

1.021, 3.021, 10.333, 22.00 Introduction to Modeling and Simulation
Spring 2011

Part I – Continuum and particle methods

Application to modeling brittle materials

Lecture 7

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Content overview

I. Particle and continuum methods

Lectures 2-13

1. Atoms, molecules, chemistry
2. Continuum modeling approaches and solution approaches
3. Statistical mechanics
4. Molecular dynamics, Monte Carlo
5. Visualization and data analysis
6. Mechanical properties – application: how things fail (and how to prevent it)
7. Multi-scale modeling paradigm
8. Biological systems (simulation in biophysics) – how proteins work and how to model them

II. Quantum mechanical methods

Lectures 14-26

1. It's A Quantum World: The Theory of Quantum Mechanics
2. Quantum Mechanics: Practice Makes Perfect
3. The Many-Body Problem: From Many-Body to Single-Particle
4. Quantum modeling of materials
5. From Atoms to Solids
6. Basic properties of materials
7. Advanced properties of materials
8. What else can we do?

Overview: Material covered so far...

- **Lecture 1: Broad introduction to IM/S**
- **Lecture 2: Introduction to atomistic and continuum modeling** (multi-scale modeling paradigm, difference between continuum and atomistic approach, case study: diffusion)
- **Lecture 3: Basic statistical mechanics – property calculation I** (property calculation: microscopic states vs. macroscopic properties, ensembles, probability density and partition function)
- **Lecture 4: Property calculation II** (Monte Carlo, advanced property calculation, introduction to chemical interactions)
- **Lecture 5: How to model chemical interactions I** (example: movie of copper deformation/dislocations, etc.)
- **Lecture 6: How to model chemical interactions II** (pair potentials, fracture – introduction)
- **Lecture 7: Application – MD simulation of materials failure**

Lecture 7: Application to modeling brittle materials

Outline:

1. Basic deformation mechanism in brittle materials - crack extension
2. Atomistic modeling of fracture
 - 2.1 Physical properties of atomic lattices
 - 2.2 Application
3. Bond order force fields - how to model chemical reactions

Goal of today's lecture:

- Apply our tools to model a particular material phenomena – brittle fracture (**useful for pset #2**)
- Learn basics in fracture of brittle materials
- Learn how to build a model to describe brittle fracture (from scratch)

1. Basic deformation mechanism in brittle materials - crack extension

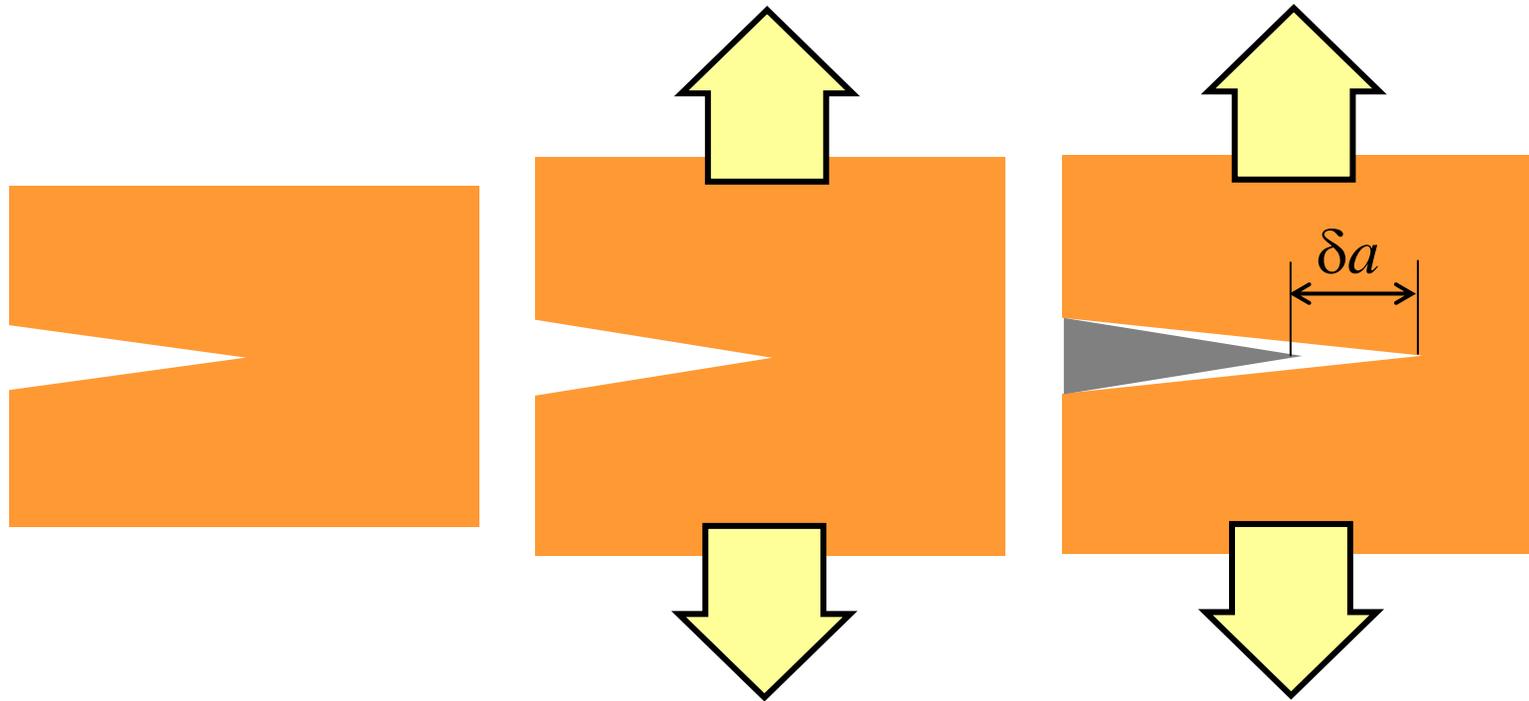
Brittle fracture

- Materials: **glass, silicon, many ceramics, rocks**
- At large loads, rather than accommodating a shape change, materials break

Image courtesy of [quinn.anya](#).
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Basic fracture process: dissipation of elastic energy



Undeformed



Stretching=store elastic energy



Release elastic energy
dissipated into breaking
chemical bonds

Continuum description of fracture

- Fracture is a dissipative process in which elastic energy is dissipated to break bonds (and to heat at large crack speeds)
- Energy to break bonds = surface energy γ_s (energy necessary to create new surface, dimensions: energy/area, Nm/m²)

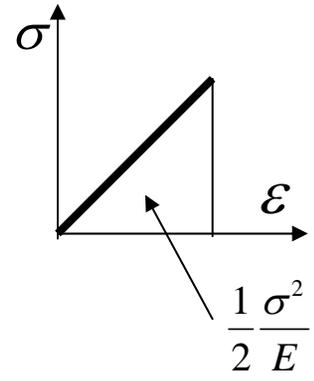
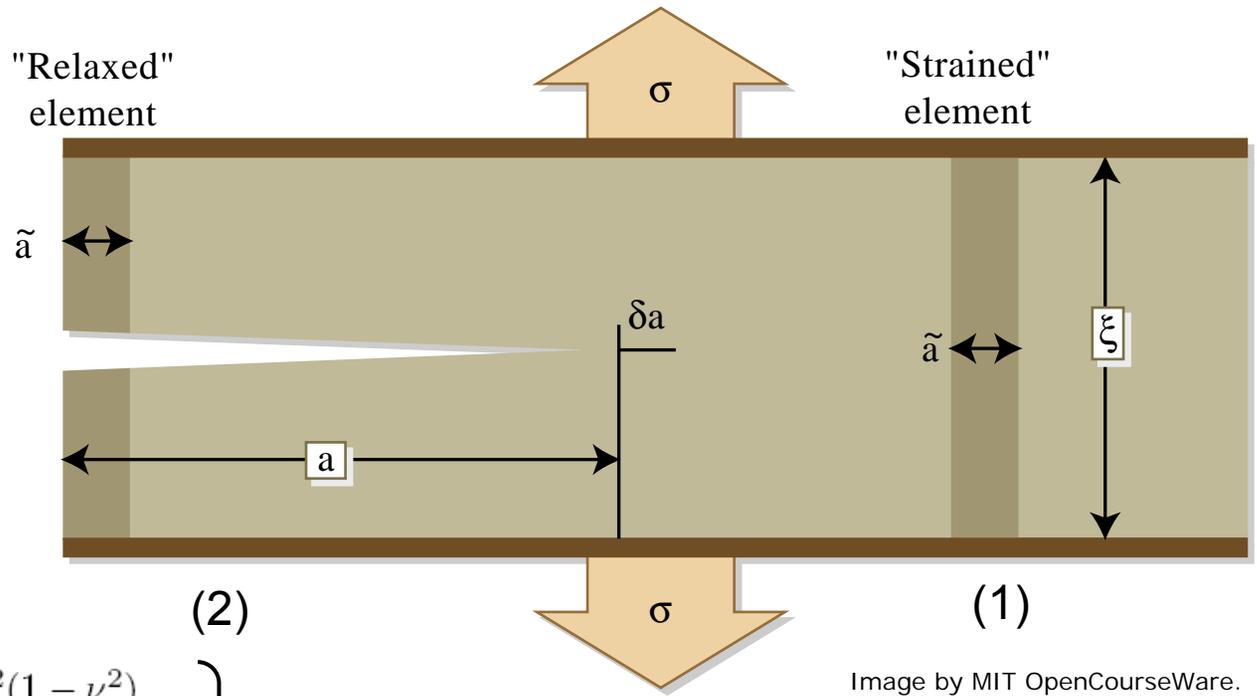


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$$\left. \begin{aligned} W_P^{(1)} &= \frac{\sigma^2(1-\nu^2)}{2E} \xi \tilde{a} B \\ W_P^{(2)} &= 0 \end{aligned} \right\} W_P = W_P^{(1)} - W_P^{(2)} = \underbrace{\frac{1}{2} \frac{\sigma^2}{E} \xi \tilde{a} B}_{\text{change of elastic (potential) energy} = G} - \underbrace{2\gamma_s B \tilde{a}}_{\text{energy to create surfaces}}$$

$$\sigma = \sqrt{\frac{4\gamma_s E}{\xi}}$$

Griffith condition for fracture initiation

- **Energy release rate** G , that is, the elastic energy released per unit crack advance must be equal or larger than the energy necessary to create new surfaces

$$G := \frac{1}{2} \frac{\sigma^2}{E} \xi = 2y_s$$

$$G = 2\gamma_s$$

- Provides **criterion to predict failure initiation**
- Calculation of G can be complex, but straightforward for thin strips as shown above
- Approach to calculate G based on “**stress intensity factor**” (see further literature, e.g. Broberg, Anderson, Freund, Tada)

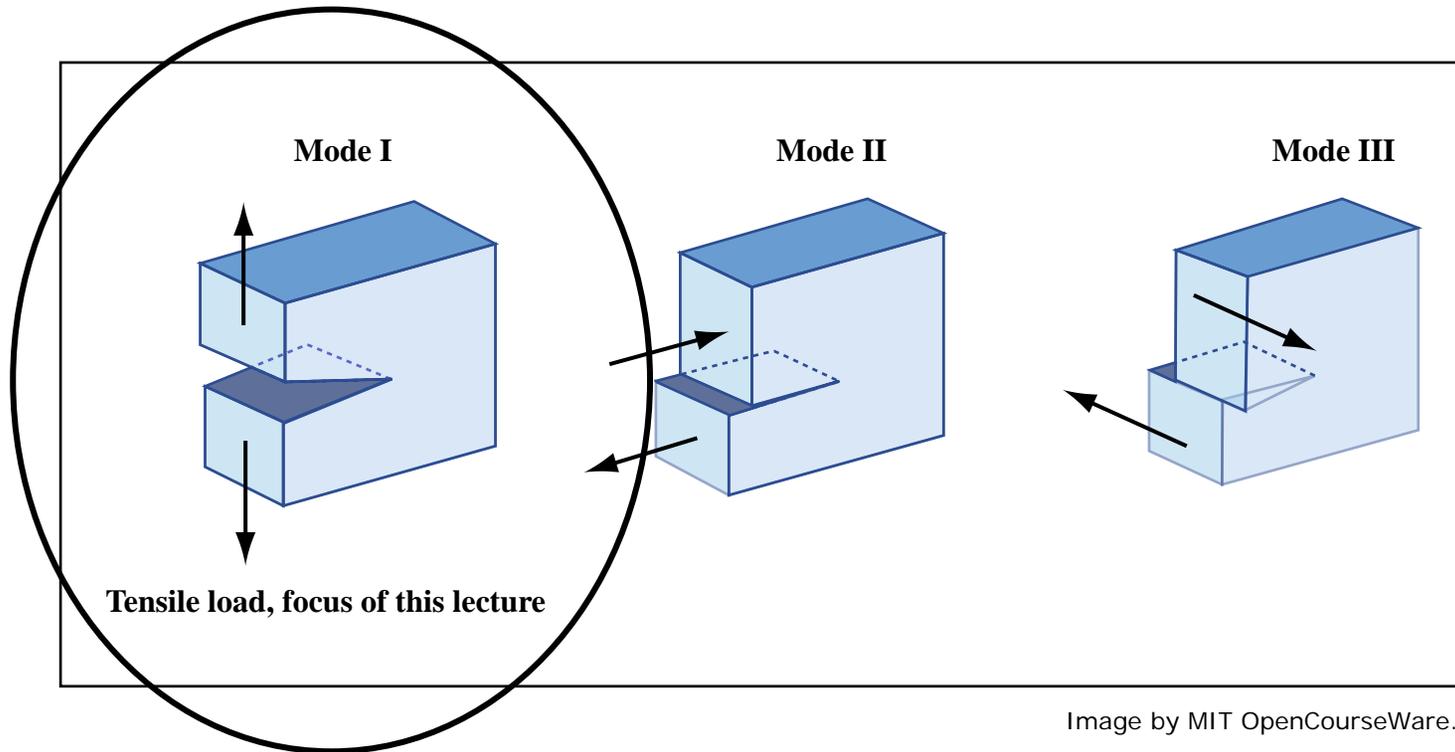
Brittle fracture mechanisms

- Once nucleated, cracks in brittle materials spread rapidly, on the order of sound speeds
- Sound speeds in materials (=wave speeds):
 - Rayleigh-wave speed c_R (speed of surface waves)
 - shear wave speed c_s (speed of shear waves)
 - longitudinal wave speed c_l (speed of longitudinal waves)
- ***Maximum speeds of cracks is given by sound speeds, depending on mode of loading (mode I, II, III)***

Linear elastic continuum theory

Brittle fracture loading conditions

- Commonly consider a single crack in a material geometry, under three types of loading: mode I, mode II and mode III



Limiting speeds of cracks: linear elastic continuum theory

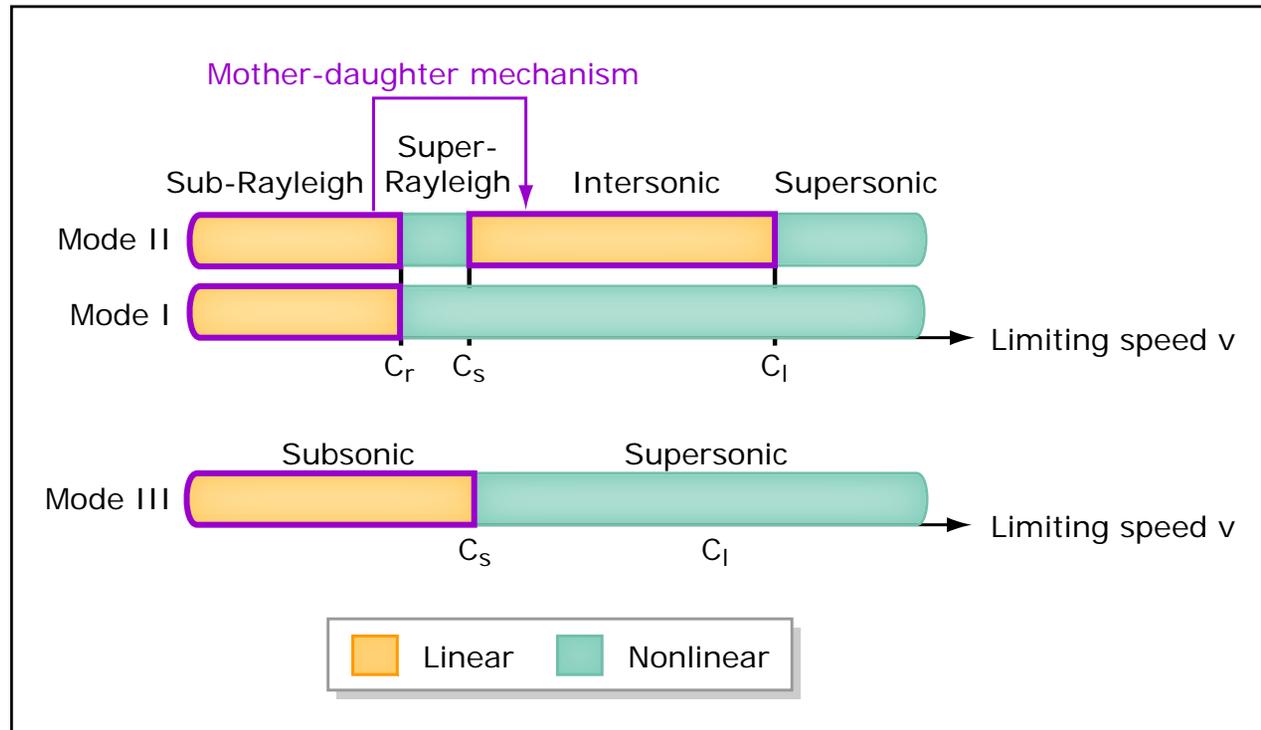


Image by MIT OpenCourseWare.

