



Engineering Risk Benefit Analysis

**1.155, 2.943, 3.577, 6.938, 10.816, 13.621, 16.862, 22.82,
ESD.72, ESD.721**

RPRA 5. Data Analysis

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Statistical Inference

Theoretical Model

Failure distribution,
e.g., $f(t) = \lambda e^{-\lambda t}$

Evidence

Sample, e.g.,
 $\{t_1, \dots, t_n\}$

- How do we estimate λ from the evidence?
- How confident are we in this estimate?
- Two methods:
 - *Classical (frequentist) statistics*
 - *Bayesian statistics*



Random Samples

- The observed values are independent and the underlying distribution is constant.

- Sample mean:
$$\bar{t} = \frac{1}{n} \sum_{1}^n t_i$$

- Sample variance:
$$s^2 = \frac{1}{(n-1)} \sum_{1}^n (t_i - \bar{t})^2$$



The Method of Moments: Exponential Distribution

- Set the theoretical moments equal to the sample moments and determine the values of the parameters of the theoretical distribution.

- *Exponential distribution:* $\frac{1}{\lambda} = \bar{t}$

Sample: {10.2, 54.0, 23.3, 41.2, 73.2, 28.0} hrs

$$\bar{t} = \frac{1}{6}(10.2 + 54 + 23.3 + 41.2 + 73.2 + 28) = \frac{229.9}{6} = 38.32$$

$$\text{MTTF} = 38.32 \quad \text{hrs;}$$

$$\lambda = \frac{1}{38.32} = 0.026 \quad \text{hr}^{-1}$$



The Method of Moments: Normal Distribution

- **Sample: {5.5, 4.7, 6.7, 5.6, 5.7}**

$$\bar{x} = \frac{(5.7 + 4.7 + 6.7 + 5.6 + 5.7)}{5} = \frac{28.4}{5} = 5.68 = \mu$$

$$\sum_1^5 (x_i - \bar{x})^2 = (5.5 - 5.68)^2 + \dots + (5.7 - 5.68)^2 = 2.032$$

$$s^2 = \frac{2.032}{(5 - 1)} = 0.508$$
$$s = 0.713 = \sigma$$



The Method of Moments: Poisson Distribution

- Sample: {r events in t}

- Average number of events: $\lambda t = r$

$$\lambda t = r \quad \Rightarrow \quad \lambda = \frac{r}{t}$$

- {3 eqs in 7 years} $\Rightarrow \lambda = \frac{3}{7} = 0.43 \text{ yr}^{-1}$



The Method of Moments: Binomial Distribution

- **Sample:** {k 1s in n trials}
- **Average number of 1s:** k
- $qn = k \Rightarrow q = \frac{k}{n}$
- {3 failures to start in 17 tests} $q = \frac{3}{17} = 0.176$



Censored Samples and the Exponential Distribution

- *Complete sample*: All n components fail.
- *Censored sample*: Sampling is terminated at time t_0 (with k failures observed) or when the r^{th} failure occurs.
- Define the *total operational time* as:

$$T = \sum_1^k t_i + (n - k)t_0$$

$$T = \sum_1^r t_i + (n - r)t_r$$

- It can be shown that: $\lambda = \frac{k}{T}$ or $\lambda = \frac{r}{T}$
- Valid for the exponential distribution only (no memory).



Example

- **Sample: 15 components are tested and the test is terminated when the 6th failure occurs.**
- **The observed failure times are:
{10.2, 23.3, 28.0, 41.2, 54.0, 73.2} hrs**
- **The total operational time is:**

$$T = 10.2 + 23.3 + 28 + 41.2 + 54 + 73.2 + (15 - 6)73.2 = 888.7$$

- **Therefore** $\lambda = \frac{6}{888.7} = 6.75 \times 10^{-3} \text{ hr}^{-1}$



Bayesian Methods

- Recall Bayes' Theorem (slide 16, RPRA 2):

Likelihood of the Evidence

Prior Probability

$$P(H_i/E) = \frac{P(E/H_i)P(H_i)}{\sum_1^N P(E/H_i)P(H_i)}$$

Posterior Probability

- Prior information can be utilized via the prior distribution.
- Evidence other than statistical can be accommodated via the likelihood function.



