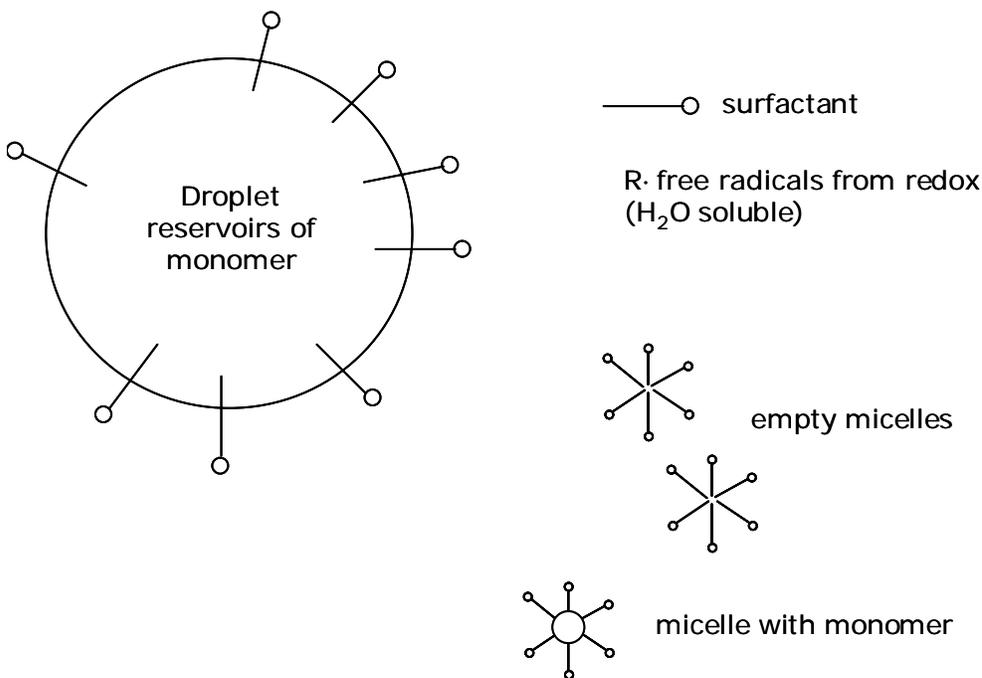


Lecture 15: Processing Approaches: Suspension (bead) Polymerization Processes, Polyvinyl Chloride via Precipitation Polymerization, Polyethylene via Radical Polymerization



Rate of conversion, emulsion polymerization

$$\bar{\rho}_n = k_p[M]\Delta t = k_p[M]\frac{n}{\rho}$$

In general,

$$R_p = \frac{n}{2}$$

$$-\frac{dm}{dt} = \frac{1}{2}k_p[M]$$

$$R_p = \frac{n}{2}k_p[M]$$

ρ (radicals)

$$\bar{\rho}_n = k_p[M]\Delta t = k_p[M]\frac{n}{\rho}$$

handout

Emulsion Polymerization: monomer → porous particles

introduce plasticizer
more readily processible, aerodyn. in powder form

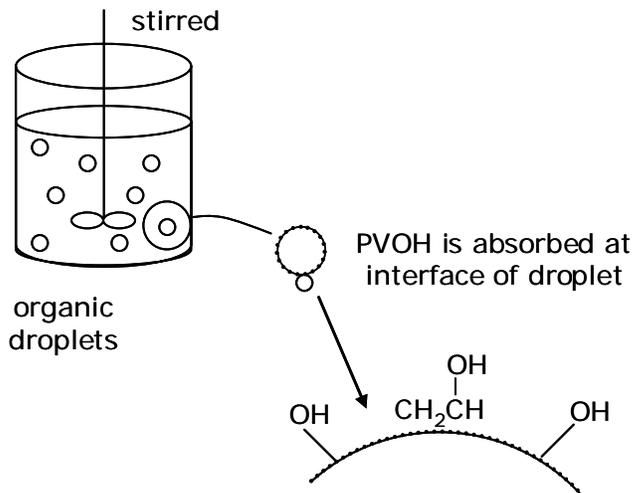
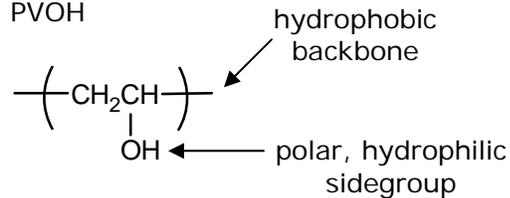
Common emulsion polymers:
styrene + copolymers
vinyl chlorides ex. Pleather
butadiene
vinylidene chloride
vinyl acetate
vinyl acrylates (acrylics)
methyl acrylates

Advantages:
- low η (viscosity)
- great T control
- final product \rightarrow fine powder
or water form \Rightarrow coatings