- Cracks **can not exceed** the limiting speed given by the corresponding wave speeds **unless material behavior is nonlinear**
- Cracks that exceed limiting speed would produce energy (physically impossible - **linear elastic continuum theory**)

Sound speeds in materials: overview

| Material | c_R (in m/s) | c_s (in m/s) | c_l (in m/s) |
|----------|----------------|----------------|----------------|
| Steel | 2,940 | 3,200 | 6,000 |
| Al | 2,850 | 3,100 | 6,300 |
| Glass | 3,030 | 3,300 | 5,800 |
| PMMA | 920 | 1,000 | 2,400 |

Wave speeds are calculated based on elastic properties of material

$$c_l = \sqrt{\frac{3\mu}{\rho}} \quad c_s = \sqrt{\frac{\mu}{\rho}} \quad c_R \approx \beta c_s \quad \beta \approx 0.923$$

$$\mu = \text{shear modulus} \quad E = 8/3\mu \quad \mu = 3/8E$$

Brittle fracture mechanisms: fracture is a multi-scale phenomenon, from nano to macro

Image removed due to copyright restrictions. Fig. 6.2 in Buehler, Markus J. *Atomistic Modeling of Materials Failure*. Springer, 2008.

Physical reason for crack limiting speed

- Physical (mathematical) reason for the limiting speed is that it becomes increasingly difficult to increase the speed of the crack by adding a larger load
- When the crack approaches the limiting speed, the **resistance to fracture diverges to infinity (=dynamic fracture toughness)**

divergence

Driving force
(applied load)

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Please see: Fig. 6.15 in Buehler, Markus J. *Atomistic Modeling of Materials Failure*. Springer, 2008.

$$G = \frac{1}{2} \frac{\sigma^2}{E} \xi = f(y_s, v)$$

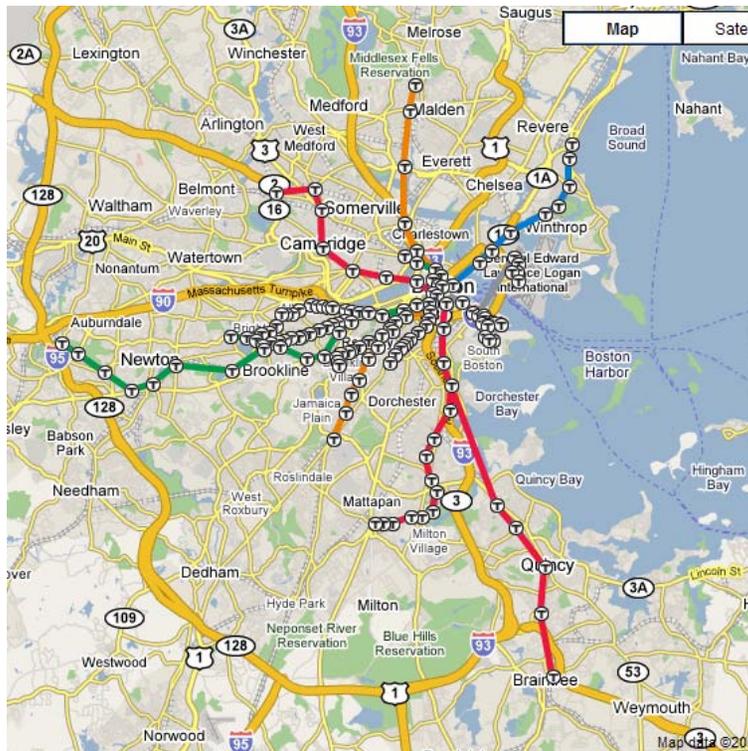
$$G \sim \frac{\sigma^2}{E}$$

2. Atomistic modeling of fracture

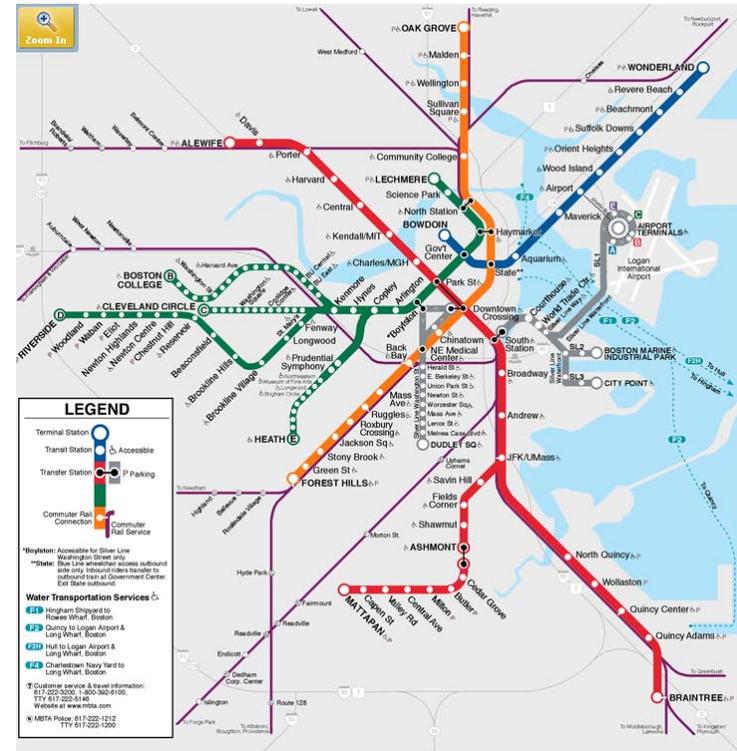
What is a model?

Mike Ashby (Cambridge University):

- *A model is an idealization. Its relationship to the real problem is like that of the map of the London tube trains to the real tube systems: a gross simplification, but one that captures certain essentials.*



“Physical situation”



“Model”

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A “simple” atomistic model: geometry

$$\phi = \frac{1}{2}k_0(r - r_0)^2$$

elasticity (store energy)

stable configuration of pair potential

2D triangular (hexagonal) lattice

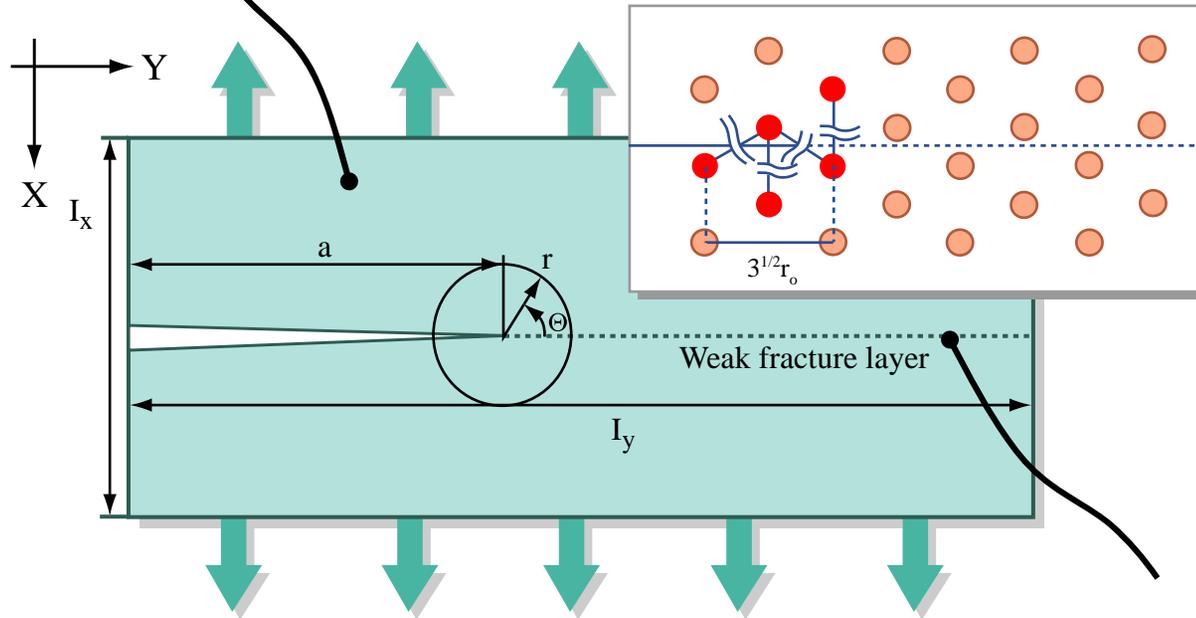


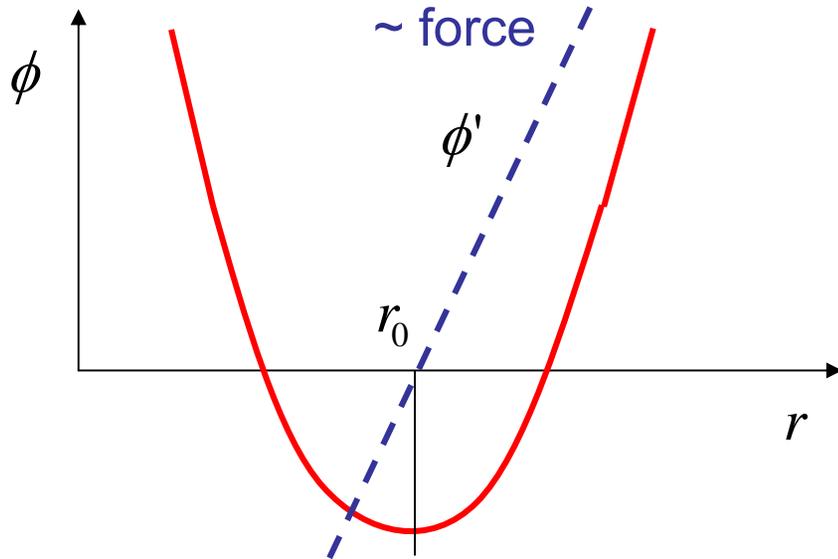
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Pair potential to describe atomic interactions
Confine crack to a 1D path (weak fracture layer):
Define a pair potential
whose bonds never break (bulk) and a potential
whose bonds break

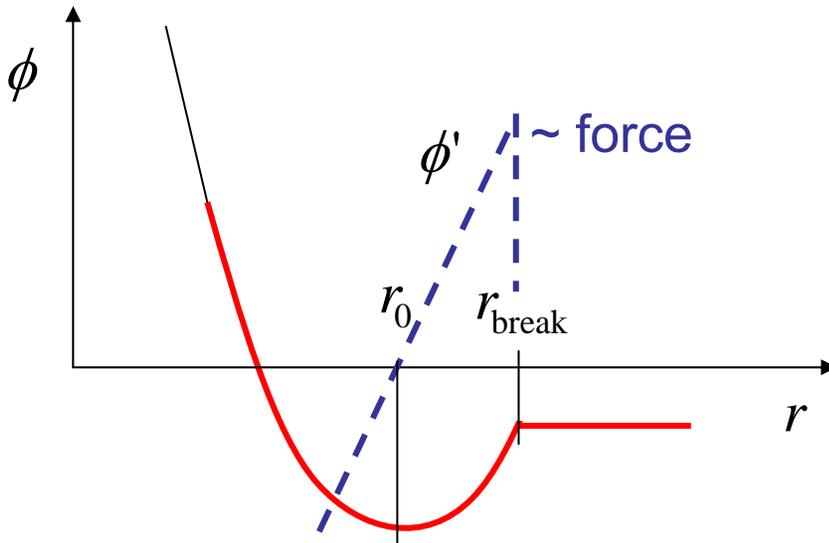
$$\phi = \begin{cases} \frac{1}{2}k_0(r - r_0)^2 & r < r_{\text{break}} \\ \frac{1}{2}k_0(r_{\text{break}} - r_0)^2 & r \geq r_{\text{break}} \end{cases}$$

bond can break

Harmonic and harmonic bond snapping potential



$$\phi = \frac{1}{2}k_0(r - r_0)^2$$



$$\phi = \begin{cases} \frac{1}{2}k_0(r - r_0)^2 & r < r_{\text{break}} \\ \frac{1}{2}k_0(r_{\text{break}} - r_0)^2 & r \geq r_{\text{break}} \end{cases}$$

2.1 Physical properties of atomic lattices

How to calculate elastic properties and fracture surface energy – parameters to link with continuum theory of fracture

free energy density (energy per unit volume)

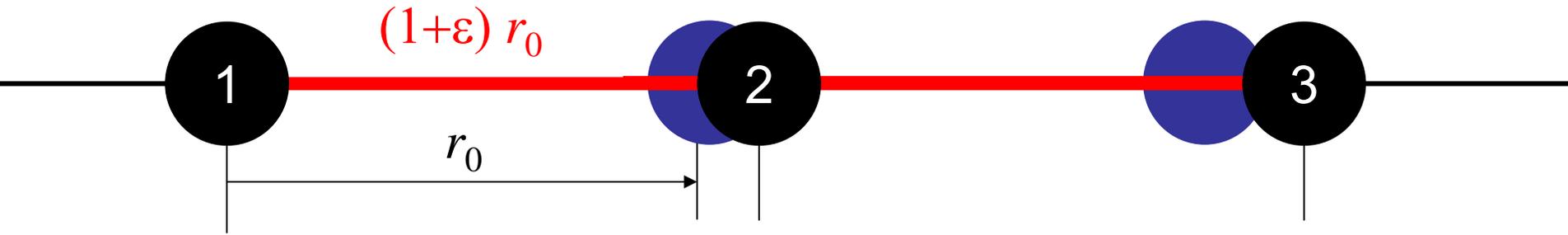
Stress $\sigma = \frac{\partial \psi(\varepsilon)}{\partial \varepsilon}$

Young's modulus $E = \frac{\partial^2 \psi(\varepsilon)}{\partial \varepsilon^2}$

$$\sigma = E\varepsilon$$

1D example – “Cauchy-Born rule”

- Impose homogeneous strain field on 1D string of atoms
- Then obtain $\sigma = E\varepsilon$ from that



$$\psi(\varepsilon) = \frac{1}{r_0 \cdot D} \phi(r) = \frac{1}{r_0 \cdot D} \phi((1 + \varepsilon) \cdot r_0)$$

$r = (1 + \varepsilon) \cdot r_0$
 \downarrow
 interatomic potential

\uparrow
 out-of-plane area $\longrightarrow r_0 \cdot D$ atomic volume

Strain energy density function
 $\sigma = \frac{\partial \psi(\varepsilon)}{\partial \varepsilon} \quad E = \frac{\partial^2 \psi(\varepsilon)}{\partial \varepsilon^2}$

2D hexagonal lattice

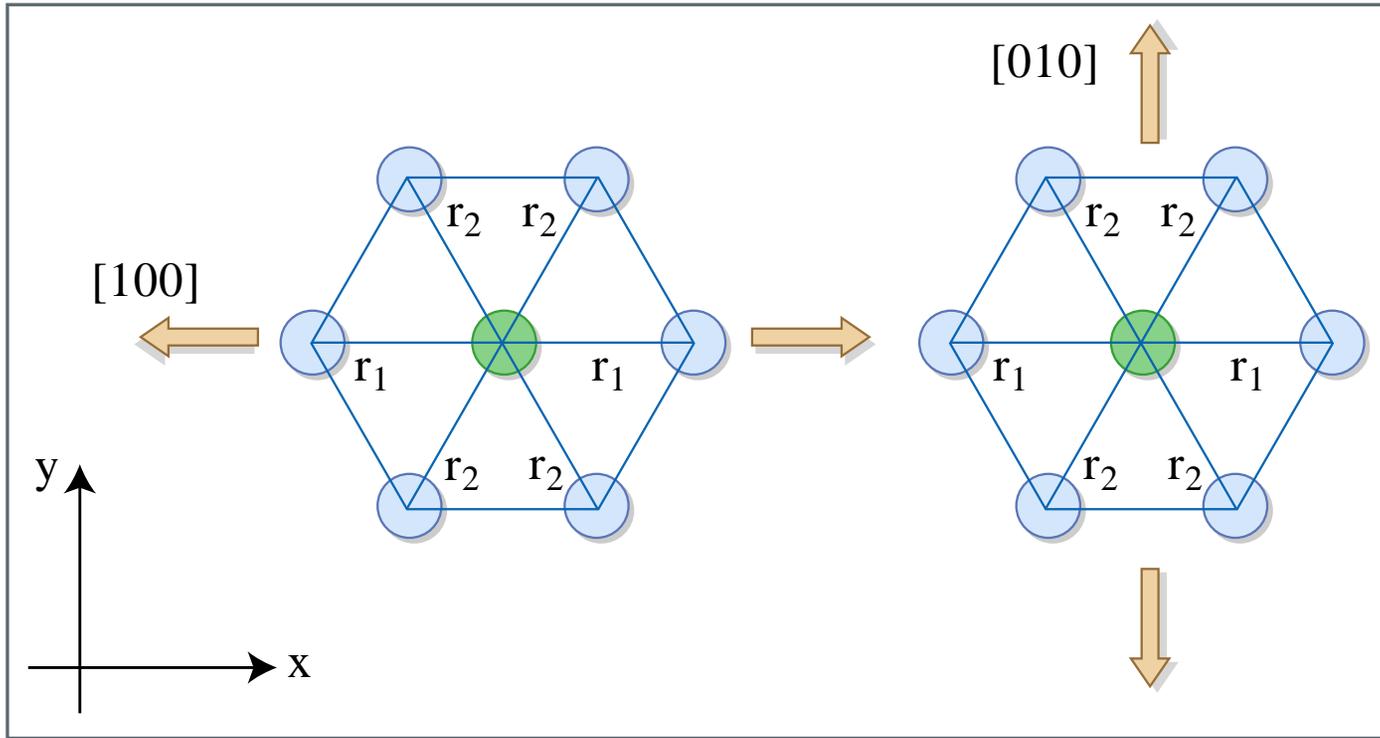


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$$\phi'' = k$$

$$\psi(\varepsilon_{ij}) = \frac{\sqrt{3}}{8} \phi'' \left(3\varepsilon_{11}^2 + 2\varepsilon_{11}\varepsilon_{22} + 3\varepsilon_{22}^2 + (\varepsilon_{21} + \varepsilon_{12})^2 \right)$$

$$\sigma_{ij} = \frac{\partial \psi(\varepsilon_{ij})}{\partial \varepsilon_{ij}} \quad c_{ijkl} = \frac{\partial^2 \psi(\varepsilon_{ij})}{\partial \varepsilon_{ij} \partial \varepsilon_{kl}}$$

