

## LECTURE #5

### 1.060 ENGINEERING MECHANICS II

Fluid at rest  $\Rightarrow \vec{q} = \text{velocity vector} = (u, v, w) = 0$

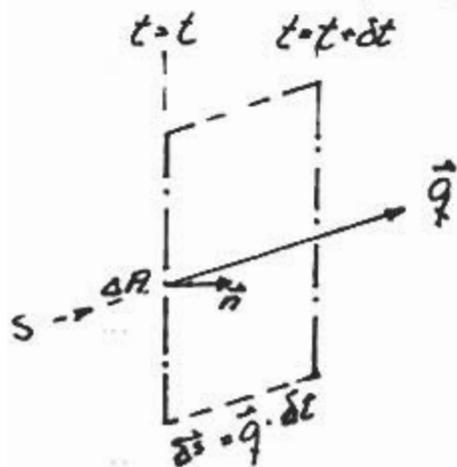
HYDROSTATICS : Been there - done that

Fluid in motion is described by its velocity field

$$\vec{q}(x, y, z, t) = \lim_{\delta t \rightarrow 0} (\delta x_p, \delta y_p, \delta z_p) / \delta t = \lim_{\delta t \rightarrow 0} (\vec{\delta s} / \delta t)$$

where

$\vec{\delta s}$  = infinitesimally small displacement vector along the streamline passing through  $(x, y, z)$  at time  $t$ .



$\Delta A$  = elementary area over which

$\vec{q}$  and  $\rho$  are  $\approx$  constant

$\vec{n}$  = unit vector  $\perp \Delta A$

$$q_{\perp} = \vec{q} \cdot \vec{n} = \text{velocity component } \perp \Delta A$$

$$\Delta V = \text{volume between } \Delta A \text{ at } t \text{ and } t + \Delta t = (q_{\perp} \Delta t) \Delta A$$

This volume,  $\Delta V$ , must have been supplied by the flow through  $\Delta A$  at  $t = t$ .

Volume flow rate per unit area = Volume flux =  $(\Delta V / \Delta t) / \Delta A = q_L \Delta t \Delta A / (\Delta t \Delta A) = q_L = \vec{q} \cdot \vec{n}$

Mass flow rate per unit area = Mass flux = [Volume flux][mass/volume] =  $\dot{m} = \rho q_L = \rho \vec{q} \cdot \vec{n}$

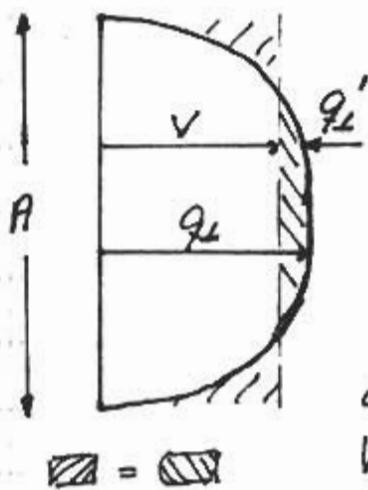
If flow area  $A$  is much larger than  $\Delta A$ , so that neither  $\rho$  nor  $\vec{q}$  can be considered constant over  $A$ , we have

Rate of Mass Flow across  $A = \sum \dot{m} \Delta A = \dot{m} = \int_A \rho q_L dA = \int_A \rho \vec{q} \cdot \vec{n} dA$

Rate of Volume Flow across  $A = \sum q_L \Delta A = Q = \int_A q_L dA = \int_A \vec{q} \cdot \vec{n} dA$

