

Massachusetts Institute of Technology

Department of Electrical Engineering and Computer Science  
6.245: MULTIVARIABLE CONTROL SYSTEMS

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## Problem Set 6 Solutions <sup>1</sup>

### Problem 6.1

A STANDARD FEEDBACK CONTROL DESIGN SETUP IS DEFINED BY THE DIFFERENTIAL EQUATIONS

$$\dot{x}_1 = -ax_1 + u, \quad \dot{x}_2 = -x_2 + w,$$

AND BY

$$y = w + bx_2, \quad z = \begin{bmatrix} cu \\ x_1 \end{bmatrix},$$

WHERE  $a, b, c$  ARE REAL PARAMETERS.

- (a) FIND MATRICES  $A, B_1, B_2, C_1, C_2, D_{11}, D_{12}, D_{21}, D_{22}$  FOR THIS SETUP.

By inspection,

$$A = \begin{bmatrix} -a & 0 \\ 0 & -1 \end{bmatrix}, \quad B_1 = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad B_2 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad C_1 = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix}, \quad C_2 = [0 \quad b],$$

$$D_{11} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \quad D_{12} = \begin{bmatrix} c \\ 0 \end{bmatrix}, \quad D_{21} = 1, \quad D_{22} = 0.$$

- (b) FIND ALL VALUES OF  $a, b, c$  FOR WHICH THE SETUP IS SINGULAR, INDICATING FREQUENCY, MULTIPLICITY, AND TYPE (CONTROL/SENSOR) OF THE SINGULARITY.

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Matrix

$$M_u(s) = \begin{bmatrix} -a - s & 0 & 1 \\ 0 & -1 - s & 0 \\ 0 & 0 & c \\ 1 & 0 & 0 \end{bmatrix}$$

is right invertible for all  $s = j\omega$ ,  $\omega \in \mathbf{R}$ . The largest degree of determinant of a 3-by-3 minor of  $M_u(s)$  equals  $d_u^\infty = 1$  when  $c = 0$ , and 2 otherwise. Hence, for  $c = 0$ , there is a control singularity at  $\omega = \infty$ , multiplicity 1 (the difference between system order and  $d_u^\infty$ ). For  $c \neq 0$ , there are no control singularities.

The determinant of

$$M_y(s) = \begin{bmatrix} -a - s & 0 & 0 \\ 0 & -1 - s & 1 \\ 0 & b & 1 \end{bmatrix}$$

equals

$$\delta_y(s) = \det(M_y(s)) = (s + a)(s + b + 1).$$

Hence, the system has sensor singularities only when  $a = 0$  or  $b = -1$ , in which case the singularity is located at  $\omega = 0$ , and its multiplicity 1 equals the multiplicity of the zero  $s = 0$  of  $\delta_y(s)$  (one unless  $a = b + 1 = 0$ , which implies multiplicity 2).

## Problem 6.2

FIND H-INFINITY AND H2 NORMS OF  $G(s) = G_a(s)$  AS A FUNCTION OF REAL PARAMETER  $a$ :

(a)  $G(s) = 1/(s + a) - 2/(s + 2a)$ ;

The impulse response  $g = g(t)$  of  $G$  is given by

$$g(t) = e^{-at} - 2e^{-2at}.$$

Since

$$\int_0^\infty |g(t)|^2 dt = \int_0^\infty \{e^{-2at} - 4e^{-3at} + 4e^{-4at}\} dt = \frac{1}{6a},$$

$$\|G\|_{H2} = 1/\sqrt{6a}.$$

Since

$$G(s) = -\frac{s}{s^2 + 3as + 2a^2} = -\frac{1}{3a + s + 2a^2/s},$$

we have  $|G(j\omega)| \geq 1/3a$ , where the equality takes place at  $\omega = \sqrt{2}a$ . Hence  $\|G\|_\infty = 1/3a$ .

(b)  $G(s) = (1 - \exp(-a^2s))/s$ .

The impulse response  $g = g(t)$  of  $G$  is given by

$$g(t) = \begin{cases} 1, & t \in [0, a^2], \\ 0, & \text{otherwise.} \end{cases}$$

Hence  $\|G\|_{H2} = a$ , and  $\|G\|_{\infty} = a^2$ .

### Problem 6.3

FIND L2 GAINS OF SYSTEMS DESCRIBED BELOW (INPUT  $f$ , OUTPUT  $g$ , DEFINED FOR  $t \geq 0$ ). YOU ARE NOT REQUIRED TO *prove* CORRECTNESS OF YOUR ANSWER.

(a)  $y(t) = e^{-at}f(t)$ .

L2 gain equals 1 for  $a \geq 0$ , and infinity for  $a < 0$ .

(b)  $y(t) = f(t)/(1 + a^2f(t)^2)$ .

L2 gain equals 1 for all  $a$ .

(c)  $y(t) = f(t + a)$ .

L2 gain equals 1 for  $a \leq 0$ , and infinity for  $a > 0$ .