2D triangular lattice, LJ potential

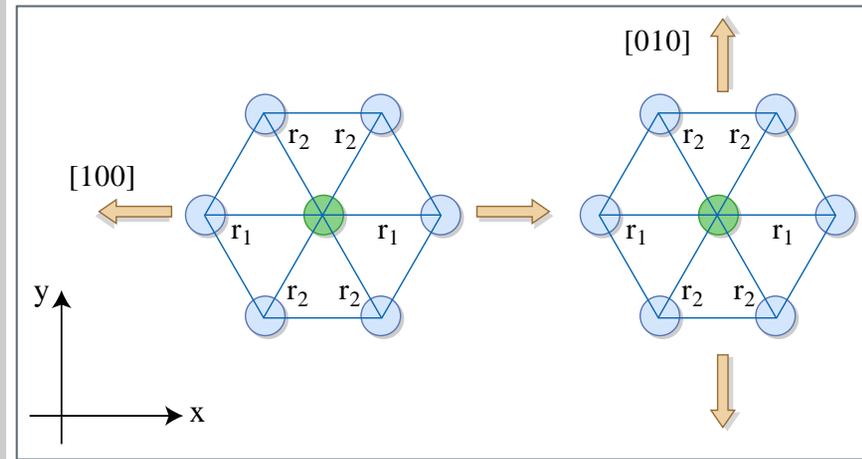
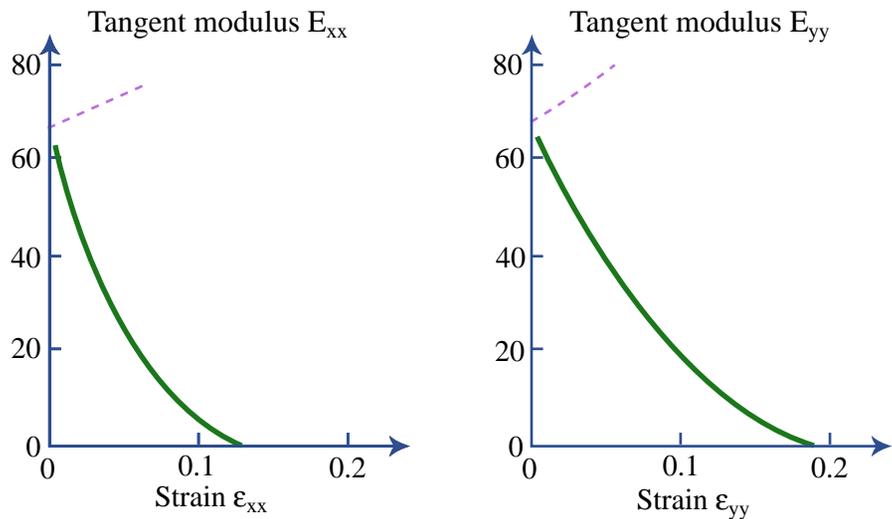
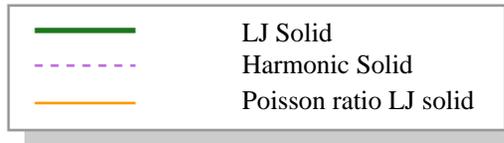
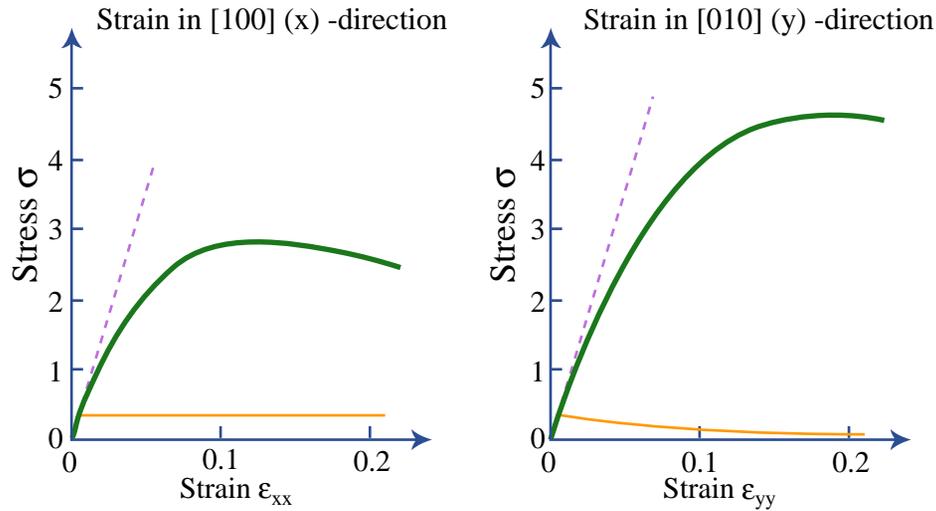


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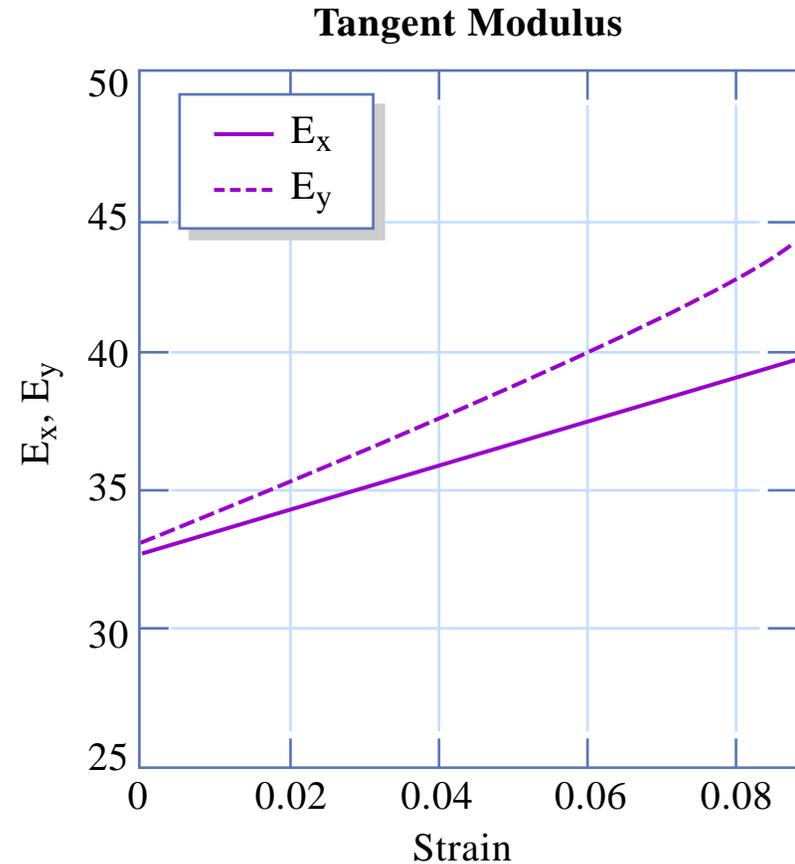
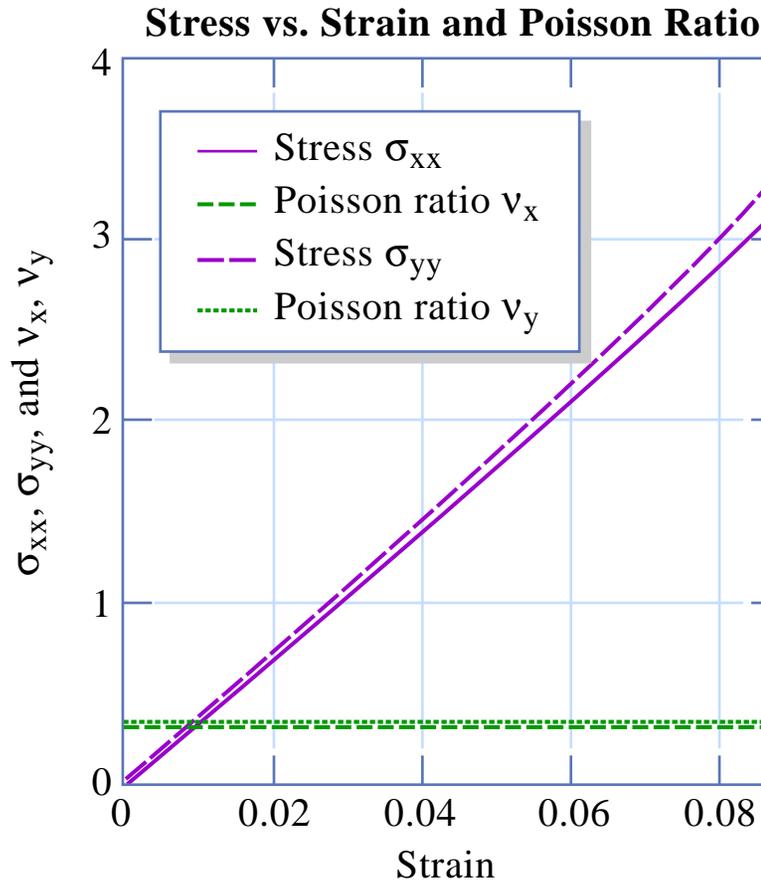
$$\epsilon = 1$$

$$\sigma = 1$$

12:6 LJ potential

Image by MIT OpenCourseWare.

2D triangular lattice, harmonic potential



Elastic properties of the triangular lattice with harmonic interactions, stress versus strain (left) and tangent moduli E_x and E_y (right). The stress state is uniaxial tension, that is the stress in the direction orthogonal to the loading is relaxed and zero.

Elastic properties

$$E = \frac{2}{\sqrt{3}}k, \quad \mu = \frac{\sqrt{3}}{4}k \quad \phi'' = k$$

Enables to calculate wave speeds:

| Spring constant k | Young's modulus E | Shear modulus μ | Poisson's ratio ν | c_l | c_s | c_R |
|-------------------------------|---------------------|---------------------|-----------------------|-------|-------|-------|
| $36\sqrt[3]{2} \approx 28.57$ | 33 | 12.4 | 0.33 | 6.36 | 3.67 | 3.39 |
| $72\sqrt[3]{2} \approx 57.14$ | 66 | 24.8 | 0.33 | 9 | 5.2 | 4.8 |

Surface energy calculation

$$\gamma_s = -\frac{\Delta\phi}{d}$$

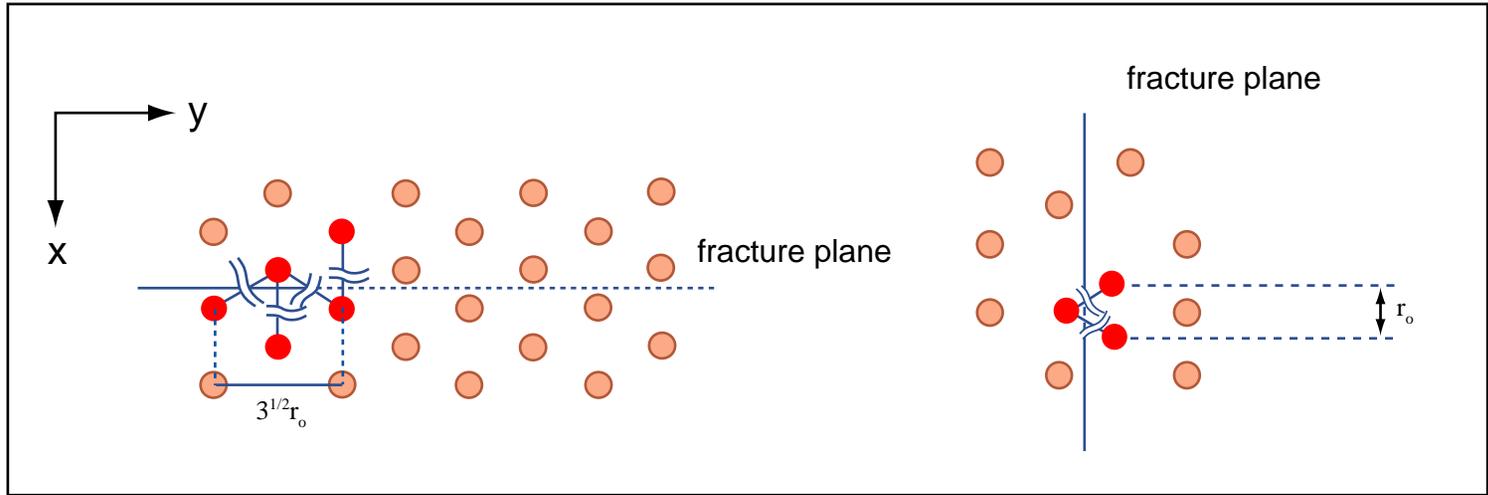


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Harmonic potential with bond snapping distance r_{break}

$$\gamma_s^{\text{bs,h}} = \frac{k(r_{\text{break}} - r_0)^2}{\sqrt{3}r_0}$$

$$\gamma_s^{\text{bs,l}} = \frac{k(r_{\text{break}} - r_0)^2}{2r_0}$$

Note: out-of-plane unity thickness

2.2 Application

***Focus: effects of material nonlinearities
(reflected in choice of model)***

Coordinate system and atomistic model

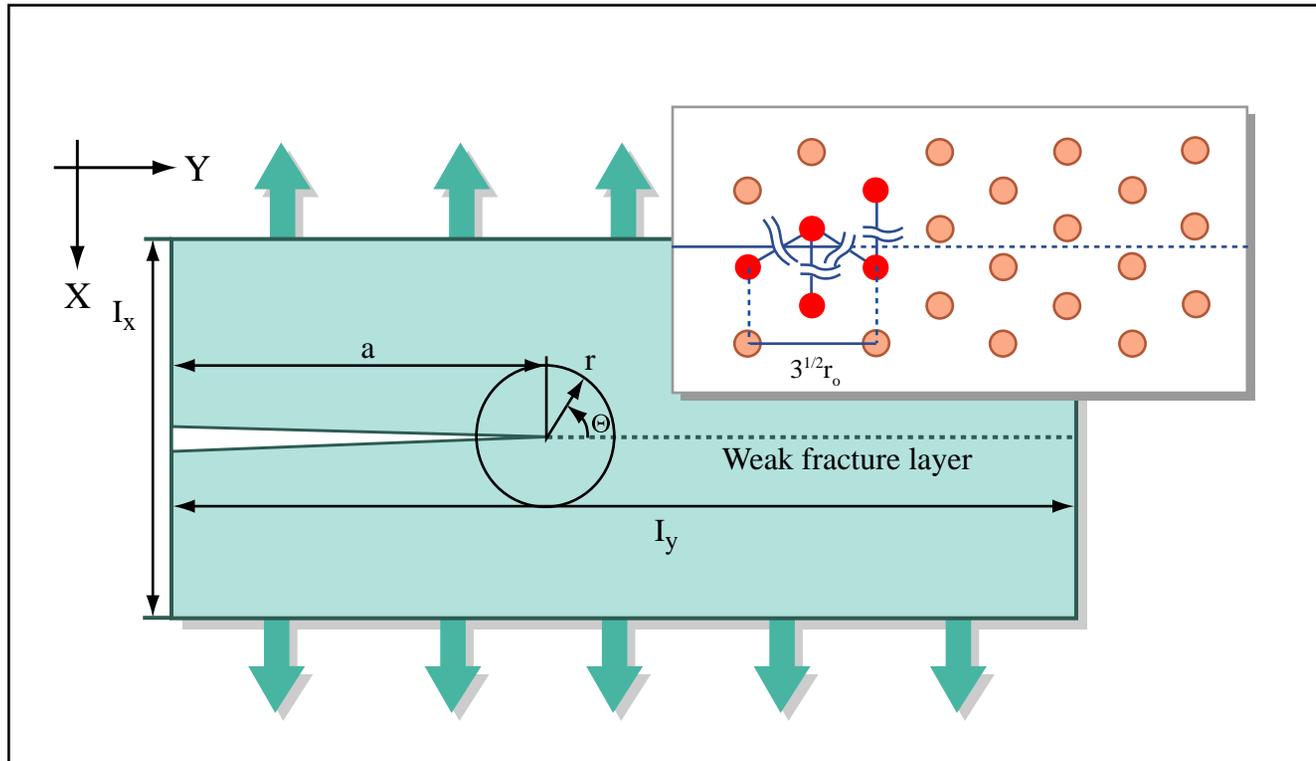


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Pair potential to describe atomic interactions
Confine crack to a 1D path (weak fracture layer)

