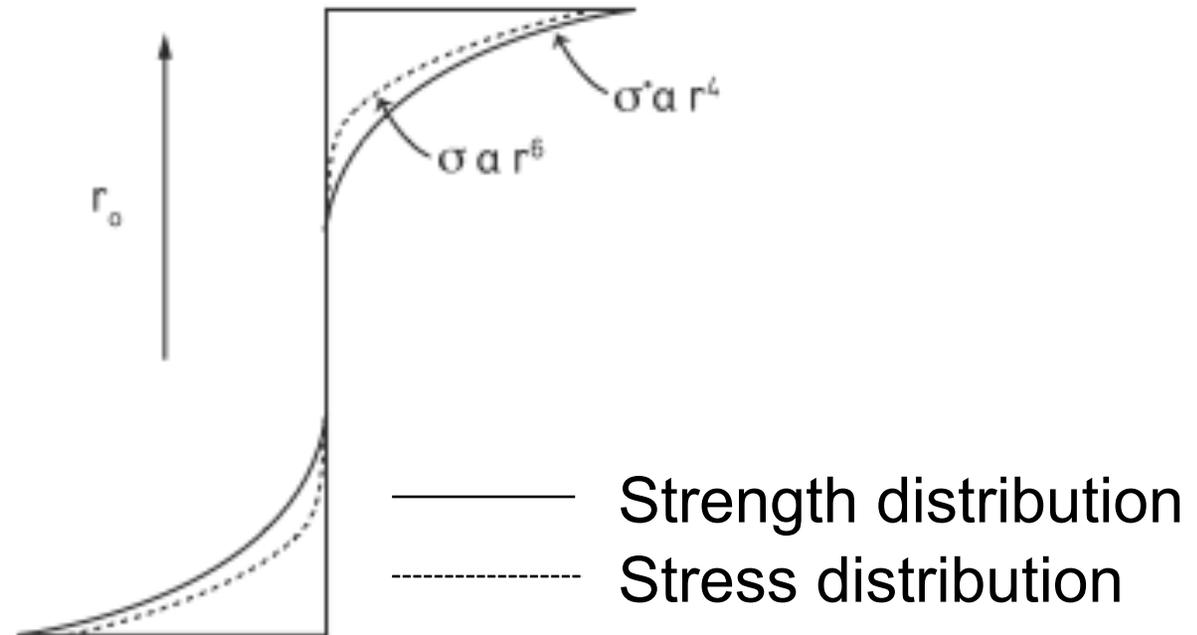
# Palm: Mechanical Efficiency Bending *Strength* Distribution

$$\sigma^* \propto \left( \frac{\rho}{\rho_{\max}} \right)^q \propto \left( \frac{r}{r_o} \right)^{nq}$$

*Iriartea gigantea*:  $n = 2, q = 2$

$$\sigma^* \propto r^4$$

# Palm bending stress, strength



# Figure sources

Sources for all figures in:  
Cellular Materials in Nature and Medicine (2010)

## Circular sections with radial density gradients: Palm Stems

- Palms can grow up to 20-40m - largest stresses from hurricane winds
- Unlike trees, palms do not have a cambium layer at the periphery, with dividing cells to allow increase in diameter as palm grows in height
- Instead, diameter of palm roughly constant as it grows in height
- Increasing stress resisted by cell walls increasing in thickness
- Add additional layers of secondary cell wall
- Produces radial density gradient
  - Density higher at periphery and at base of stem
  - A single stem can have densities from 100-1000 kg/m<sup>3</sup>, nearly spanning the density range of all woods (balsa ~200 kg/m<sup>3</sup> → lignum vitae ~ 1300 kg/m<sup>3</sup>)
- Specimen of palm taken from different radial positions tested in bending (Paul Rich, 1980s)
- Found  $E_{\text{axial}}^* = C' \rho^{*2.46}$
- Might expect  $E_{\text{axial}}^* \propto \rho$  - vascular bundles honeycomb-like