Disadvantages:
- a lot of soap as impurity
ex. In medical applications, can be irritant

Suspension Polymerization:

(Pearl of Bead)
"Ingredients"
monomer – organic phase
aqueous phase
initiator (soluble in monomer phase)
stabilizer, often a polymer, such as PVOH



much more soluble in water

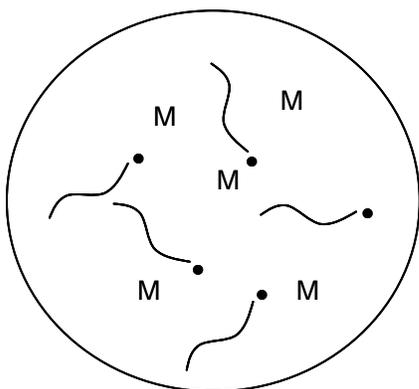
Organic droplets: $\sim 1 \mu\text{m} - 1 \text{cm}$
 Drop size determined by impeller speed
 Within each droplet, have

- initiator
- monomer

⇒ Batch reactor within droplet

Kinetics are identical to typical large scale free radical polymerization

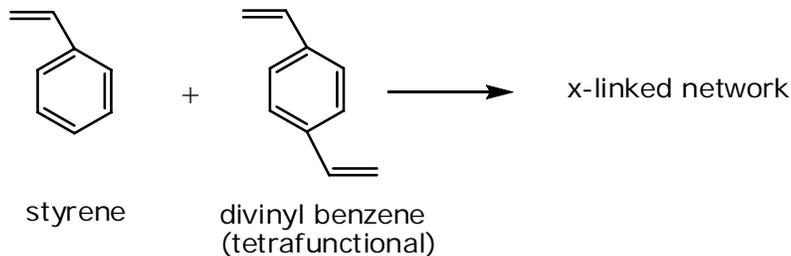
- initiation
- propagation
- termination
- steady state assumption



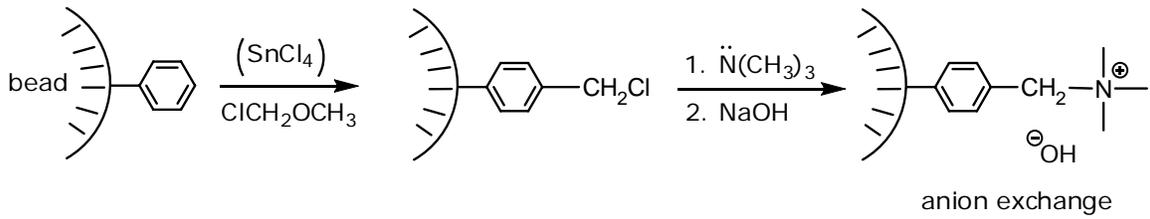
Concerned with avoiding drop coalescence
 → premix initiator + monomer
 → agitate H₂O phase + add organic phase
 $\sim 20 - 30 \%$ vol
 → adjust impellar speed to get desired drop size
 → add stabilizer (PVOH)
 → continue stirring at more gentle speed and
 increase T to $40^\circ\text{C} \rightarrow 80^\circ\text{C}$ depending on which
 initiator you're using
 → initiator activation
 → go to near complete conversion
 (may need to increase T for final % π)

Products:

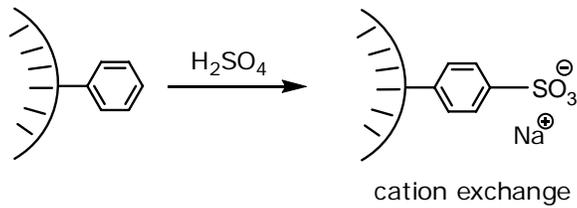
- glassy rigid beads often called "latex beads"
- very uniform
- nice spherical shapes



vary surface chain:



or



Form Pores:

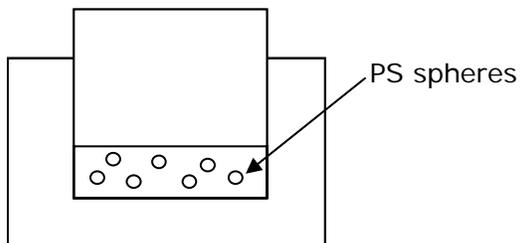
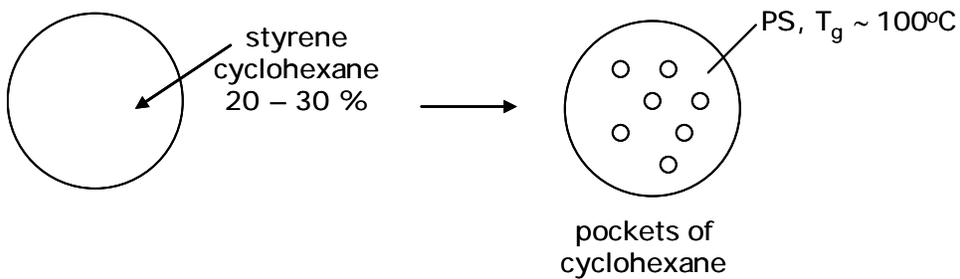
- add non-solvent + monomer w/organic phase