Linear versus nonlinear elasticity=hyperelasticity

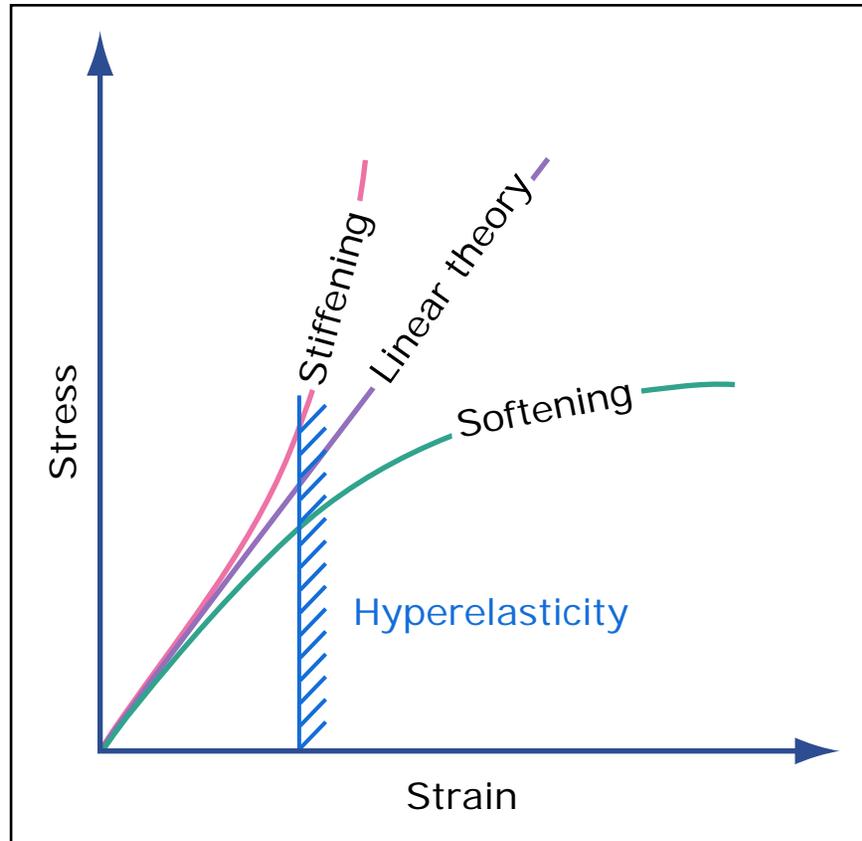


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Linear elasticity: Young's modulus (stiffness) does not change with deformation

Nonlinear elasticity = hyperelasticity: Young's modulus (stiffness) changes with deformation

Subsonic and supersonic fracture

- Under certain conditions, material nonlinearities (that is, the behavior of materials under large deformation = hyperelasticity) becomes important

- This can lead to different limiting speeds than described by the model introduced above

$$\sigma(r) \sim \frac{1}{\sqrt{r}}$$

Deformation field near a crack

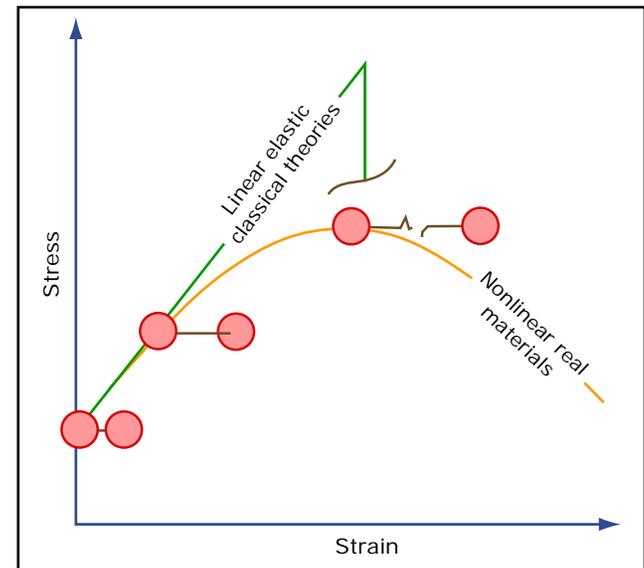
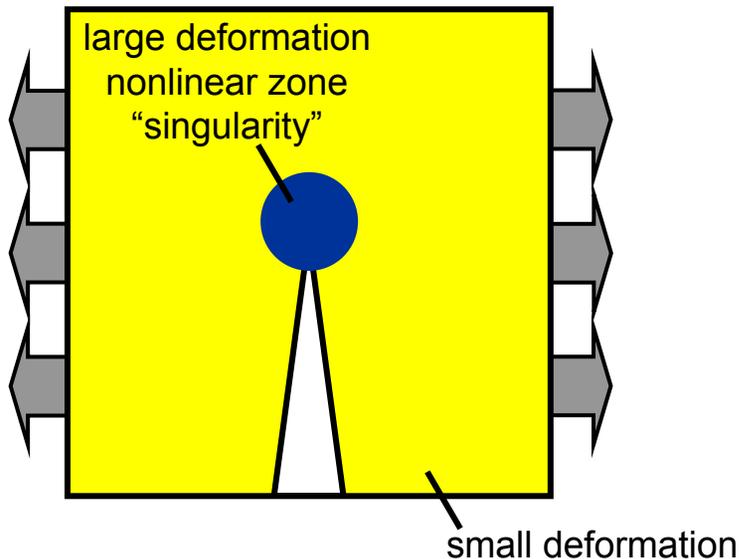


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Limiting speeds of cracks

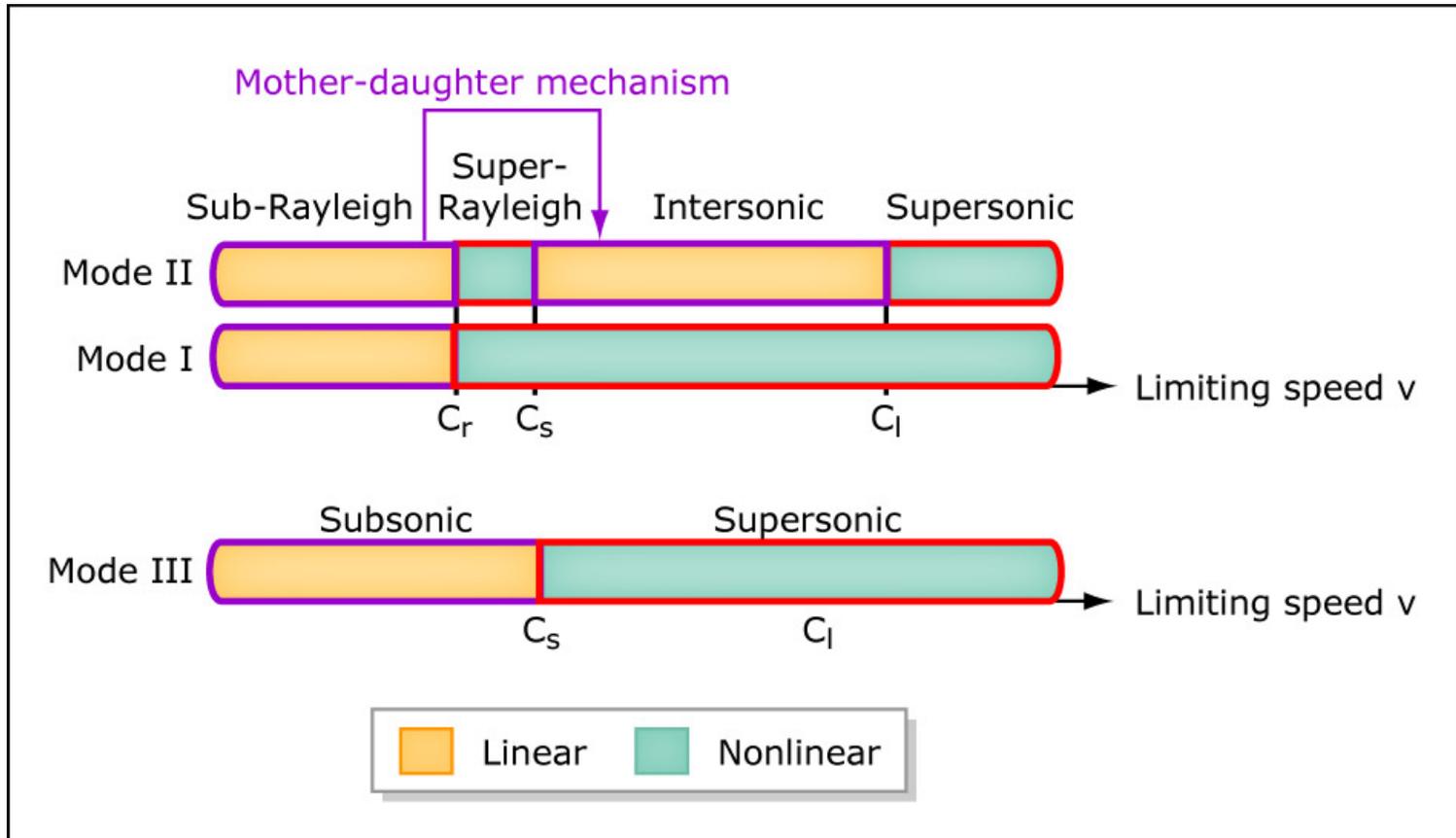
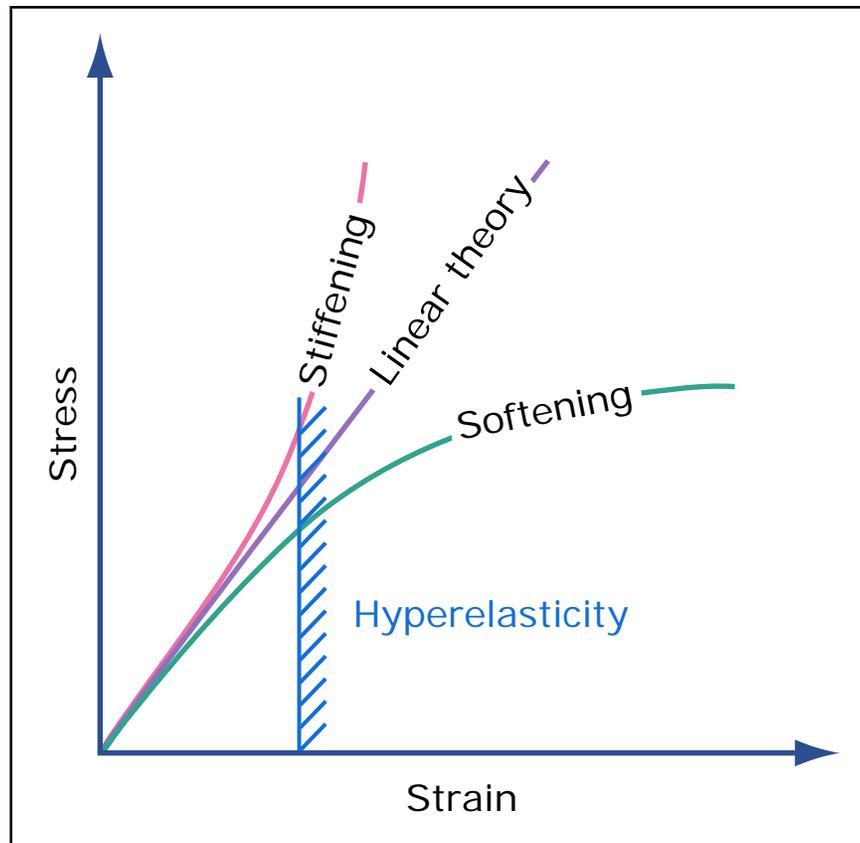


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- Under presence of hyperelastic effects, cracks can exceed the conventional barrier given by the wave speeds
- This is a “local” effect due to enhancement of energy flux
- Subsonic fracture due to local softening, that is, reduction of energy flux

Stiffening vs. softening behavior

real materials



“linear elasticity”

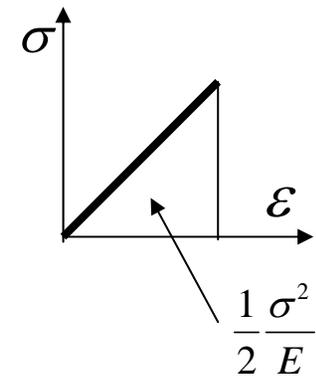


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Increased/decreased wave speed