The Model of the World

- **Deterministic**, e.g., a mechanistic computer code
- **Probabilistic (Aleatory)**, e.g., $R(t/\lambda) = \exp(-t/\lambda)$
- The MOW deals with observable quantities.
- Both deterministic and aleatory models of the world have assumptions and parameters.
- How confident are we about the validity of these assumptions and the numerical values of the parameters?



The Epistemic Model

- **Uncertainties in assumptions are not handled routinely. If necessary, sensitivity studies are performed.**
- **The epistemic model deals with non-observable quantities.**
- **Parameter uncertainties are reflected on appropriate probability distributions.**
- **For the failure rate: $\pi(\lambda) d\lambda = \text{Pr}(\text{the failure rate has a value in } d\lambda \text{ about } \lambda)$**

Unconditional (predictive) probability

$$\mathbf{R}(\mathbf{t}) = \int \mathbf{R}(\mathbf{t} / \lambda) \pi(\lambda) d\lambda$$

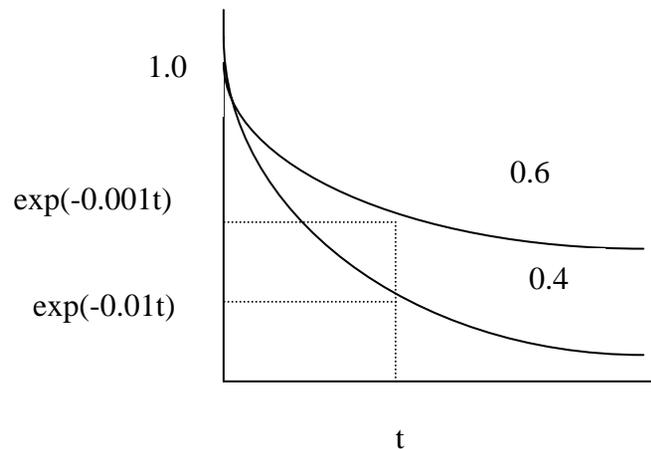


Communication of Epistemic Uncertainties: The discrete case

Suppose that $P(\lambda = 10^{-2}) = 0.4$ and $P(\lambda = 10^{-3}) = 0.6$

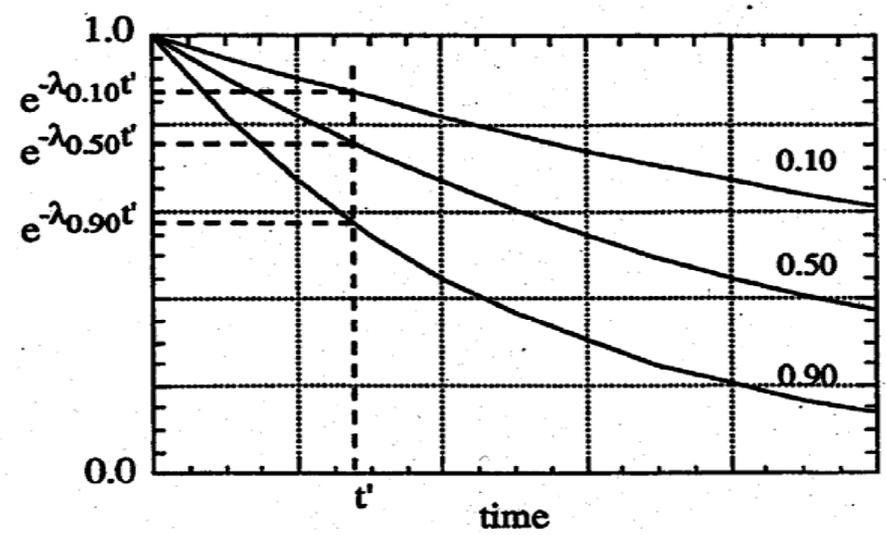
Then, $P(e^{-0.001t}) = 0.6$ and $P(e^{-0.01t}) = 0.4$