If  $\rho = \text{constant}$

$$\dot{m} = \rho Q$$



$$Q = \text{discharge (m}^3/\text{s)} = \int_A q_L dA = VA$$

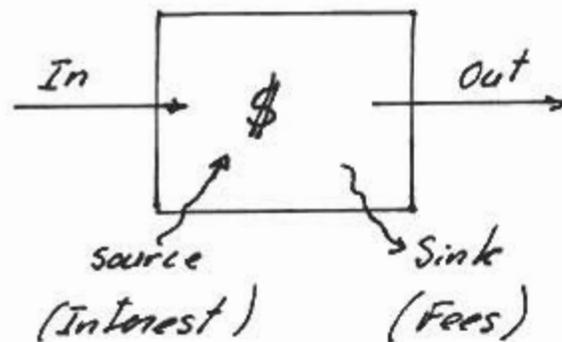
$$V = \frac{Q}{A} = \text{AVERAGE VELOCITY OVER } A$$

If  $q_L = V + q_L'$  then  $\int q_L' dA = 0$  and if  $q_L' \ll V$  over most of  $A$ ,  $V$  may be considered to represent  $q_L$  quite well.

## NATURE OF CONSERVATION LAWS

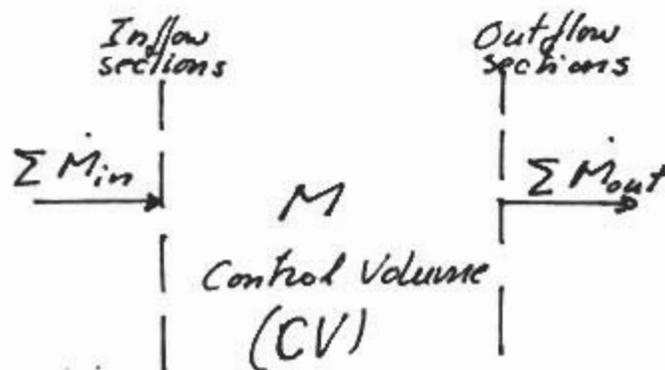
Conservation laws are analogous to a  
BANK ACCOUNT :

"In" minus "Out" = "Rate of Change Within"  
Deposit Account      Withdrawal



$$\Delta \$ = \Delta \$_{\text{deposit}} - \Delta \$_{\text{withdrawal}} + \Delta \$_{\text{interest (source)}} - \Delta \$_{\text{fees (sink)}}$$

## CONSERVATION OF MASS

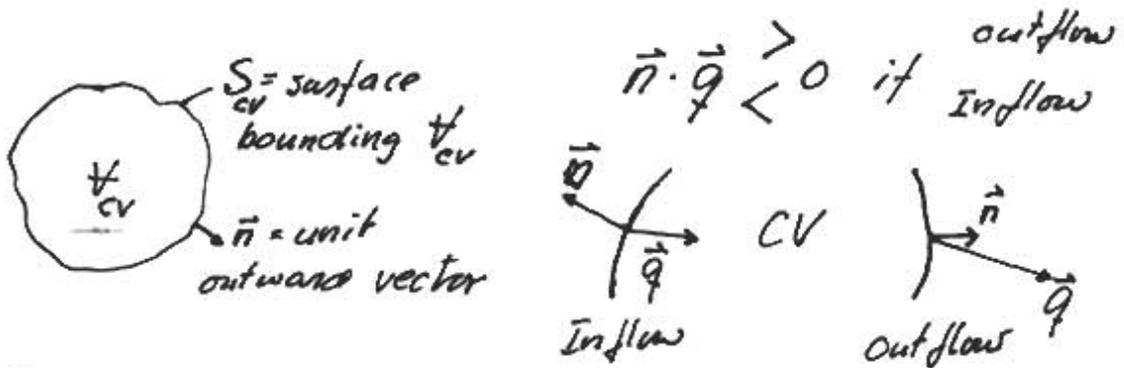


$$\sum \dot{M}_{in} - \sum \dot{M}_{out} = \text{Net rate of mass in} =$$

$$\frac{\partial M}{\partial t} = \text{Rate of change of mass within CV.}$$

(for mass - no source or sinks)

$$\sum_{\text{inflow areas}} [\int \rho \vec{q}_L dA] - \sum_{\text{outflow areas}} [\int \rho \vec{q}_L dA] = \frac{\partial}{\partial t} [\int_{V_{cv}} \rho dV]$$