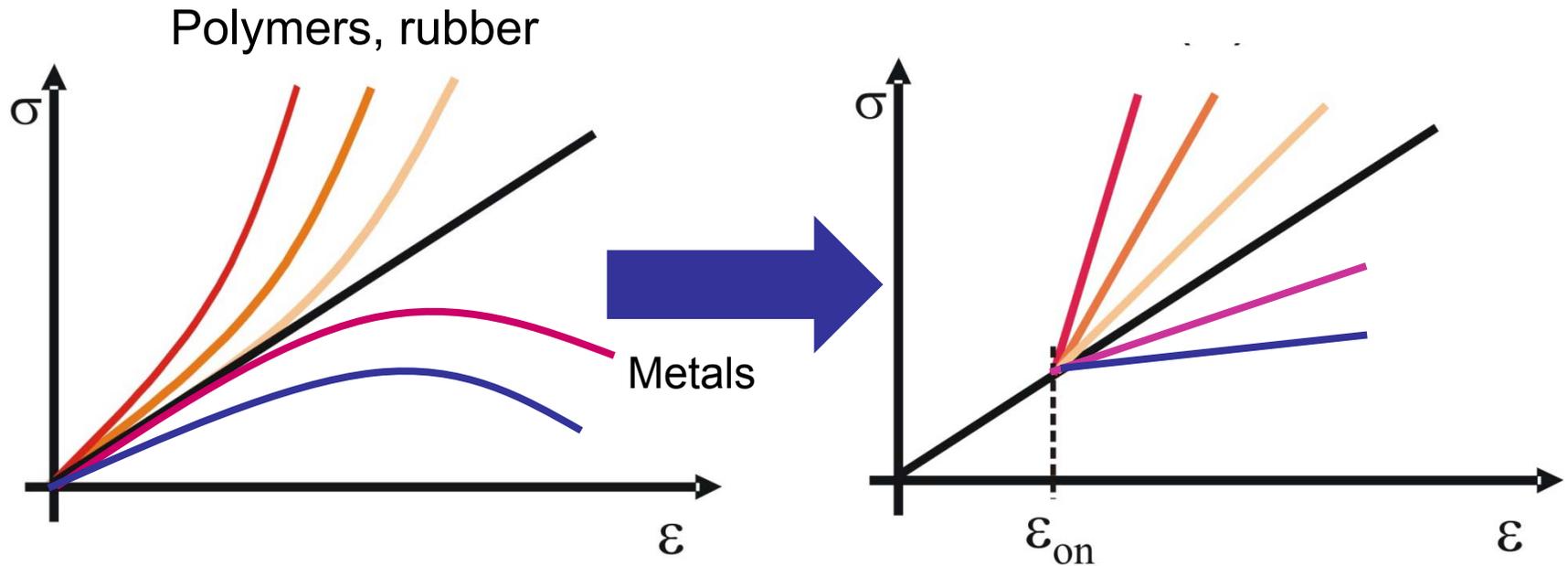
$$c_l = \sqrt{\frac{3\mu}{\rho}}$$

$$c_s = \sqrt{\frac{\mu}{\rho}}$$

$$c_R \approx \beta c_s$$

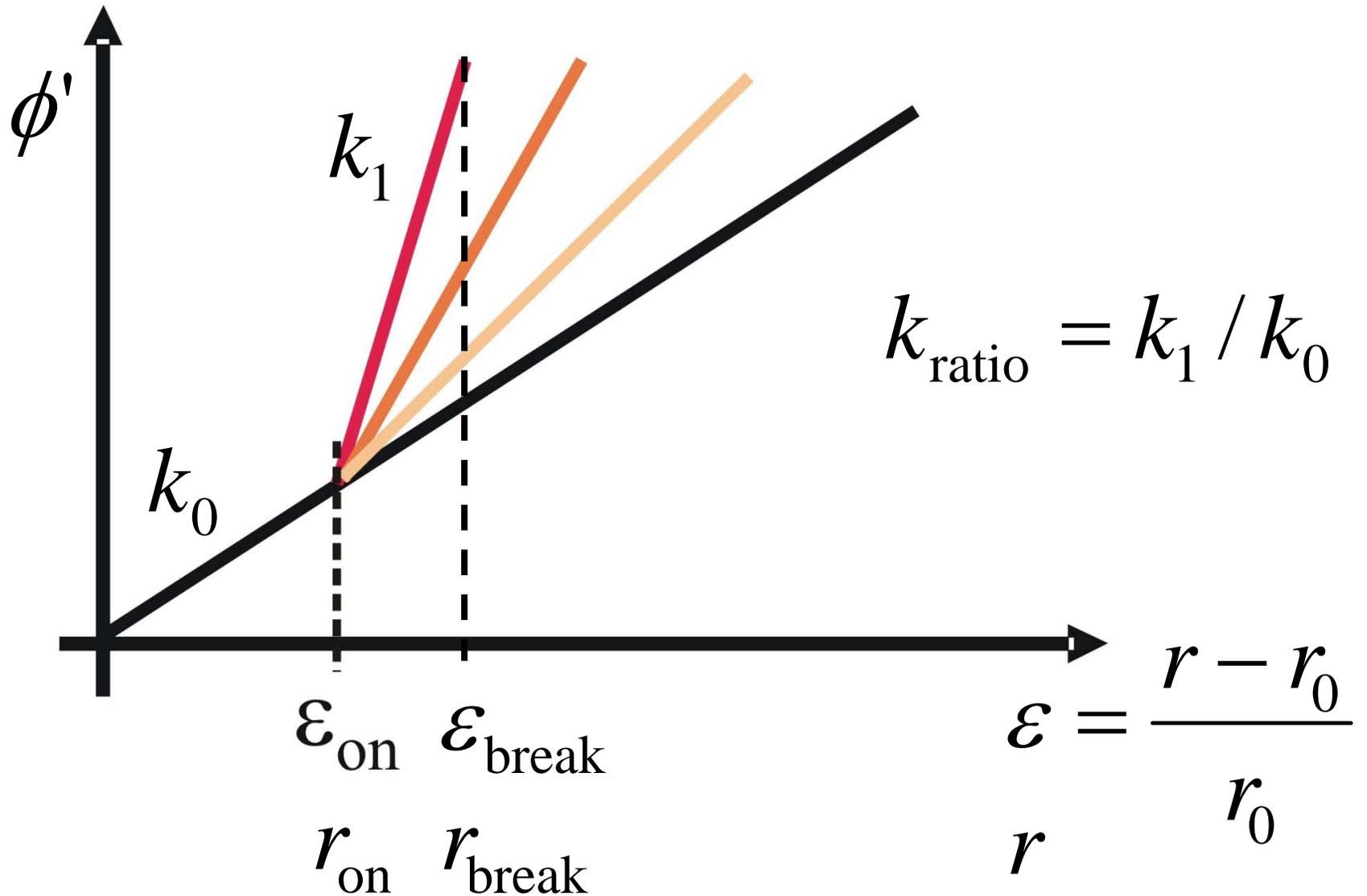
$$\beta \approx 0.923$$

MD model development: biharmonic potential



- **Stiffness change under deformation**, with different strength
- Atomic bonds break at critical atomic separation
- **Want:** simple set of parameters that control these properties (as few as possible, to gain generic insight)

Bi-harmonic potential – control parameters



Biharmonic potential definition

The biharmonic potential is defined as:

$$\phi(r_{ij}) = \begin{cases} a_0 + \frac{1}{2}k_0(r_{ij} - r_0)^2 & \text{if } r_{ij} < r_{\text{on}}, \\ a_1 + \frac{1}{2}k_1(r_{ij} - r_1)^2 & \text{if } r_{ij} \geq r_{\text{on}} \end{cases}$$

where r_{on} is the critical atomic separation for the onset of the hyperelastic effect, and

$$a_1 = a_0 + \frac{1}{2}k_0(r_{\text{on}} - r_0)^2 - \frac{1}{2}k_1(r_{\text{on}} - r_1)^2$$

and

$$r_1 = \frac{1}{2}(r_{\text{on}} + r_0)$$

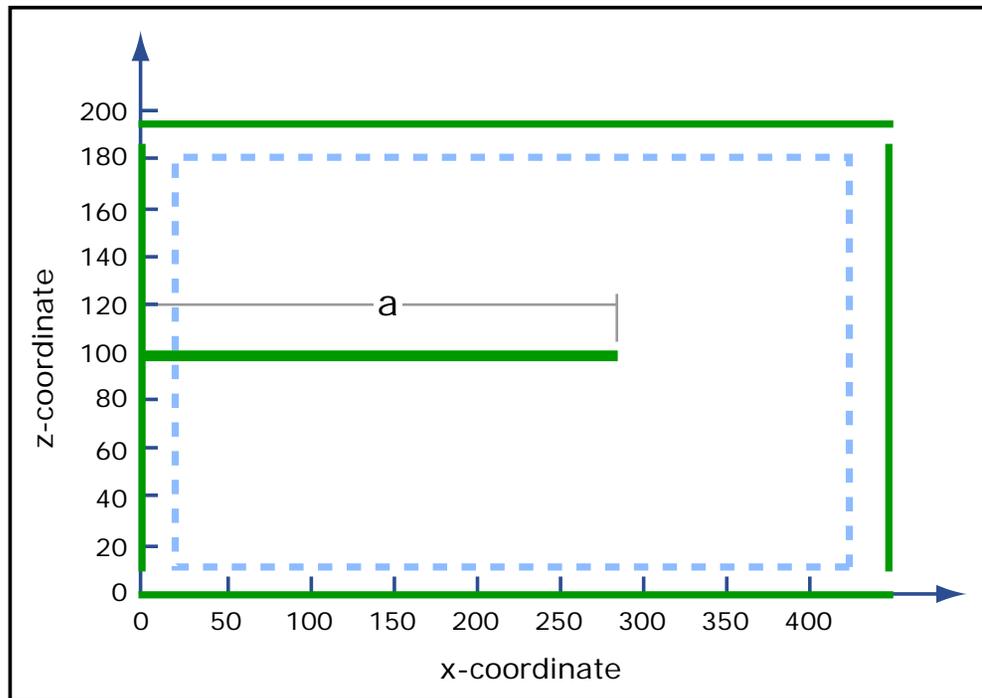
are found by continuity conditions of the potential at $r = r_{\text{on}}$.

The values k_0 and k_1 refer to the small- and large-strain spring constants.

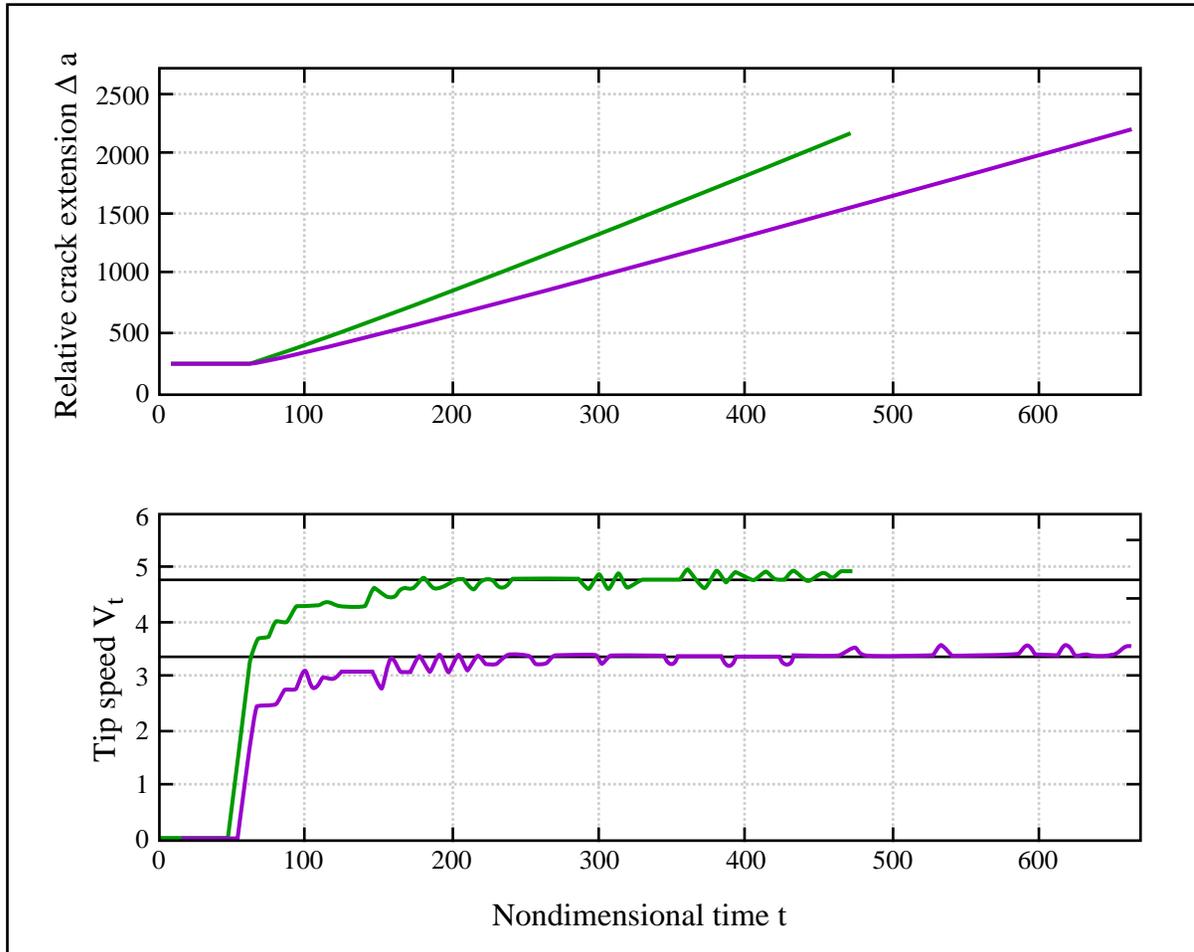
Energy filtering: visualization approach

- Only plot atoms associated with higher energy
- Enables determination of crack tip (atoms at surface have higher energy, as they have fewer neighbors than atoms in the bulk)

$$\text{Energy of atom } i \quad U_i = \sum_{j=1}^N \phi(r_{ij})$$



MD simulation results: confirms linear continuum theory



$$a(t)$$

crack speed
=time derivative of a

$$v(t) = da/dt$$

Image by MIT OpenCourseWare.

| Spring constant k | Young's modulus E | Shear modulus μ | Poisson's ratio ν | c_l | c_s | c_R |
|--------------------------------|---------------------|---------------------|-----------------------|-------|-------|-------|
| $36 \sqrt[3]{2} \approx 28.57$ | 33 | 12.4 | 0.33 | 6.36 | 3.67 | 3.39 |
| $72 \sqrt[3]{2} \approx 57.14$ | 66 | 24.8 | 0.33 | 9 | 5.2 | 4.8 |

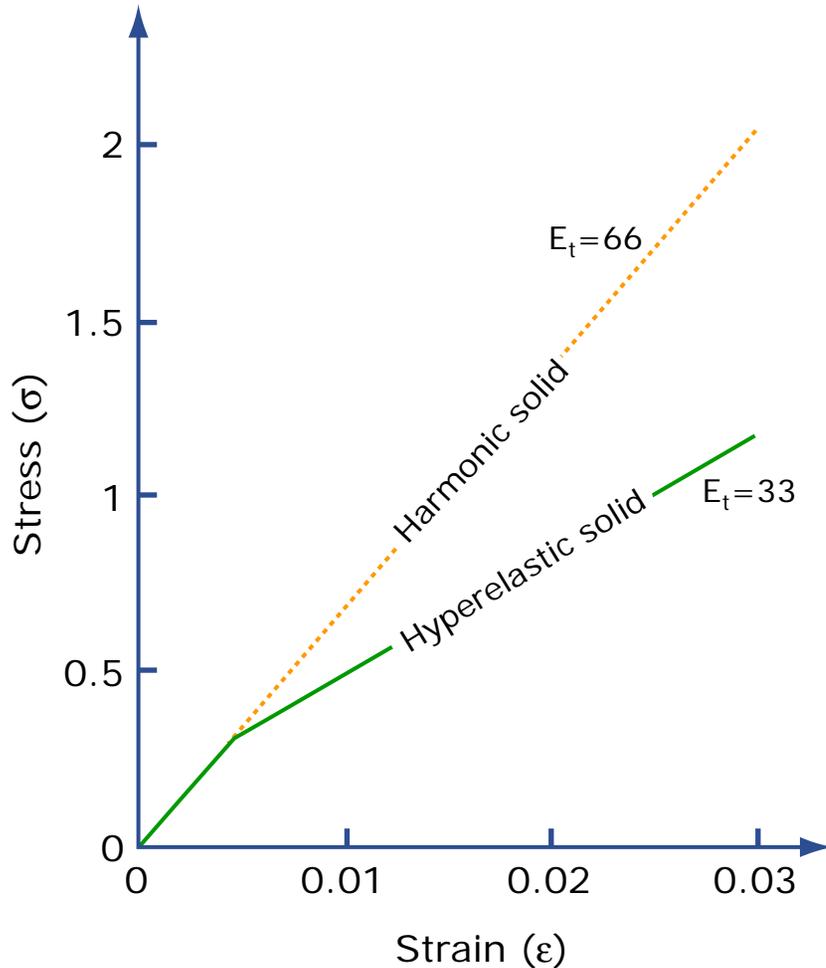
Virial stress field around a crack

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Please see: Fig. 6.30 in Buehler, Markus J. *Atomistic Modeling of Materials Failure*. Springer, 2008.

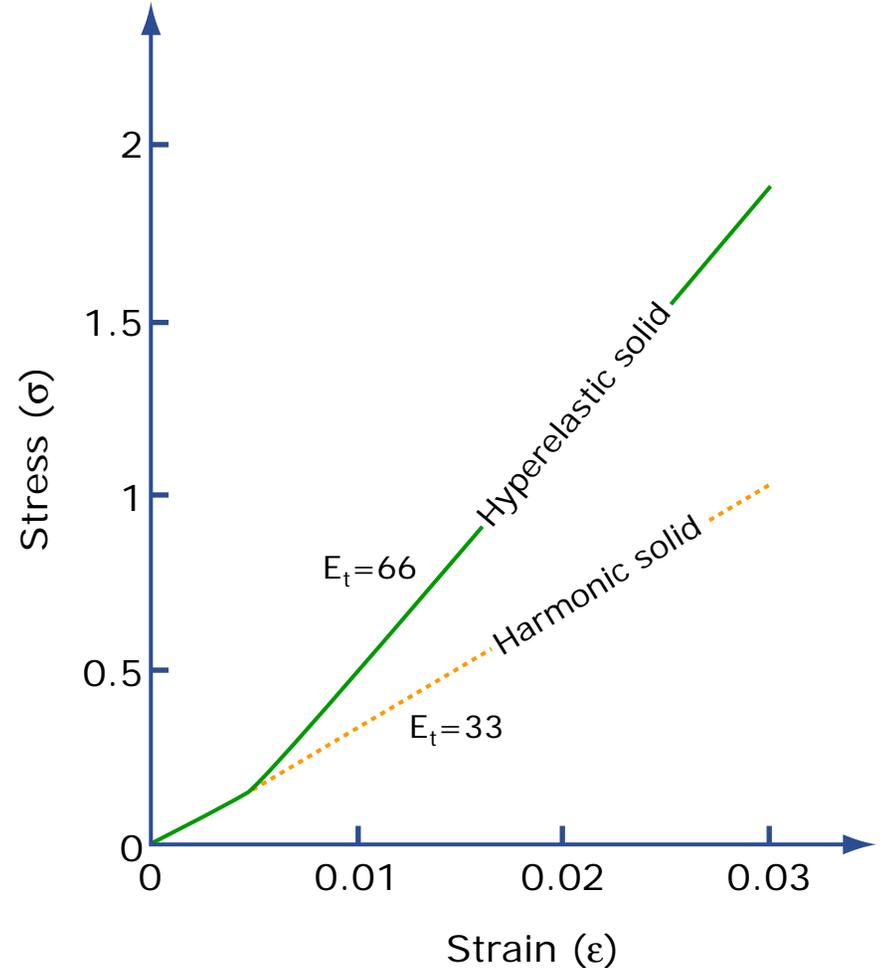
large stresses
at crack tip
- induce bond failure