$$R(t) = 0.6 e^{-0.001t} + 0.4 e^{-0.01t}$$





Communication of Epistemic Uncertainties: The continuous case





Risk Curves

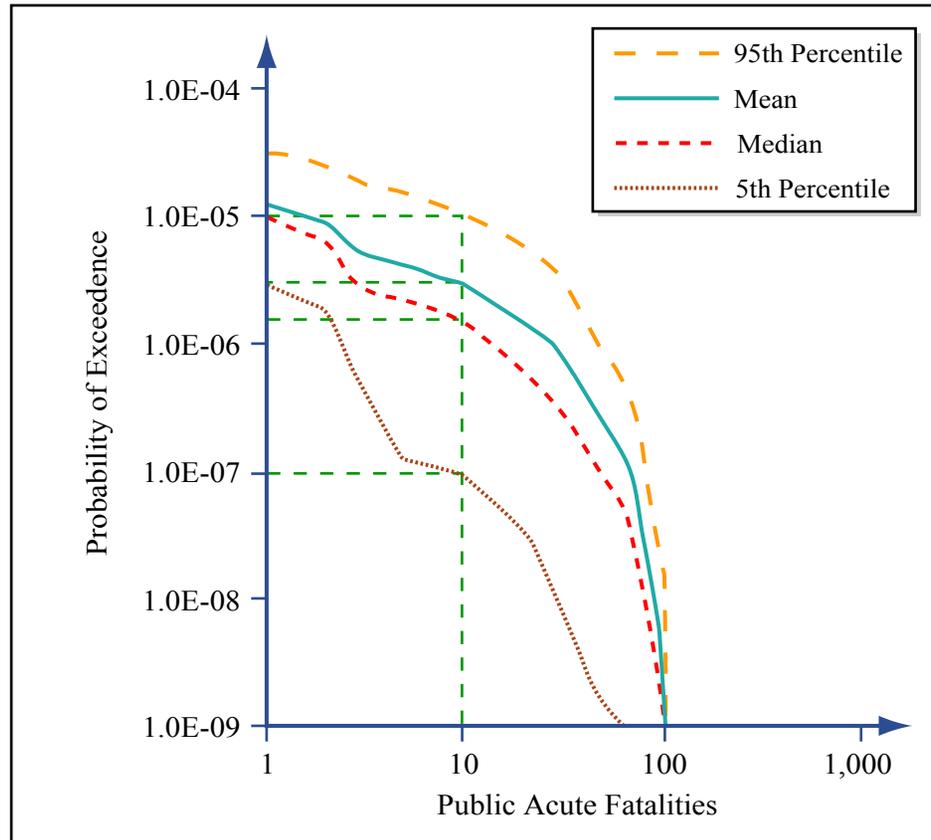


Figure by MIT OCW.



The Quantification of Judgment

- **Where does the epistemic distribution $\pi(\lambda)$ come from?**
- **Both substantive and normative “goodness” are required.**
- **Direct assessments of parameters like failure rates should be avoided.**
- **A reasonable measure of central tendency to estimate is the median.**
- **Upper and lower percentiles can also be estimated.**