Compact expression:

$$\frac{\partial}{\partial t} \int_{V_{cv}} \rho dV + \int_{S_{cv}} \rho \vec{q} \cdot \vec{n} dS = 0 \quad (1)$$

CONSERVATION OF VOLUME (Continuity)

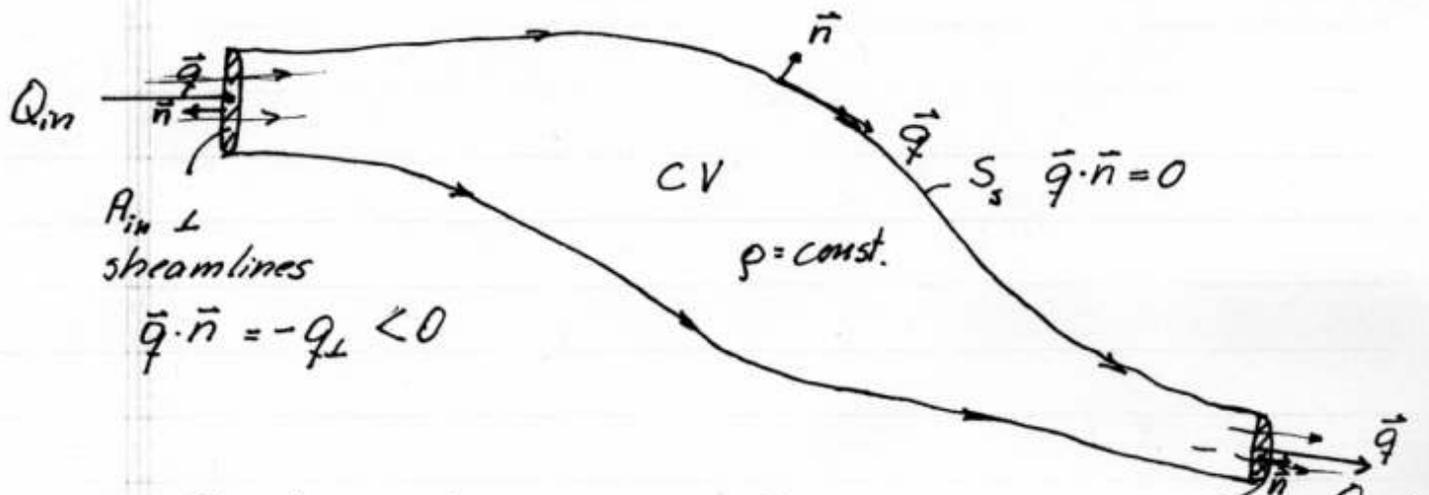
$$\sum Q_{in} - \sum Q_{out} = \frac{\partial V_{cv}}{\partial t} = \frac{\partial}{\partial t} \left[ \int_{V_{cv}} dV \right]$$

or, in compact form

$$\frac{\partial V_{cv}}{\partial t} + \int_{S_{cv}} \vec{q} \cdot \vec{n} dS = 0 \quad (2)$$

For a homogeneous fluid of constant density,  $\rho$  cancels out in (1) and it becomes (2). BUT (2) holds for any incompressible fluid [one whose volume remains the same regardless of Temperature and Pressure] whether  $\rho$  is constant or not.

## The Stream Tube



Surface bounding CV consists of  $S_s =$  streamline "walls" and flow cross-sections  $A$

$$\frac{\partial \mathcal{H}_{cv}}{\partial t} + \int_A \vec{q} \cdot \vec{n} dA = \frac{\partial \mathcal{H}_{cv}}{\partial t} + Q_{out} - Q_{in} = 0$$

If flow is steady:  $\partial \mathcal{H}_{cv} / \partial t = 0$  and

$$Q = Q_{in} = Q_{out} = \text{Constant along Stream Tube}$$

or

$$Q = VA = \text{const} \Rightarrow V = \frac{Q}{A}$$

$V$  is large where  $A$  (area of stream tube) is small and vice versa.  
(This should be called the da Vinci Principle!)