Biharmonic potential – bilinear elasticity

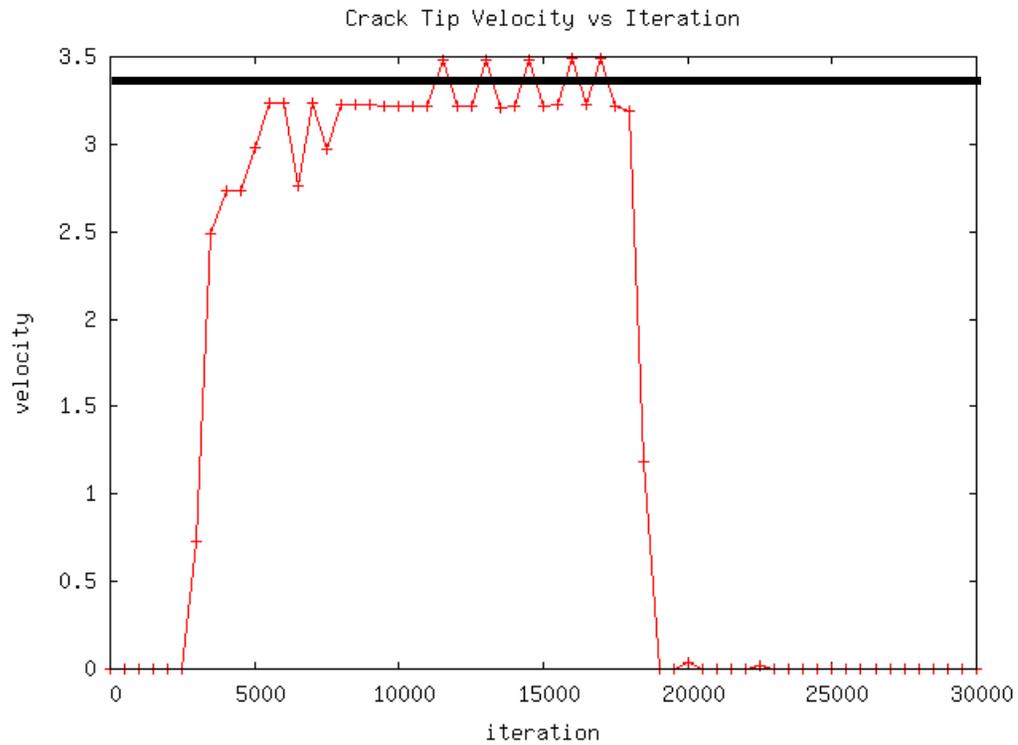
Softening



Stiffening

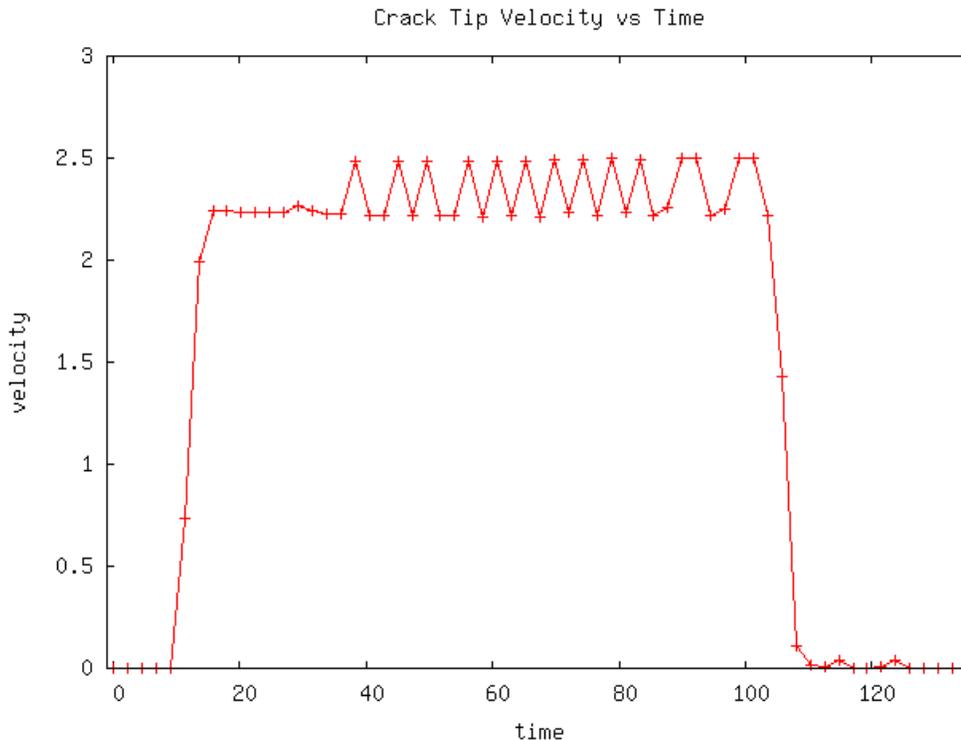


Harmonic system



Subsonic fracture

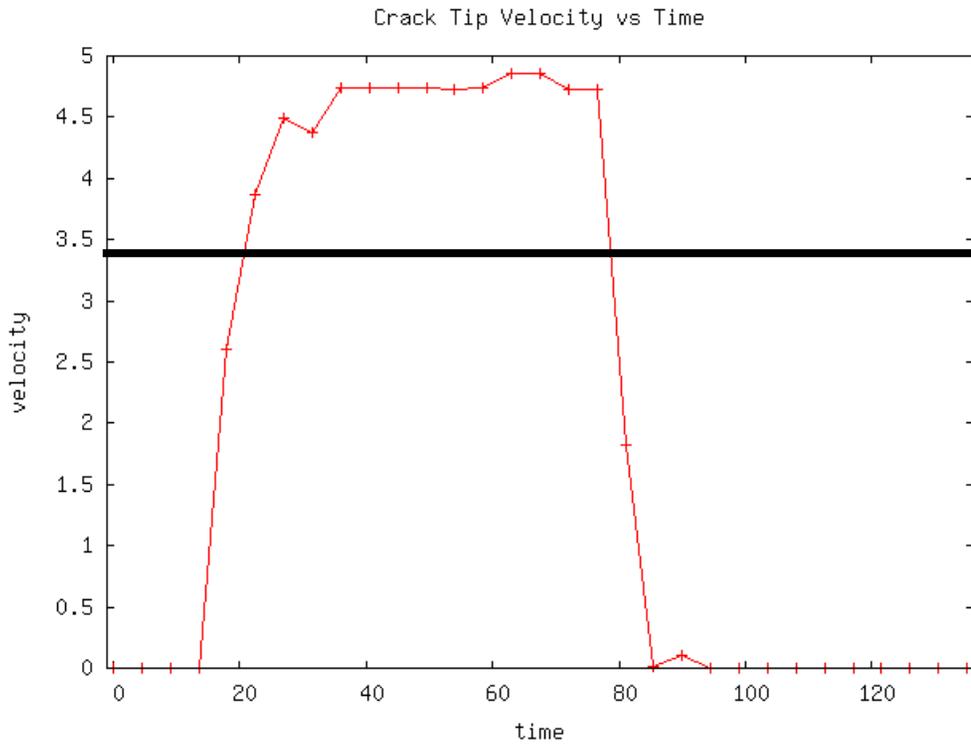
- Softening material behavior leads to subsonic fracture, that is, the crack can never attain its theoretical limiting speed
- Materials: metals, ceramics



$$< 3.4 = c_R$$

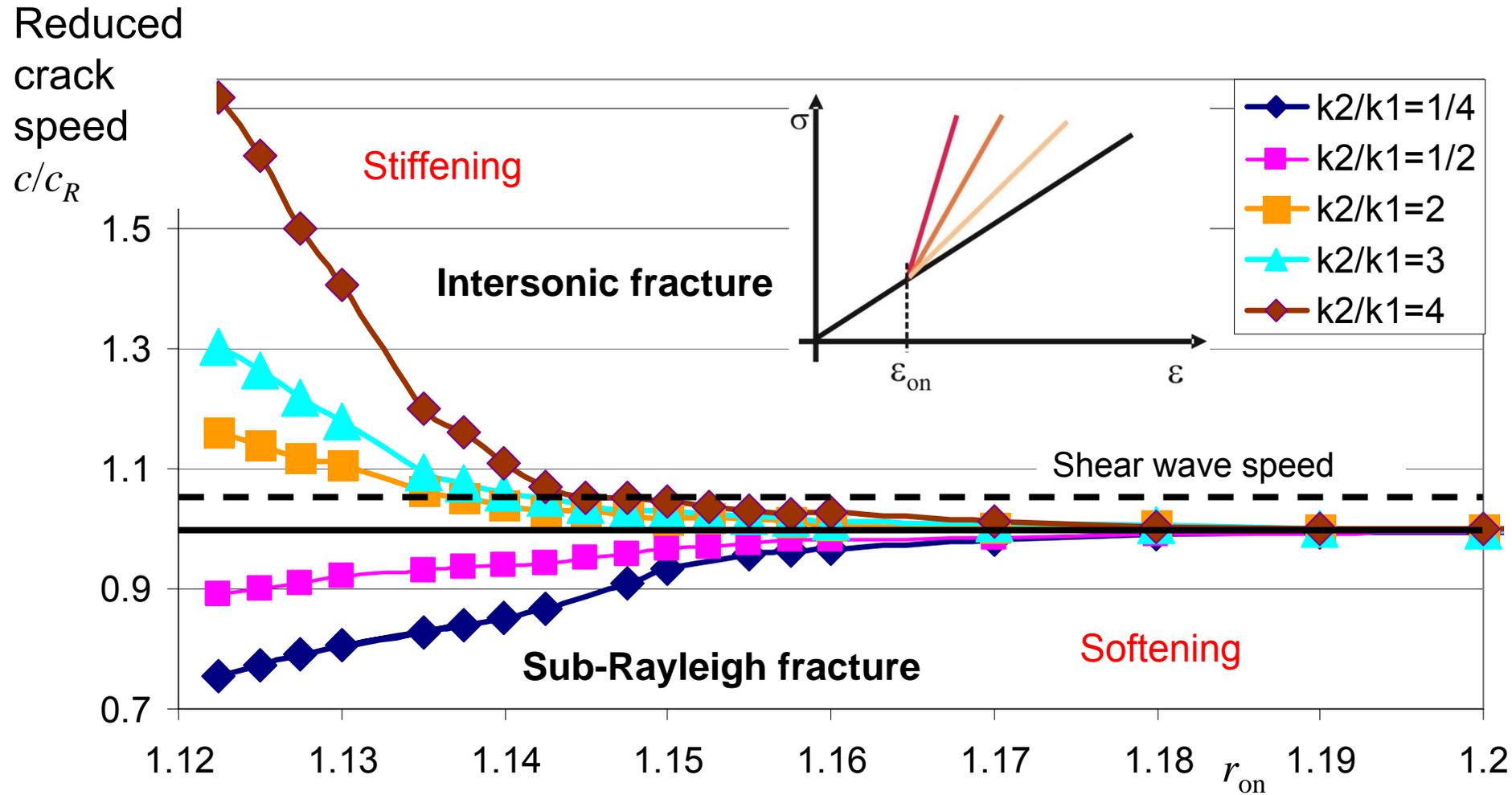
Supersonic fracture

- Stiffening material behavior leads to subsonic fracture, that is, the crack can exceed its theoretical limiting speed
- Materials: polymers



$> 3.4 = c_R$

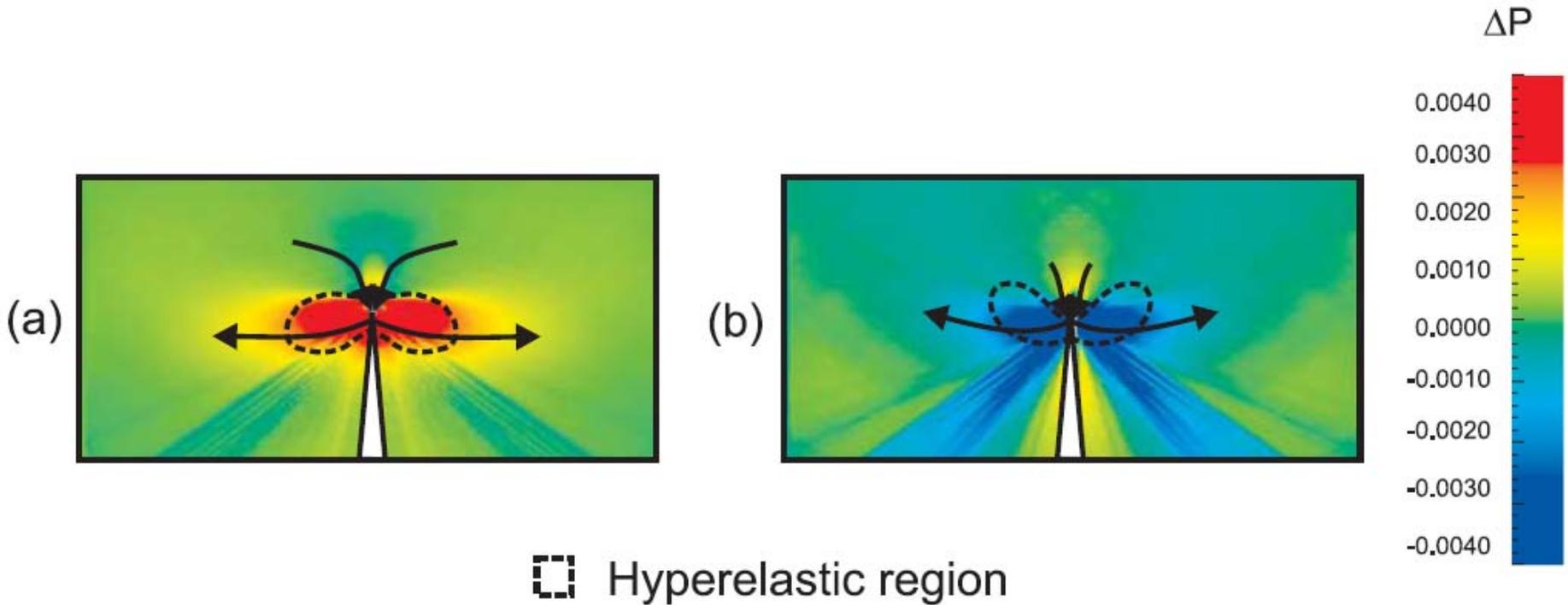
Different ratios of spring constants



Stiffening and softening effect: Increase or reduction of crack speed

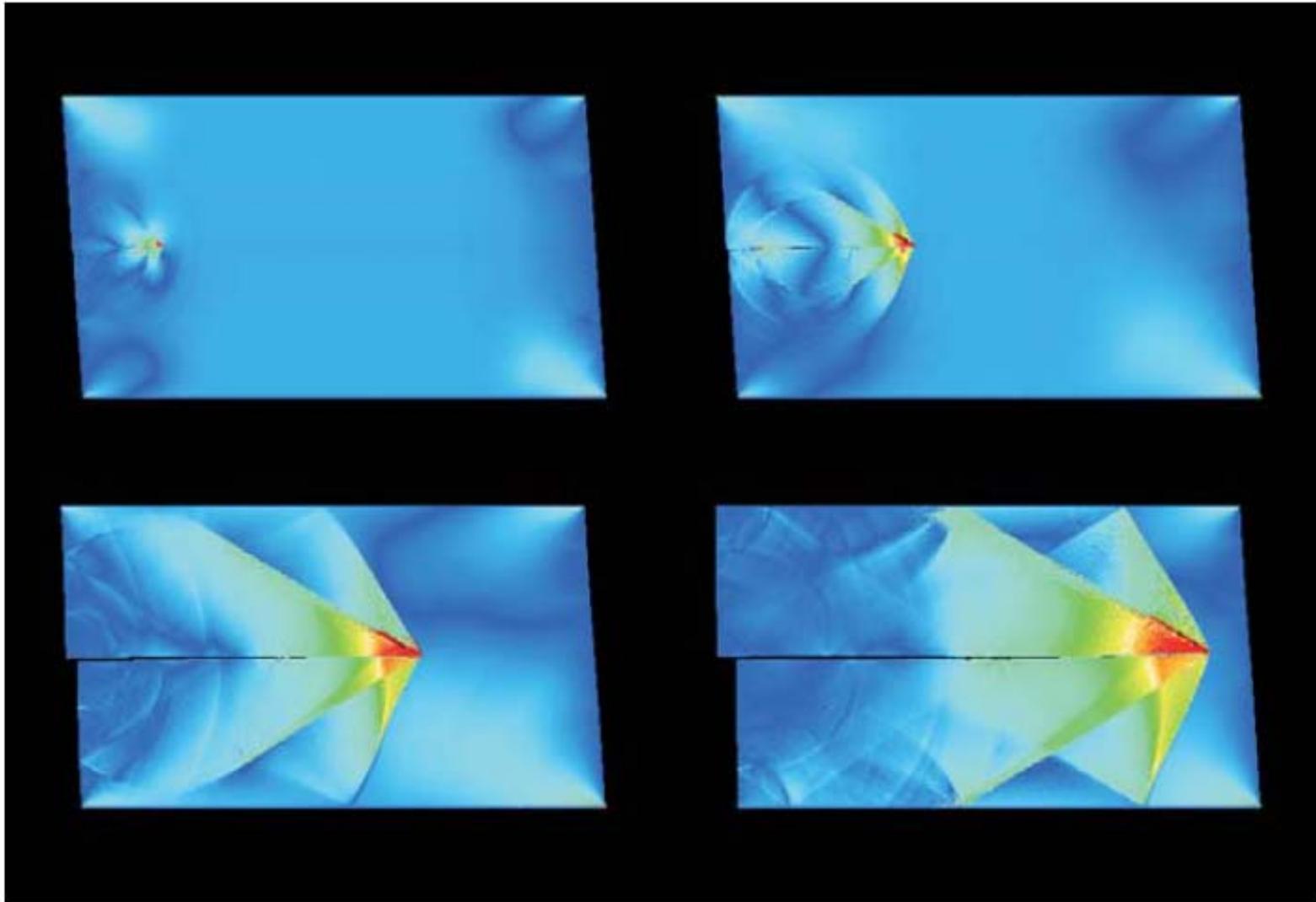
Physical basis for subsonic/supersonic fracture

- Changes in energy flow at the crack tip due to changes in local wave speed (energy flux higher in materials with higher wave speed)
- Controlled by a characteristic length scale χ



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Source: Buehler, M., F. Abraham, and H. Gao. "Hyperelasticity Governs Dynamic Fracture at a Critical Length Scale." *Nature* 426 (2003): 141-6. © 2003.