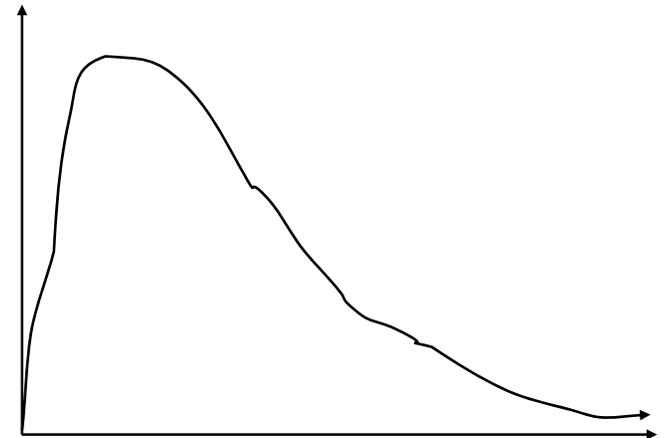
The lognormal distribution

- It is very common to use the lognormal distribution as the epistemic distribution of failure rates.

$$\pi(\lambda) = \frac{1}{\sqrt{2\pi\sigma\lambda}} \exp\left[-\frac{(\ln \lambda - \mu)^2}{2\sigma^2}\right]$$

$$\text{UB} = \lambda_{95} = \exp(\mu + 1.645\sigma)$$

$$\text{LB} = \lambda_{05} = \exp(\mu - 1.645\sigma)$$





| Mechanical Hardware | | |
|--|------------------------|-----------------------|
| Component/Primary Failure Modes | Assessed Values | |
| | Lower Bound | Upper Bound |
| Pumps | | |
| Failure to start, Q_d : | $3 \times 10^{-4}/d$ | $3 \times 10^{-3}/d$ |
| Failure to run, λ_o : (Normal Environments) | $3 \times 10^{-6}/hr$ | $3 \times 10^{-4}/hr$ |
| Valves | | |
| <i>Motor Operated</i> | | |
| Failure to operate, Q_d : | $3 \times 10^{-4}/d$ | $3 \times 10^{-3}/d$ |
| Plug, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| <i>Solenoid Operated</i> | | |
| Failure to operate, Q_d : | $3 \times 10^{-4}/d$ | $3 \times 10^{-3}/d$ |
| Plug, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| <i>Air Operated</i> | | |
| Failure to operate, Q_d : | $1 \times 10^{-4}/d$ | $1 \times 10^{-3}/d$ |
| Plug, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| <i>Check</i> | | |
| Failure to open, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| <i>Relief</i> | | |
| Failure to open, Q_d : | $3 \times 10^{-6}/d$ | $3 \times 10^{-5}/d$ |
| <i>Manual</i> | | |
| Plug, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| Pipe | | |
| <i>Plug/rupture</i> | | |
| < 3" diameter, λ_o : | $3 \times 10^{-11}/hr$ | $3 \times 10^{-8}/hr$ |
| > 3" diameter, λ_o : | $3 \times 10^{-12}/hr$ | $3 \times 10^{-9}/hr$ |
| Clutches | | |
| <i>Mechanical</i> | | |
| Failure to engage/disengage | $1 \times 10^{-4}/d$ | $1 \times 10^{-3}/d$ |

Table by MIT OCW.

Adapted from Rasmussen, et al.
 "The Reactor Safety Study."
 WASH-1400, US Nuclear Regulatory
 Commission, 1975.