- But additional cell wall layers change  $E_s$ : data  $E_s=0.1-3$  GPa
- Also: lower density palm has more ground tissue (parenchyma) with  $E \propto \rho$  if at high turgor, but  $E \propto \rho^2$  if at low turgor. (bending specimens dry)
- Modulus of rupture  $\sigma^* = C'' \rho^{*2.05}$
- Radial density gradient increases flexural rigidity
- Compare (EI) with density gradient to (EI) of section of same mass+radius but uniform density
- For *Iriarteia gigantea*:

$$\left(\frac{\rho^*}{\rho_{\max}}\right) = \left(\frac{r}{r_0}\right)^n \quad r_0 = \text{outer radius}$$

$$n = 2$$

$$E = C \left(\frac{\rho}{\rho_{\max}}\right)^m = C \left(\frac{r}{r_0}\right)^{mn}$$

$$(EI)_{\text{gradient}} = \int_0^{r_0} = C \left(\frac{\rho}{\rho_{\max}}\right)^m \frac{2\pi r r^2 dr}{2}$$

$$= \int_0^{r_0} C \left(\frac{r}{r_0}\right)^{mn} \pi r^3 dr$$



$$\int r^2 2\pi r dr = J = 2I$$

$$\begin{aligned}
(EI)_{\text{gradient}} &= \frac{C\pi}{r_0^{mn}} \int_0^{r_0} r^{mn+3} dr \\
&= \frac{C\pi}{r_0^{mn}} \frac{r_0^{mn+4}}{mn+4} \\
&= \frac{C\pi r_0^4}{mn+4}
\end{aligned}$$

Equivalent mass,  $r_0$ , uniform density  $\bar{\rho}$ :

$$\frac{\bar{\rho}}{\rho_{\max}} = \frac{1}{\pi r_0^2} \int_0^{r_0} \left(\frac{r}{r_0}\right)^n 2\pi r dr = \frac{1}{\pi r_0^2} \frac{2\pi}{r_0^n} \frac{r_0^{n+2}}{n+2} = \frac{2}{n+2}$$

$$\begin{aligned}
(EI)_{\text{uniform density}} &= C \left(\frac{\bar{\rho}}{\rho_{\max}}\right)^m \frac{\pi r_0^4}{4} \\
&= C \left(\frac{2}{n+2}\right)^m \frac{\pi r_0^4}{4}
\end{aligned}$$

$$\boxed{\frac{(EI)_{\text{gradient}}}{(EI)_{\text{uniform}}} = \frac{C\pi r_0^4}{mn+4} \frac{4}{C\pi r_0^4} \left(\frac{n+2}{2}\right)^m = \frac{4}{mn+4} \left(\frac{n+2}{2}\right)^m}$$

I.gigantea  $m = 2.5$   $n = 2$

$$\boxed{\frac{(EI)_{\text{gradient}}}{(EI)_{\text{uniform}}} = 2.5}$$

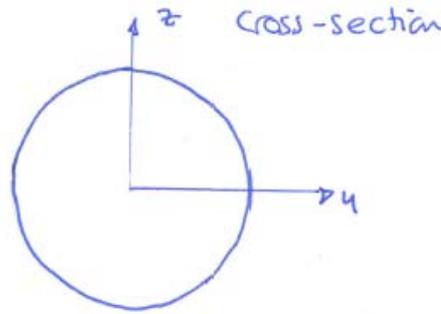
# Stress and Strength distribution

$$\frac{\rho}{\rho_{\max}} = \left(\frac{r}{r_0}\right)^n$$

Stress  $\sigma(y) = E \epsilon = E \mathcal{K} y$

$$= C \left(\frac{\rho}{\rho_{\max}}\right)^m \mathcal{K} y$$

$$= C \left(\frac{r}{r_0}\right)^{mn} \mathcal{K} r$$



$\mathcal{K}$ =curvature at the cross-section  
 $y$ =distance from neutral axis  
 $E = C \left(\frac{\rho}{\rho_{\max}}\right)^m$

$$\sigma(r) \propto r^{mn+1} \quad \text{I. gigantea} \quad m=2.5 \quad n=2 \quad \sigma(r) \propto r^6$$

Strength  $\sigma^*(r) = C' \left(\frac{\rho}{\rho_{\max}}\right)^q = C \left(\frac{r}{r_0}\right)^{nq}$

$$\sigma^* r \propto r^{nq} \quad \text{I. gigantea} \quad q=2 \quad n=2 \quad \sigma^*(r) \propto r^4$$

Figure: if max normal stress at  $r = r_0$  is  $\sigma = \sigma^*$  then bending stress distribution closely follows strength distribution!

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