### Problem 6.4

A STANDARD H2 OPTIMIZATION SETUP IS DEFINED BY THE FOLLOWING TRANSFER FUNCTIONS:

$$P_{wz}(s) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \quad P_{wy}(s) = 1, \quad P_{uz}(s) = \begin{bmatrix} 1/(s+a) \\ 1 \end{bmatrix}, \quad P_{uy}(s) = -1/(s+a),$$

WHERE  $a \in \mathbf{R}$  IS A PARAMETER. FOR ALL VALUES OF  $a$  FOR WHICH THE SETUP IS NON-SINGULAR, FIND THE H2 OPTIMAL CONTROLLER, TOGETHER WITH THE ASSOCIATED HAMILTONIAN MATRICES, SOLUTIONS OF RICCATI EQUATIONS, AND CONTROLLER/OBSERVER GAINS.

A state space model of the setup is given by

$$\dot{x} = -ax + u, \quad x(0) = x_0, \quad z = \begin{bmatrix} x \\ u \end{bmatrix}, \quad y = w - x.$$

The setup is non-singular for  $a \neq 0$  (when  $a = 0$ , there is a sensor singularity at  $\omega = 0$ ).

The full information abstract H2 optimization has the form

$$\dot{X} = -aX + U, \int_0^{\infty} (|X|^2 + |U|^2)dt \rightarrow \min.$$

The corresponding Hamiltonian matrix is

$$\mathcal{H}_{fi} = \begin{bmatrix} -a & 1 \\ 1 & a \end{bmatrix}.$$

The stabilizing solution of the associated Riccati equation is

$$P_{fi} = \sqrt{a^2 + 1} - a,$$

and the optimal full state feedback gain is given by

$$K_{fi} = a - \sqrt{a^2 + 1}.$$

The state estimation abstract H2 optimization has the form

$$\dot{\psi} = -a\psi - q, \psi(0) = \psi_0, \int_0^{\infty} |q|^2 dt \rightarrow \min.$$

The corresponding Hamiltonian matrix is

$$\mathcal{H}_{se} = \begin{bmatrix} -a & 1 \\ 0 & a \end{bmatrix}.$$

The stabilizing solution of the associated Riccati equation is

$$P_{se} = \begin{cases} 0, & \text{for } a > 0, \\ -2a, & \text{for } a < 0, \end{cases}$$

and the optimal state estimator gain is given by

$$L_{se} = \begin{cases} 0, & \text{for } a > 0, \\ -2a, & \text{for } a < 0. \end{cases}$$

For  $a > 0$ , the H2 optimal controller has zero transfer function. For  $a < 0$ , the H2 optimal controller can be written in the observer-based form

$$u = (a - \sqrt{a^2 + 1})\hat{x}, \quad \frac{d}{dt}\hat{x} = -a\hat{x} + u - 2a(-\hat{x} - y),$$

and its transfer function is

$$K(s) = \frac{2a(a - \sqrt{a^2 + 1})}{s + \sqrt{a^2 + 1} - 2a}.$$

### Problem 6.5

OPEN-LOOP PLANT  $P(s)$  IS STRICTLY PROPER, HAS A DOUBLE POLE AT  $s = 0$ , AND A ZERO AT  $s = 0.1$ . CONTROLLER  $C = C(s)$  STABILIZES THE SYSTEM ON FIGURE 6.1,

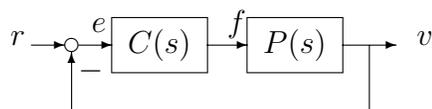


Figure 6.1: A SISO Feedback Setup

AND ENSURES GOOD TRACKING (TRANSFER FUNCTION FROM  $r$  TO  $e$  HAS GAIN LESS THAN 0.1) FOR FREQUENCIES UP TO 1 RAD/SEC. FIND A GOOD LOWER BOUND ON THE MAXIMAL GAIN FROM  $r$  TO  $e$ .

Let  $S$  denote the closed loop transfer function from  $r$  to  $e$ . Then, by assumption,  $S(0.1) = 1$ . Hence

$$\int_0^{\infty} \frac{\log |S(j\omega)| d\omega}{\omega^2 + 0.1^2} \geq 0.$$

Using the fact that  $|S(j\omega)| \leq 0.1$  for  $\omega \leq 1$ , and  $|S(j\omega)| \leq \|S\|_{\infty}$  for  $\omega \geq 1$ , we get

$$\log \|S\|_{\infty} \int_{10}^{\infty} \frac{d\omega}{\omega^2 + 1} \geq \log 10 \int_0^{10} \frac{d\omega}{\omega^2 + 1},$$

i.e.

$$\|S\|_{\infty} \geq 10^{\frac{\arctan(10)}{\pi/2 - \arctan(10)}} \geq 10^{14.76}.$$

### Problem 6.6

FIND THE SQUARE OF THE H2 NORM OF

$$G(s) = \frac{s}{s^2 + a_1 s + a_0}$$

AS A RATIONAL FUNCTION OF REAL PARAMETERS  $a_1, a_0$ .

A state space model of  $G$  is given by

$$A = \begin{bmatrix} 0 & 1 \\ -a_0 & -a_1 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad C = [0 \quad 1], \quad D = 0.$$

The solution  $P$  of the Lyapunov equation

$$AP + PA' = -BB'$$

has the form

$$P = \begin{bmatrix} 1/2a_0a_1 & 0 \\ 0 & 1/2a_1 \end{bmatrix}.$$

Hence

$$\|G\|_{H_2} = \sqrt{CPC'} = \frac{1}{\sqrt{2a_1}}.$$