| Electrical Hardware | | |
|---|-----------------------|-----------------------|
| Component/Primary Failure Modes | Assessed Values | |
| | Lower Bound | Upper Bound |
| Electrical Clutches | | |
| Failure to operate, Q_d : | $1 \times 10^{-4}/d$ | $1 \times 10^{-3}/d$ |
| Motors | | |
| Failure to start, Q_d : | $1 \times 10^{-4}/d$ | $1 \times 10^{-3}/d$ |
| Failure to run (Normal Environments), λ_o : | $3 \times 10^{-6}/hr$ | $3 \times 10^{-5}/hr$ |
| Transformers | | |
| Open/shorts, λ_o : | $3 \times 10^{-7}/hr$ | $3 \times 10^{-6}/hr$ |
| Relays | | |
| Failure to energize, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| Circuit Breaker | | |
| Failure to transfer, Q_d : | $3 \times 10^{-4}/d$ | $3 \times 10^{-3}/d$ |
| Limit Switches | | |
| Failure to operate, Q_d : | $1 \times 10^{-4}/d$ | $1 \times 10^{-3}/d$ |
| Torque Switches | | |
| Failure to operate, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| Pressure Switches | | |
| Failure to operate, Q_d : | $3 \times 10^{-5}/d$ | $3 \times 10^{-4}/d$ |
| Manual Switches | | |
| Failure to operate, Q_d : | $3 \times 10^{-6}/d$ | $3 \times 10^{-5}/d$ |
| Battery Power Supplies | | |
| Failure to provide proper output, λ_s : | $1 \times 10^{-6}/hr$ | $1 \times 10^{-5}/hr$ |
| Solid State Devices | | |
| Failure to function, λ_o : | $3 \times 10^{-7}/hr$ | $3 \times 10^{-5}/hr$ |
| Diesels (complete plant) | | |
| Failure to start, Q_d : | $1 \times 10^{-2}/d$ | $1 \times 10^{-1}/d$ |
| Failure to run, λ_o : | $3 \times 10^{-4}/hr$ | $3 \times 10^{-2}/hr$ |
| Instrumentation | | |
| Failure to operate, λ_o : | $1 \times 10^{-7}/hr$ | $1 \times 10^{-5}/hr$ |

- All values are rounded to the nearest half order of magnitude on the exponent.
- Derived from averaged data on pumps, combining standby and operate time.
- Approximated from plugging that was detected.
- Derived from combined standby and operate data.
- Derived from standby test on batteries, which does not include load.

Table by MIT OCW.

Adapted from Rasmussen, et al. "The Reactor Safety Study." WASH-1400, US Nuclear Regulatory Commission, 1975.



Example

Lognormal prior distribution with median and 95th percentile given as:

$$\lambda_{50} = \exp(\mu) = 3 \times 10^{-3} \text{ hr}^{-1}$$

$$\lambda_{95} = \exp(\mu + 1.645\sigma) = 3 \times 10^{-2} \text{ hr}^{-1}$$

Then $\mu = -5.81, \quad \sigma = 1.40$

$$E[\lambda] = \exp\left(\mu + \frac{\sigma^2}{2}\right) = 8 \times 10^{-3} \text{ hr}^{-1}$$

$$\lambda_{05} = \exp(\mu - 1.645\sigma) = 3 \times 10^{-4} \text{ hr}^{-1}$$



Updating Epistemic Distributions

- **Bayes' Theorem allows us to incorporate new evidence into the epistemic distribution.**