Supersonic fracture: mode II (shear)



Please see: Buehler, Markus J., Farid F. Abraham, and Huajian Gao. "Hyperelasticity Governs Dynamic Fracture at a Critical Length Scale." *Nature* 426 (November 13, 2003): 141-6.

Theoretical concept: energy flux reduction/enhancement

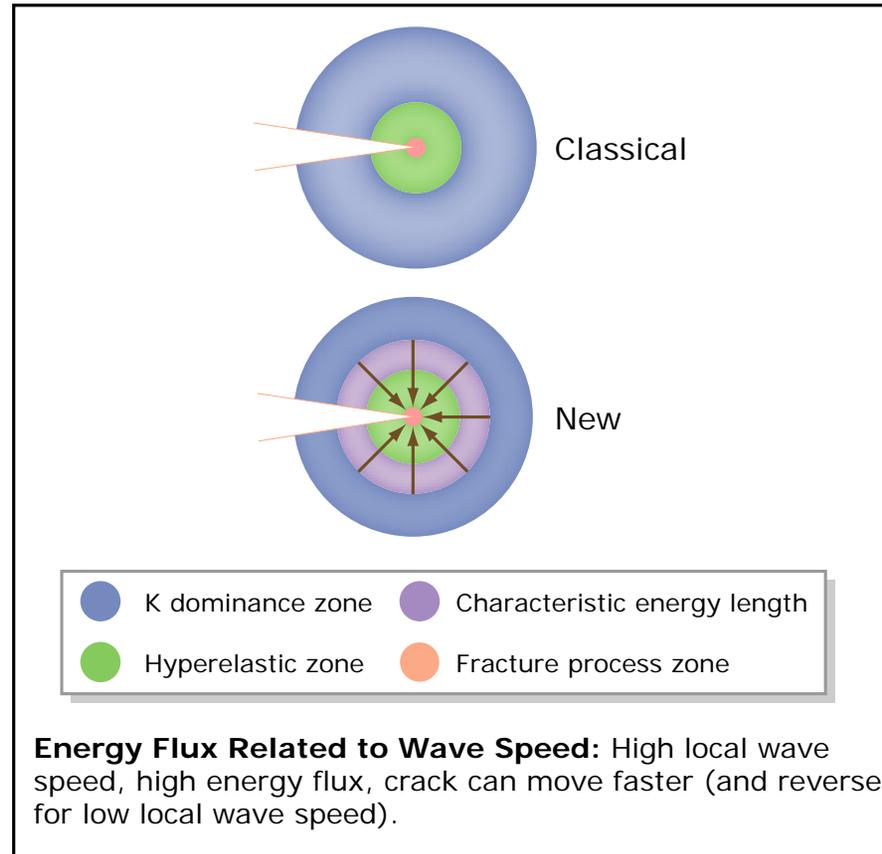
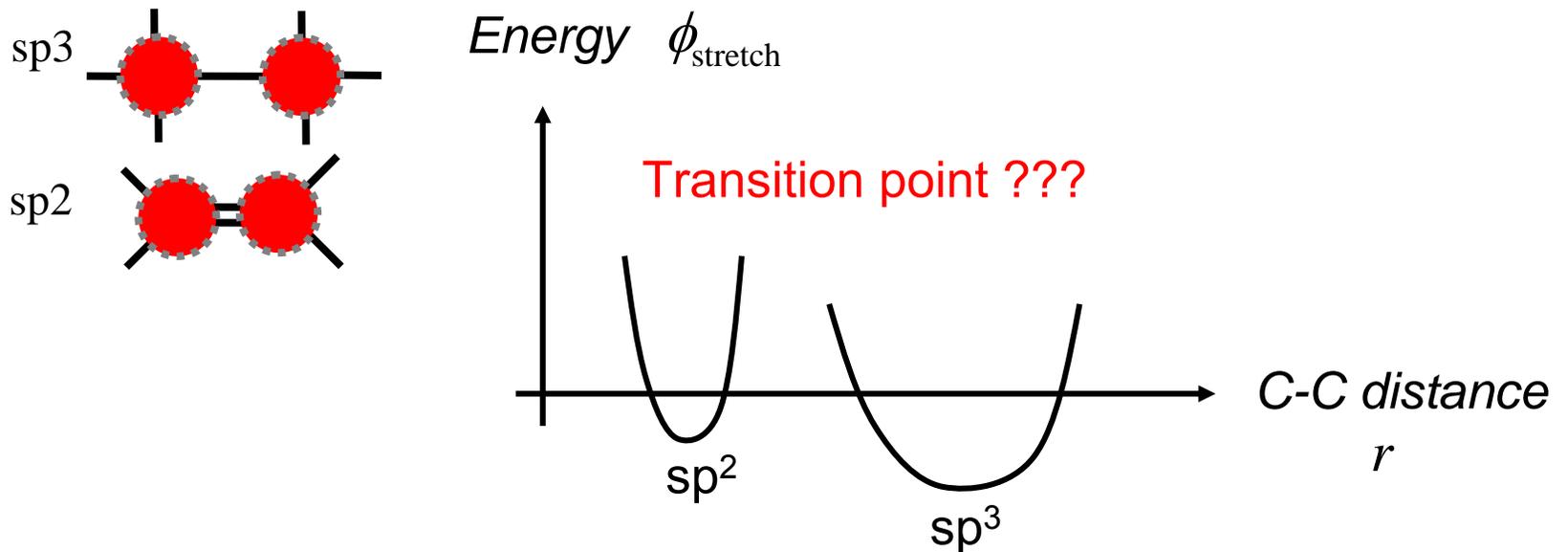


Image by MIT OpenCourseWare.

Energy flux related to wave speed: high local wave speed, high energy flux, crack can move faster (and reverse for low local wave speed)

3. Bond order force fields - how to model chemical reactions

Challenge: chemical reactions



CHARMM-type potential can not describe chemical reactions

Why can not model chemical reactions with |spring-like potentials?

$$\phi_{\text{stretch}} = \frac{1}{2} k_{\text{stretch}} (r - r_0)^2$$
$$\phi_{\text{bend}} = \frac{1}{2} k_{\text{bend}} (\theta - \theta_0)^2$$

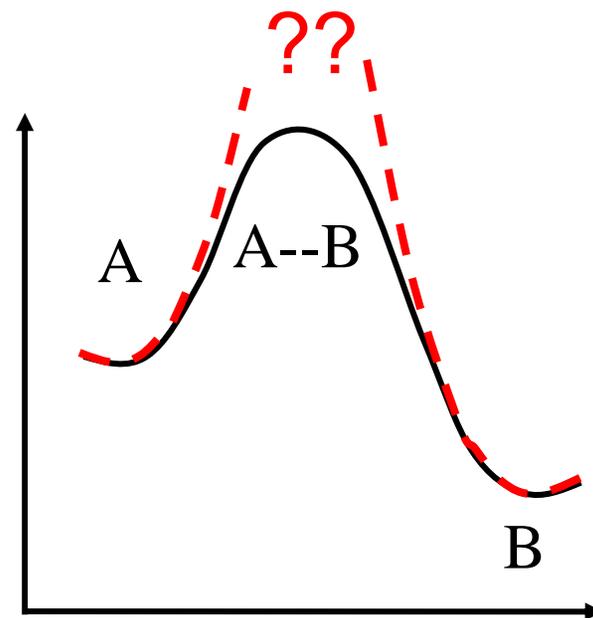
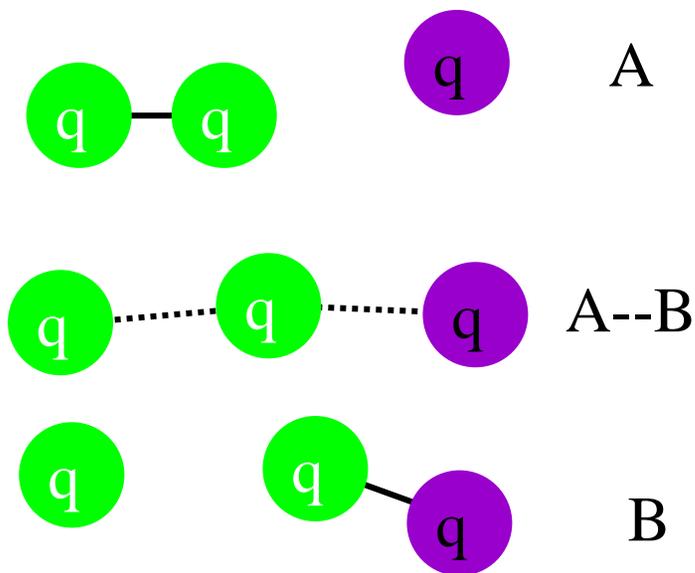
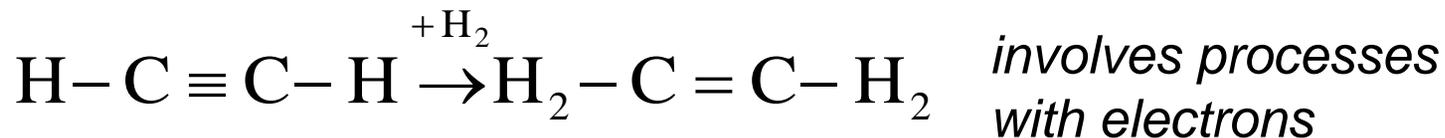
Set of parameters only valid for particular
molecule type / type of chemical bond

$$k_{\text{stretch},sp^2} \neq k_{\text{stretch},sp^3}$$

Reactive potentials or reactive force fields overcome these limitations

Key features of reactive potentials

- How can one accurately describe the transition energies during chemical reactions?
- Use computationally more efficient descriptions than relying on purely quantum mechanical (QM) methods (see part II, **methods limited to 100 atoms**)



Key features of reactive potentials

- Molecular model that is capable of describing **chemical reactions**
- **Continuous energy landscape during reactions** (key to enable integration of equations)
- No typing necessary, that is, atoms can be sp, sp², sp³... w/o further “tags” – **only element types**
- **Computationally efficient** (that is, should involve finite range interactions), so that large systems can be treated (> 10,000 atoms)
- **Parameters with physical meaning** (such as for the LJ potential)

Theoretical basis: bond order potential

Concept: Use pair potential that depends on atomic environment (similar to EAM, here applied to covalent bonds)

$$\phi(r_{ij}) = \phi_R(r_{ij}) - M_{ij}\phi_A(r_{ij})$$

↓

$$M_{ij} \sim Z^{-\delta}$$

Modulate strength of attractive part (e.g. by coordination, or “bond order”)

Abell, Tersoff

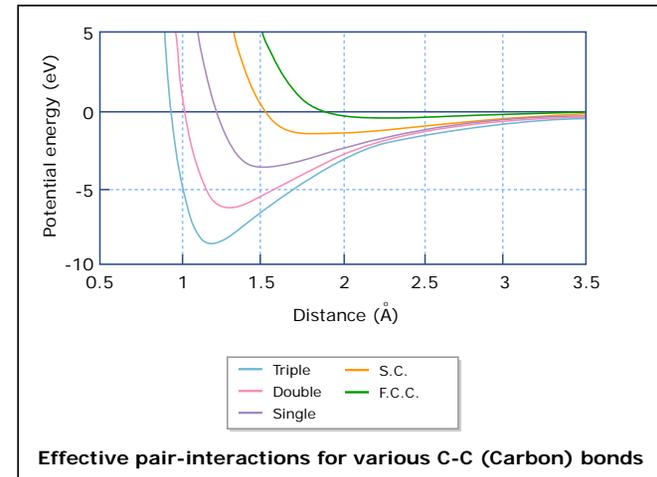


Image by MIT OpenCourseWare.

$$k(r) \sim k_0 M_{ij}(Z, \delta)$$

Changes in spring constant as function of bond order
Continuous change possible

= **continuous energy landscape during chemical reactions**

Theoretical basis: bond order potential

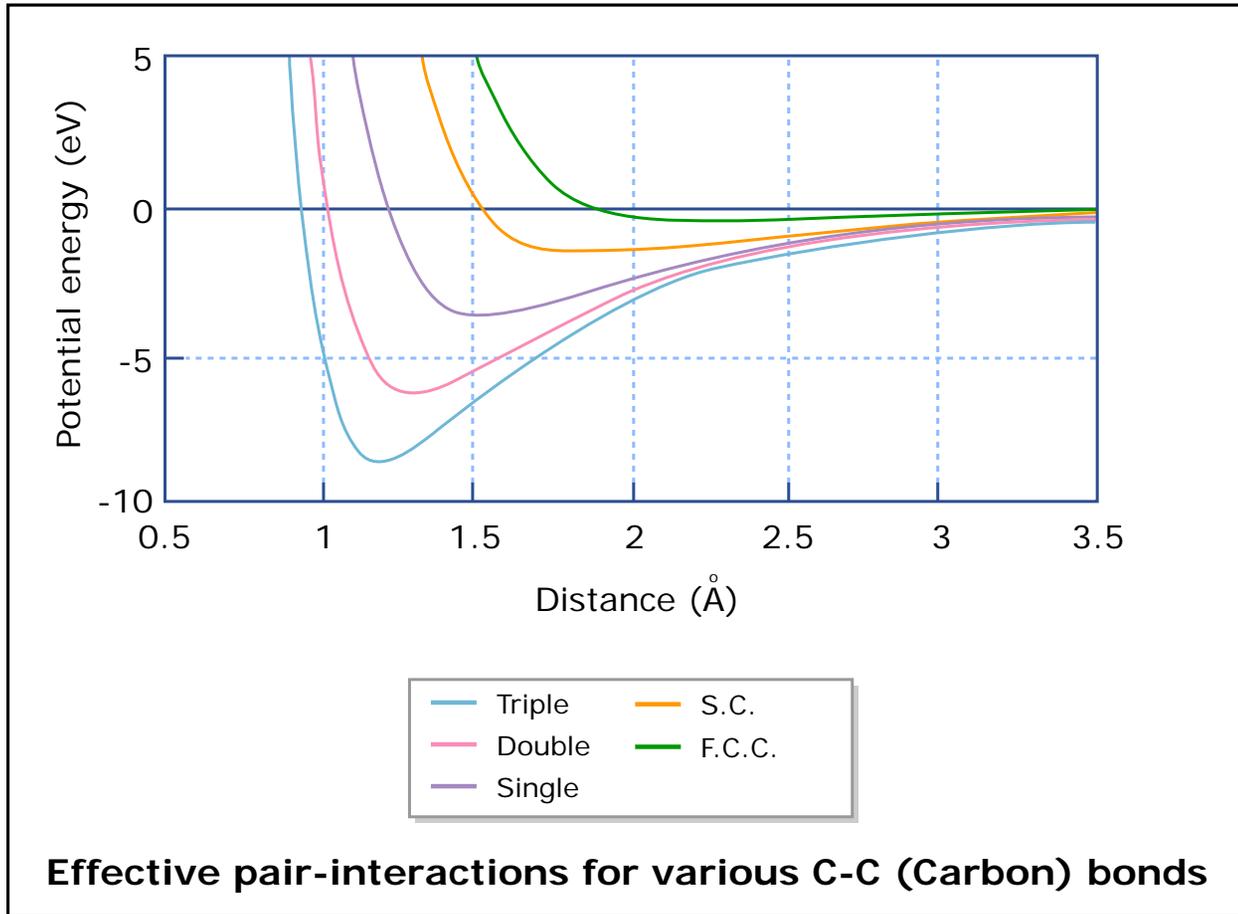
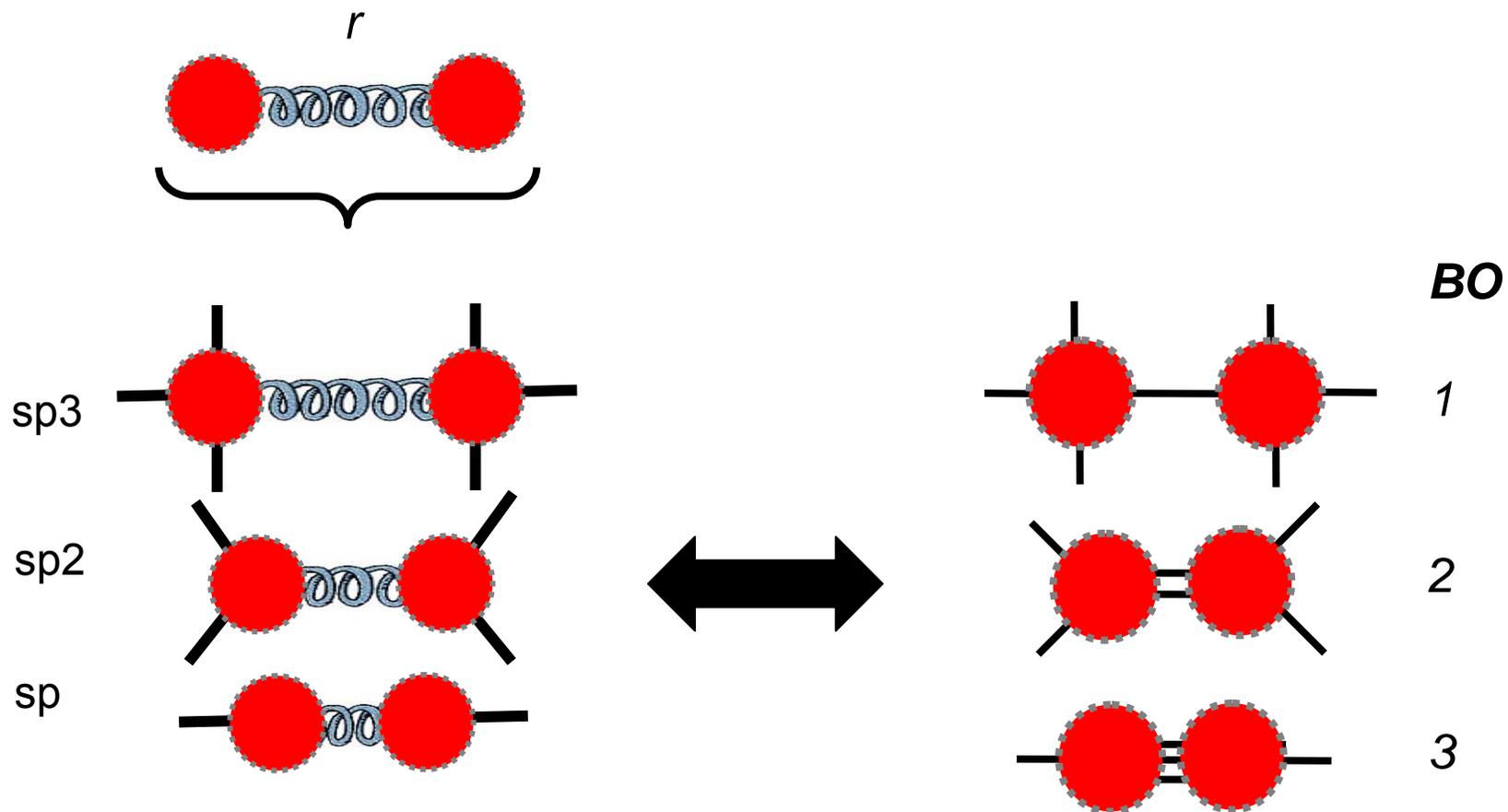
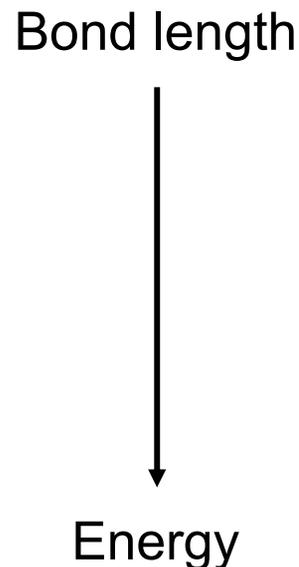
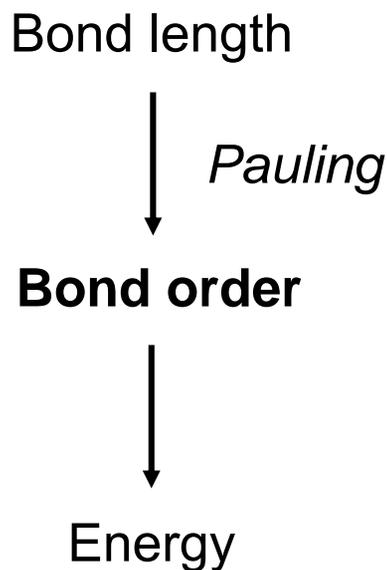