Form connected channels of non-solvent

→ go to high π
flash off non solvent

If monomer (e.g. styrene) is well-dissolved in solvent, but solvent is poor for high MW polymer (e.g. cyclohexane)



Increase T to 120°C
 ⇒ expansion – foaming effect
 → very large increases in size and decreases in density (mostly air)
 ⇒ STYROFOAM®

The following figures are adapted from page 250 of *Polymer Synthesis*:¹

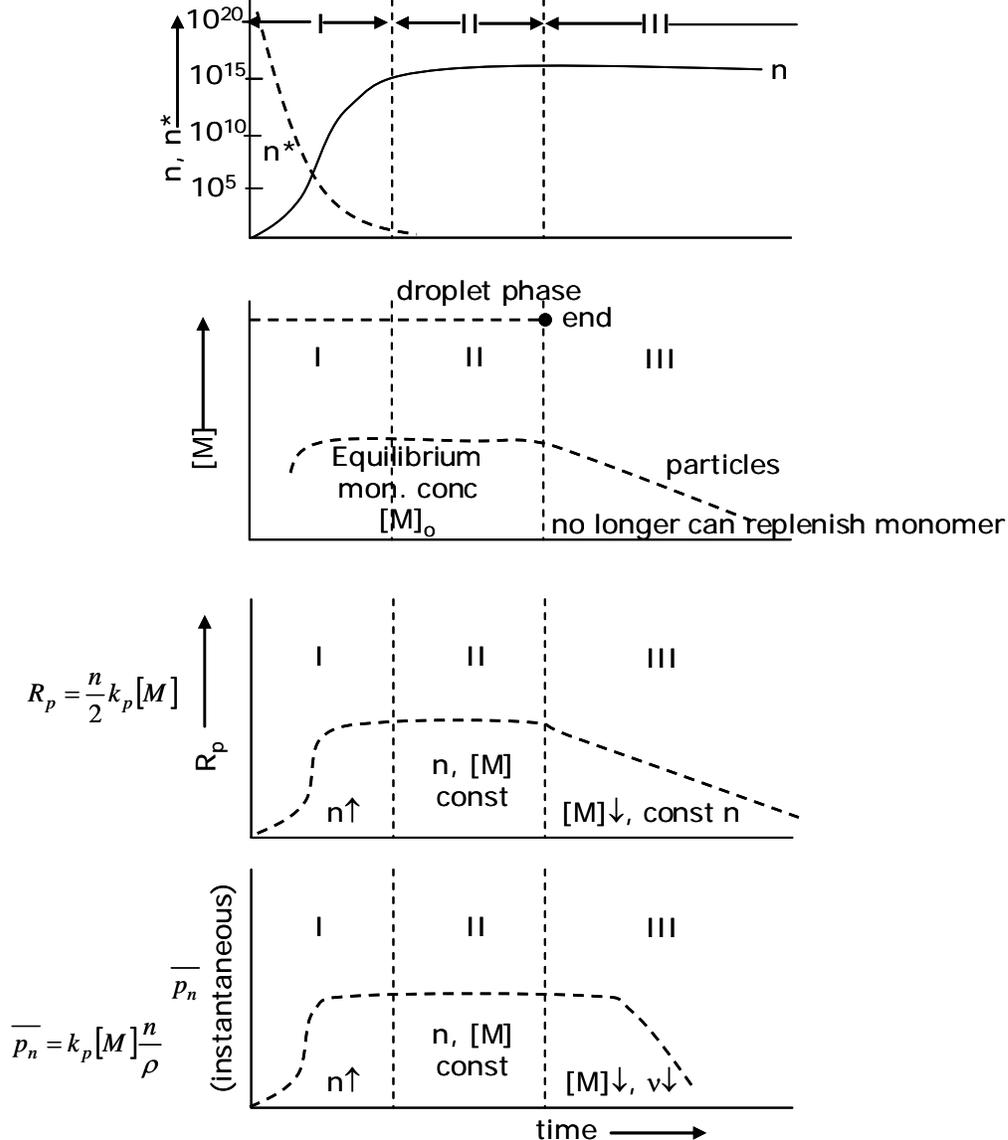


Fig 12.2. Diagrams showing the three stages of emulsion polymerization: (I) Micelles increasing; (II) micelles exhausted, droplet phase remains; (III) droplet phase exhausted.

n number of particles per unit volume

n^* number of micelles per unit volume

$[M]$ monomer concentration in the droplets and in the particles

R_p overall rate of polymerization

\bar{p}_n instantaneous degree of polymerization

¹ Rempp, P. and Edward W. Merrill. *Polymer Synthesis*. Second Edition. New York, NY: Hüthig and Wepf, 1991. page 250.