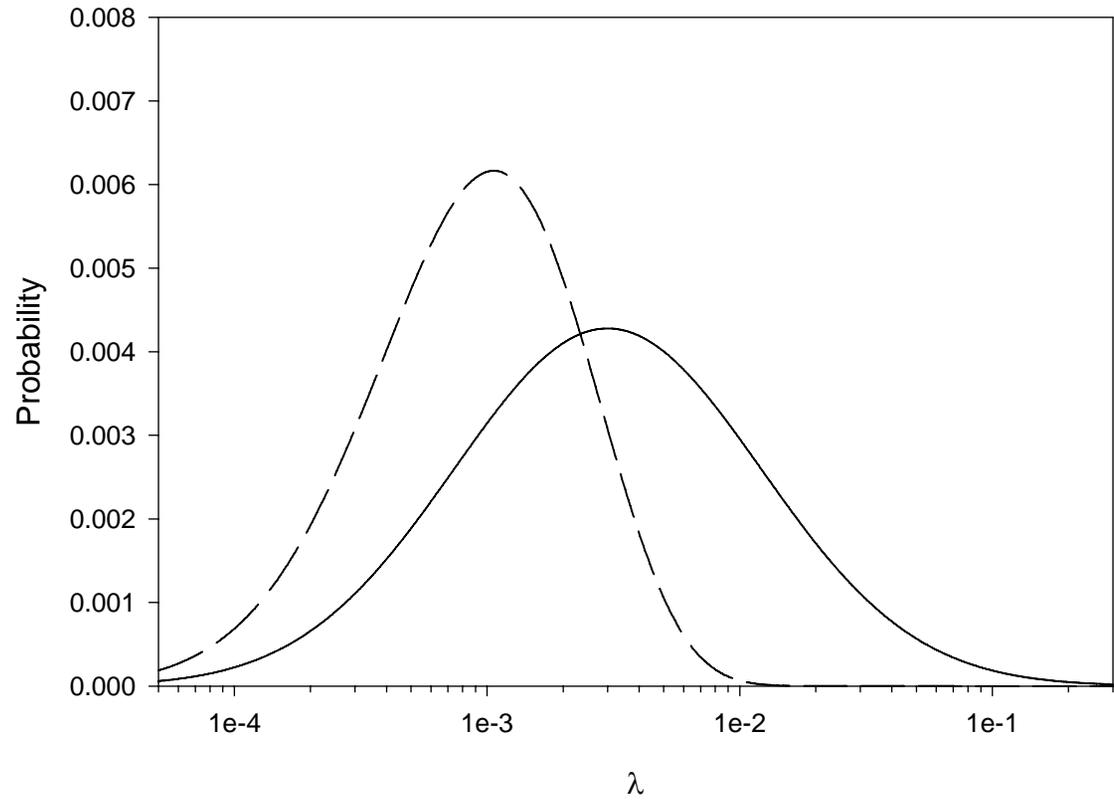
$$\pi'(\lambda / \mathbf{E}) = \frac{\mathbf{L}(\mathbf{E} / \lambda)\pi(\lambda)}{\int \mathbf{L}(\mathbf{E} / \lambda)\pi(\lambda)d\lambda}$$

Example of Bayesian updating of epistemic distributions

- *Five components were tested for 100 hours each and no failures were observed.*
- *Since the reliability of each component is $\exp(-100 \lambda)$, the likelihood function is:*
- *$L(E/\lambda) = P(\text{comp. 1 did not fail } \underline{\text{AND}} \text{ comp. 2 did not fail } \underline{\text{AND}} \dots \text{ comp. 5 did not fail}) = \exp(-100\lambda) \times \exp(-100\lambda) \times \dots \times \exp(-100\lambda) = \exp(-500\lambda)$*
- *$L(E/\lambda) = \exp(-500\lambda)$*
 - *Note: The classical statistics point estimate is zero since no failures were observed.*



Prior (—) and posterior (-----) distributions





Impact of the evidence

| | Mean (hr⁻¹) | 95th (hr⁻¹) | Median (hr⁻¹) | 5th (hr⁻¹) |
|-----------------------------|--|--|--------------------------------------|---|
| Prior distr. | 8.0×10^{-3} | 3.0×10^{-2} | 3×10^{-3} | 3.0×10^{-3} |
| Posterior distr. | 1.3×10^{-3} | 3.7×10^{-3} | 9×10^{-4} | 1.5×10^{-4} |



Selected References

- *Proceedings of Workshop on Model Uncertainty: Its Characterization and Quantification*, A. Mosleh, N. Siu, C. Smidts, and C. Lui, Eds., Center for Reliability Engineering, University of Maryland, College Park, MD, 1995.
- *Reliability Engineering and System Safety*, Special Issue on the Treatment of Aleatory and Epistemic Uncertainty, J.C. Helton and D.E. Burmaster, Guest Editors., vol. 54, Nos. 2-3, Elsevier Science, 1996.
- Apostolakis, G., “The Distinction between Aleatory and Epistemic Uncertainties is Important: An Example from the Inclusion of Aging Effects into PSA,” *Proceedings of PSA '99, International Topical Meeting on Probabilistic Safety Assessment*, pp. 135-142, Washington, DC, August 22 - 26, 1999, American Nuclear Society, La Grange Park, Illinois.