Image by MIT OpenCourseWare.

Concept of bond order (BO)



Bond order based energy landscape



Bond order potential
Allows for a more general
description of chemistry
All energy terms dependent
on bond order

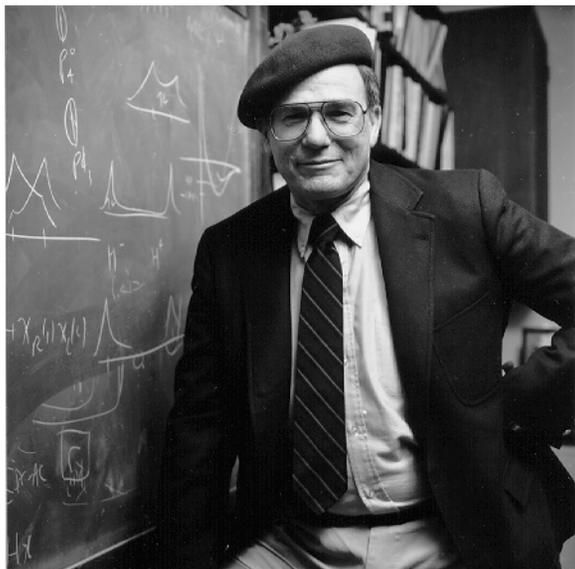
Conventional potential
(e.g. LJ, Morse)

Historical perspective of reactive bond order potentials

- **1985: Abell:** General expression for binding energy as a sum of near neighbor pair interactions moderated by local atomic environment
- **1990s: Tersoff, Brenner:** Use Abell formalism applied to silicon (successful for various solid state structures)
- **2000: Stuart et al.:** Reactive potential for hydrocarbons
- **2001: Duin, Goddard et al.:** Reactive potential for hydrocarbons “ReaxFF”
- **2002: Brenner et al.:** Second generation “REBO” potential for hydrocarbons
- **2003-2005:** Extension of ReaxFF to various materials including metals, ceramics, silicon, polymers and more in Goddard’s group

Example: ReaxFF reactive force field

William A. Goddard III
California Institute of Technology



Courtesy of Bill Goddard. Used with permission.

Adri C.T. v. Duin
California Institute of Technology

Example: Calculation of bond energy

$$E_{system} = E_{bond} + E_{vdWaals} + E_{Coulomb} + E_{val,angle} + E_{tors} + E_{over} + E_{under}$$

$$E_{bond} = -D_e \cdot BO_{ij} \cdot \exp\left[p_{be,1} \left(1 - BO_{ij}^{p_{be,1}}\right)\right]$$

Bond energy between atoms i and j does not depend on bond distance

Instead, it depends on bond order

Illustration: Bond energy

$$E_{bond} = -D_e^\sigma \cdot BO_{ij}^\sigma \cdot f(BO_{ij}^\sigma) - D_e^\pi \cdot BO_{ij}^\pi - D_e^{\pi\pi} \cdot BO_{ij}^{\pi\pi}$$

Image removed due to copyright restrictions.
Please see slide 10 in van Duin, Adri. "Dishing Out the Dirt on ReaxFF."
<http://www.wag.caltech.edu/home/duin/FFgroup/Dirt.ppt>.

vdW interactions

$$E_{system} = E_{bond} + E_{vdWaal} + E_{Coulomb} + E_{val,angle} + E_{tors} + E_{over} + E_{under}$$

- Accounts for short distance repulsion (Pauli principle orthogonalization) and attraction energies at large distances (dispersion)
- Included for all atoms with shielding at small distances

$$E_{vdWaal} = D_{ij} \cdot \left\{ \exp \left[\alpha_{ij} \cdot \left(1 - \frac{f_{13}(r_{ij})}{r_{vdW}} \right) \right] - 2 \cdot \exp \left[\frac{1}{2} \cdot \alpha_{ij} \cdot \left(1 - \frac{f_{13}(r_{ij})}{r_{vdW}} \right) \right] \right\}$$

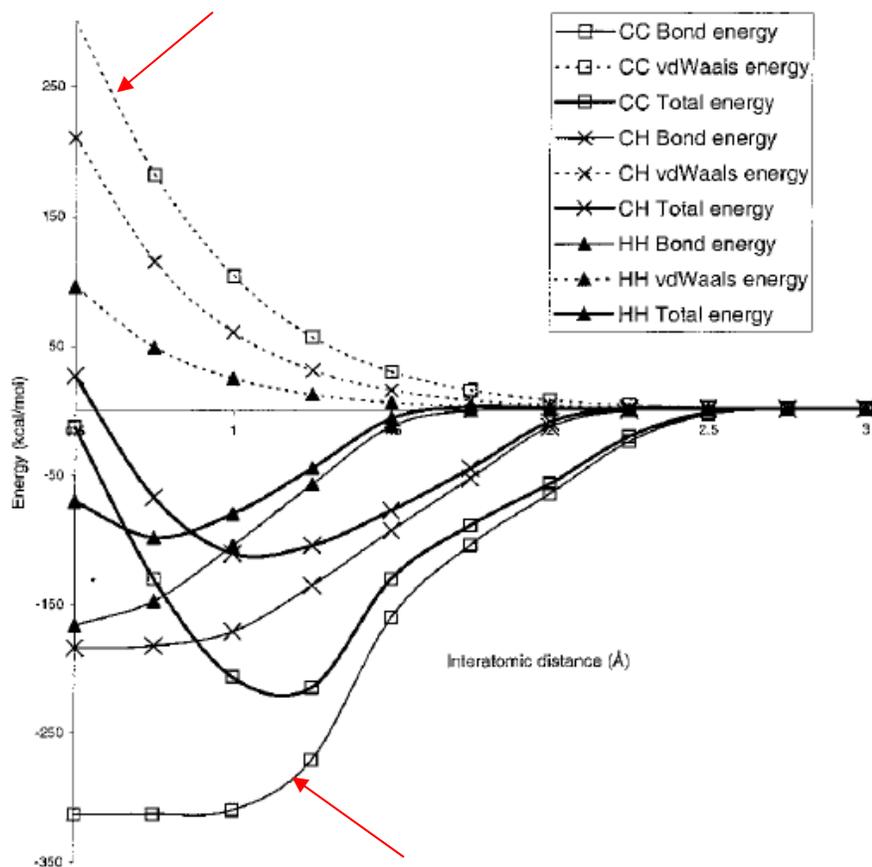
$$f_{13}(r_{ij}) = \left[r_{ij}^{\lambda_{29}} + \left(\frac{1}{\lambda_w} \right)^{\lambda_{28}} \right]^{1/\lambda_{28}}$$

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Please see slide 11 in van Duin, Adri. "Dishing Out the Dirt on ReaxFF."

<http://www.wag.caltech.edu/home/duin/FFgroup/Dirt.ppt>.

Resulting energy landscape



Contribution of E_{bond} and vdW energy

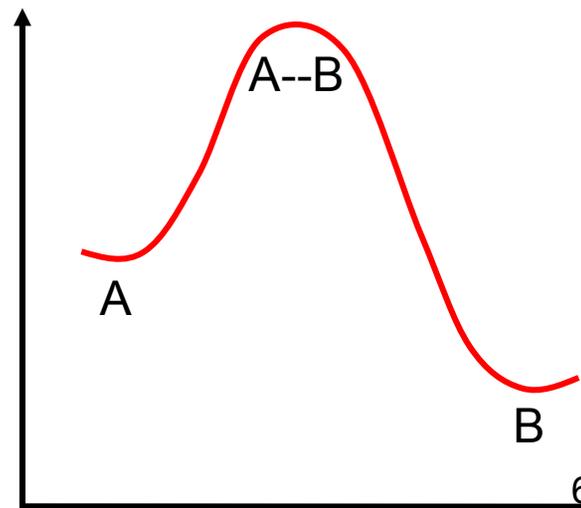
Current development status of ReaxFF

| Group → | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
|----------|----------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|------------|------------|------------|------------|---------|
| ↓ Period | | | | | | | | | | | | | | | | | | | |
| 1 | 1 H | | | | | | | | | | | | | | | | | | 2 He |
| 2 | 3 Li | 4 Be | | | | | | | | | | | 5 B | 6 C | 7 N | 8 O | 9 F | 10 Ne | |
| 3 | 11 Na | 12 Mg | | | | | | | | | | | 13 Al | 14 Si | 15 P | 16 S | 17 Cl | 18 Ar | |
| 4 | 19 K | 20 Ca | 21 Sc | 22 Ti | 23 V | 24 Cr | 25 Mn | 26 Fe | 27 Co | 28 Ni | 29 Cu | 30 Zn | 31 Ga | 32 Ge | 33 As | 34 Se | 35 Br | 36 Kr | |
| 5 | 37 Rb | 38 Sr | 39 Y | 40 Zr | 41 Nb | 42 Mo | 43 Tc | 44 Ru | 45 Rh | 46 Pd | 47 Ag | 48 Cd | 49 In | 50 Sn | 51 Sb | 52 Te | 53 I | 54 Xe | |
| 6 | 55 Cs | 56 Ba | La | 72 Hf | 73 Ta | 74 W | 75 Re | 76 Os | 77 Ir | 78 Pt | 79 Au | 80 Hg | 81 Tl | 82 Pb | 83 Bi | 84 Po | 85 At | 86 Rn | |
| 7 | 87 Fr | 88 Ra | Ac | 104 Rf | 105 Db | 106 Sg | 107 Bh | 108 Hs | 109 Mt | 110 Ds | 111 Rg | 112 Uub | 113 Uut | 114 Uuq | 115 Uup | 116 Uuh | 117 Uus | 118 Uuo | |



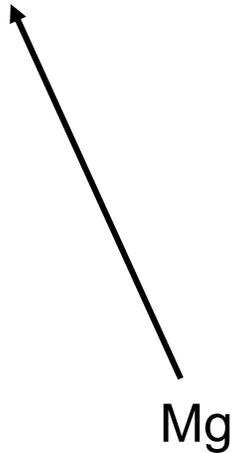
: not currently described by ReaxFF

Allows to interface metals, ceramics with organic chemistry: Key for complex materials, specifically biological materials

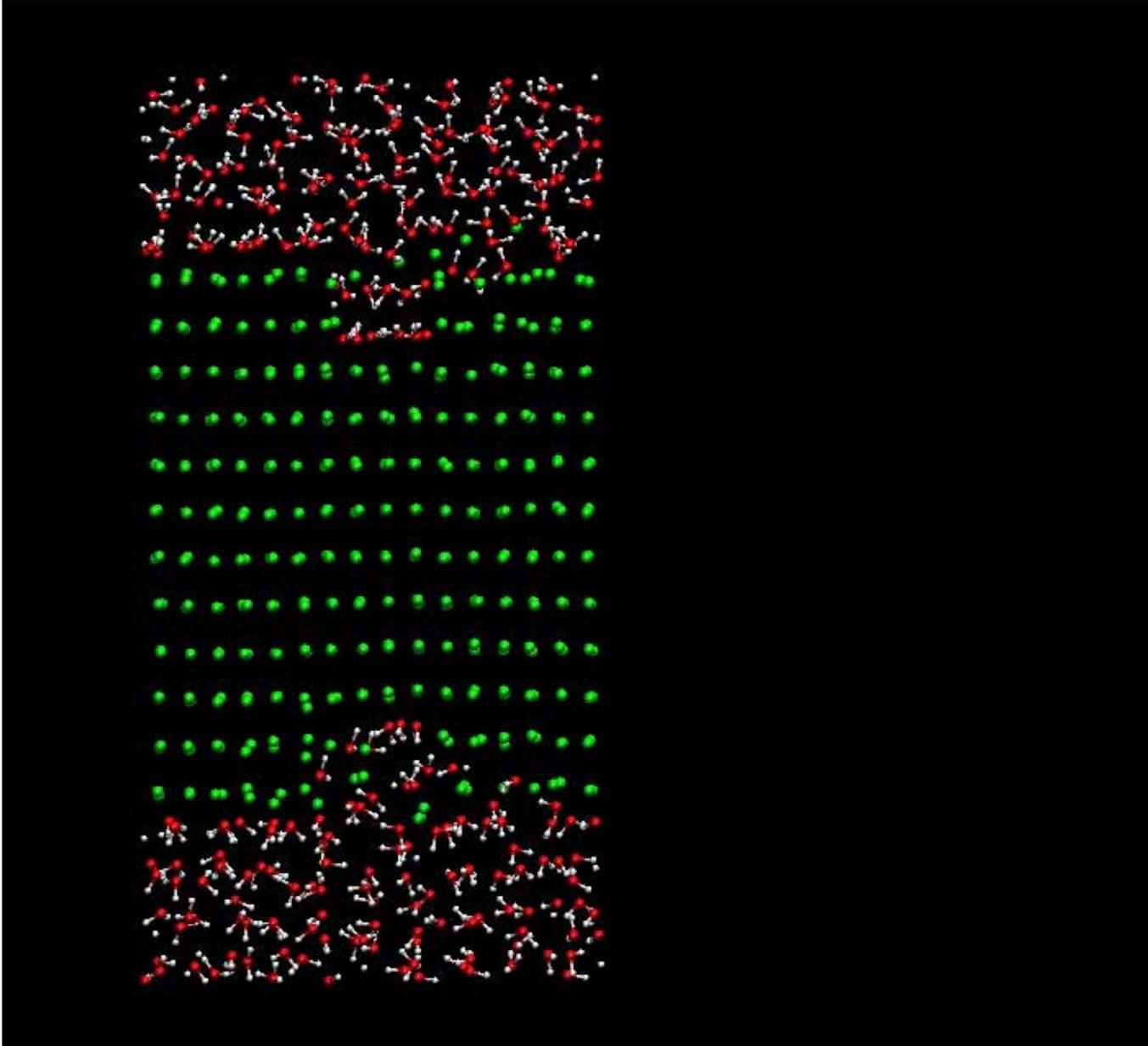


Mg-water interaction: How to make fire with water

Video stills removed due to copyright restrictions; watch the video now:
<http://www.youtube.com/watch?v=QTKivMVUcqE>.



Mg – water interaction – ReaxFF MD simulation



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3.021J / 1.021J / 10.333J / 18.361J / 22.00J Introduction to Modeling and Simulation
Spring 2012

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