Rate of Conversion, Emulsion Polymerization

$$\bar{\rho}_n = k_p [M] \Delta t = k_p [M] \frac{n}{2}$$

rate of production of free radicals

In general:

$$R_p = \frac{n}{2} k_p [M] = \text{monomer molecules per sec per cm}^3$$

particles per cm³ I/mol-sec mol/l

* (recall that the rate, $-dm/dt$ of disappearance of monomer molecules **per particle** per second is $\frac{1}{2} k_p [M]$)

In general, for conversion:

$$\frac{d\pi}{dt} = \underbrace{\frac{n}{2} k_p [M]}_{\text{monomers/sec-cm}^3} \cdot \frac{1}{C} = n \cdot \frac{-dm}{dt} \frac{1}{m_o}$$

initial # of monomer molecules charged

$$C = \frac{\Theta N_A \rho_m}{M_u} = \text{initial \# of monomers in total volume}$$

How much you've added

where $\Theta = \text{cm}^3 \text{ monomer charged/cm}^3 \text{ of total volume} = \text{volume fraction}$

$\rho = \text{density of monomer (g/cm}^3)$

$N_A = \text{Avogadro's number} = 6.023 \times 10^{23} \text{ molecules/mole}$

$M_u = \text{MW of monomer (repeat) unit}$

For Stage I:

$$[M] \cong [M]_{eq} = [M]_o (1 - \Theta_2)$$

where $[M]_o = \text{pure monomer}$

$\Theta_2 = \text{vol. Fraction of polymer in particles at equilibrium}$

$n = n(t)$ b/c number of particles \uparrow

$$\Rightarrow \int_0^{\pi_f} d\pi = \frac{1}{C} \int_0^{\pi_f} n(t) \frac{k_p}{2} [M]_o (1 - \Theta_2) dt$$

For Stage II:

Surfactant consumed, droplets still exist
Growing particles

$$[M] = \text{constant} = [M]_b (1 - \Theta_2)$$

$$n = \text{constant}$$

$$\int_{\pi_I}^{\pi_{II}} d\pi = \frac{1}{C} \int_{t_I}^{t_{II}} \underbrace{\frac{n}{2} k_p [M]_b (1 - \Theta_2)}_{\text{constant}} dt$$

$$\Rightarrow \pi_{II} - \pi_I = \frac{nk_p [M]_b (1 - \Theta_2)}{2C} (t_{II} - t_I)$$

Stage III:

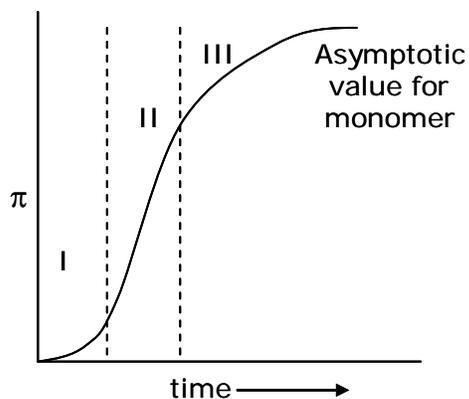
Droplets exhausted, only particles
On avg, particles all same size, grow at same rate

Here, monomer is consumed w/in particles, as monomer \rightarrow polymer,
[M] \downarrow w/in particle.

$$[M] = [M]_b (1 - \pi)$$

$$\Rightarrow \int_{\pi_I}^{\pi_{II}} d\pi = \frac{1}{C} \int_{t_I}^{t_{II}} k_p [M]_b (1 - \pi) \frac{n}{2} dt$$

$$\Rightarrow \frac{-\Delta \ln(1 - \pi)}{\Delta t} = \frac{k_p [M]_b n}{2C}$$



For Stage I:

$$n = f\left(C_s, a_s, \rho, v_n, \frac{dm}{dt}\right)$$

where C_s = surfactant concentration
 a_s = area of surfactant molecule (of polar head)
 ρ = rate of radical production
 v_n = vol of a single repeat
 dm/dt = rate of monomer polym.

Empirical expression:

$$n \approx 0.53 (C_s a_s)^{\frac{3}{5}} \rho^{\frac{2}{5}} \left(-v_n q \frac{dm}{dt}\right)$$

$$q = \frac{\text{vol polymer} + \text{vol monomer}}{\text{vol polymer}} \left. \vphantom{q} \right\} \text{inside the particle (related to [M])}$$