

- 2.3) A) N-S Equations      B) Physical parameters      C) Dynamic Similarity
- Lecture 5  
(units, scales)  
(Non-dimensional forms)
- Reading: Bat. 164 - 173      White: 81 - 94.  
Sch. 15 - 23      Kuethe & Chow: 461 - 462
- A) N-S Equations

Continuity:  $\frac{\partial p}{\partial t} + \rho \nabla \cdot \vec{u} = 0$

Momentum  $\rho \frac{D\vec{u}}{Dt} = \vec{p} - \nabla p + \frac{\partial}{\partial x_j} \left( \mu \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + \delta_{ij} \lambda \nabla \cdot \vec{u} \right)$

\* Energy.

$$\rho \frac{Dh}{Dt} = \frac{Dp}{Dt} + \nabla \cdot (k \nabla T) + \Phi$$

↑  
enthalpy    →  $h = e + p/\rho$

(White 69 - 72)  
↑ temperature    ↑ dissipation function

A1) Units and scales

A unit is a known reference quantity

Standard unit: m, kg, sec. (fixed scale)

Natural Unit: L,  $\rho_0 L^3$ ,  $L/V_0$  (adjustable scale)

Example: steady, incomp, inviscid flow



B) Non-Dimensionalization: changing from standard to natural units

For steady, incompressible, inviscid flow

length	$m$	$\xrightarrow{\text{std}}$	$L$
mass	$kg$	$\xrightarrow{\text{std}}$	$\rho_0 L^3$
time	$sec$	$\xrightarrow{\text{std}}$	$L/V_0$

If we analyse steady, compressible, viscous flow, then  
 $a_\infty$  (speed of sound) and dynamic viscosity  $\mu_0$  are  
 added so that

Length  $L$  or  $\frac{M_{\infty}}{\rho_0 U_{\infty}}$  and Time  $\frac{L}{U_{\infty}}$  or  $\frac{L}{\rho_0 U_{\infty}}$

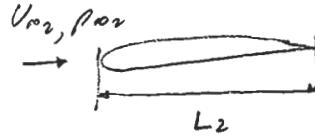
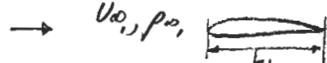
can be used. Then are redundant scales for length & time  
 The ratio of such alternate scales gives non-dimensional parameters

$$(\text{Length}) \frac{\frac{L}{M_\infty}}{\rho_0 U_\infty} = Re_L \quad \text{and (Time)} \quad \frac{t/M_\infty}{t/U_\infty} = Mach \#$$

↑  
Reynolds #

### C) Dynamic Stability

Suppose we have two airfoils  $\alpha$  &  $\beta$



geometric similarity

A & B are dynamically similar if they are identical in natural units.  $\Rightarrow$  significant non-dimensional parameters are the same ( $Re$ ,  $M_\infty$ , etc.)

(3)

Non-Dimensionalization of N-S equations

Reference Quantities:  $L_{ref}$ ,  $V_{ref}$ ,  $\rho_{ref}$ ,  $M_{ref}$

$$x_i^* = \frac{x_i}{L_{ref}}, \quad t^* = \frac{t}{L_{ref}/V_{ref}}, \quad u_i^* = \frac{u_i}{V_{ref}}, \quad \rho^* = \rho/\rho_{ref}$$

$$\mu^* = \mu/M_{ref}$$

Convective derivative  $\frac{D}{Dt} = \frac{\partial}{\partial t} + (\vec{u} \cdot \vec{\nabla})$

$$\begin{aligned} \Rightarrow \frac{D}{Dt} &= \frac{V_{ref}}{L_{ref}} \frac{\partial}{\partial t^*} + \frac{V_{ref}}{L_{ref}} \cdot u_i^* \frac{\partial}{\partial x_i^*} \\ &= \frac{V_{ref}}{L_{ref}} \left( \frac{\partial}{\partial t^*} + u_i^* \frac{\partial}{\partial x_i^*} \right) = \frac{V_{ref}}{L_{ref}} \frac{D}{DE^*} \end{aligned}$$

▷ Conservation of Mass:

$$\frac{D\rho}{Dt} + \rho \frac{\partial u_i}{\partial x_i} = 0$$

$$\Rightarrow \rho_{ref} \cdot \frac{V_{ref}}{L_{ref}} \cdot \frac{D\rho^*}{DE^*} + \rho_{ref} \frac{V_{ref}}{L_{ref}} \cdot \rho^* \frac{\partial u_i^*}{\partial x_i^*} = 0$$

$$\Rightarrow \frac{D\rho^*}{DE^*} + \rho^* \frac{\partial u_i^*}{\partial x_i^*} = 0$$

For 2D steady incompressible flow

$$\frac{\partial u_1^*}{\partial x_1^*} + \frac{\partial u_2^*}{\partial x_2^*} = 0 \quad \left( = \frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right)$$

## 2) Conservation of Momentum

$$\rho \frac{D\vec{u}}{Dt} = \rho \vec{f} + \vec{\nabla} \cdot \vec{\sigma} = \rho \vec{f} - \nabla p + \nabla \cdot \vec{\epsilon}$$

Assume  $\vec{f} = 0$ , incompressible flow  $\nabla \cdot \vec{\epsilon} = \mu \nabla^2 \vec{u}$   
 $\mu = \text{constant}$

$$\rho \frac{Du_i}{Dt} = \mu \frac{\partial^2 u_i}{\partial x_i \partial x_j} - \frac{\partial p}{\partial x_i}$$

$$P_{ref} = \rho_{ref} V_{ref}^2$$

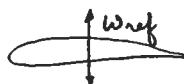
$$P^* = P/P_{ref}$$

$$\Rightarrow \rho_{ref} \cdot \frac{V_{ref}^2}{L_{ref}} \cdot P^* \frac{D u_i^*}{D t^*} = \rho_{ref} \frac{V_{ref}}{L_{ref}} \mu^* \frac{\partial^2 u_i^*}{\partial x_i^* \partial x_j^*} - \frac{\rho_{ref} V_{ref}^2}{L_{ref}} \frac{\partial P^*}{\partial x_i^*}$$

$$P^* \frac{D u_i^*}{D t^*} = \left( \frac{1}{Re_{ref}} \right) \mu^* \frac{\partial^2 u_i^*}{\partial x_i^* \partial x_j^*} - \frac{\partial P^*}{\partial x_i^*}$$

$$\frac{D u_i^*}{D t^*} = \frac{1}{Re} \frac{\partial^2 u_i^*}{\partial x_i^* \partial x_j^*} - \frac{\partial P^*}{\partial x_i^*}$$

- unsteady, compressible viscous flow



$w_{ref}$ ,  $V_{ref}$ ,  $\rho_{ref}$ ,  $\mu_{ref}$ ,  $Re_{ref}$

$$t_{ref} = \frac{L_{ref}}{V_{ref}} \quad \text{or} \quad \frac{1}{w_{ref}}$$

$$\Rightarrow \frac{w_{ref} V_{ref}}{L_{ref}} = St_{ref} \quad \text{or} \quad k_{ref}$$

$\uparrow$    
 structural  $\uparrow$  reduced frequency.

- steady compressible viscous flow

$U_{ref}$ ,  $\dots$ ,  $a_{ref}$ ,  $K_{ref}$   
 $\rho$   
speed of sound      ↑ thermal conductivity

$$M_{ref} = \frac{U_{ref}}{a_{ref}}, \quad P_{ref} = \frac{C_p M_{ref}}{K_{ref}}$$

↑ temperature variation / ht transfer

For ~~steady~~, incompressible, viscous flow

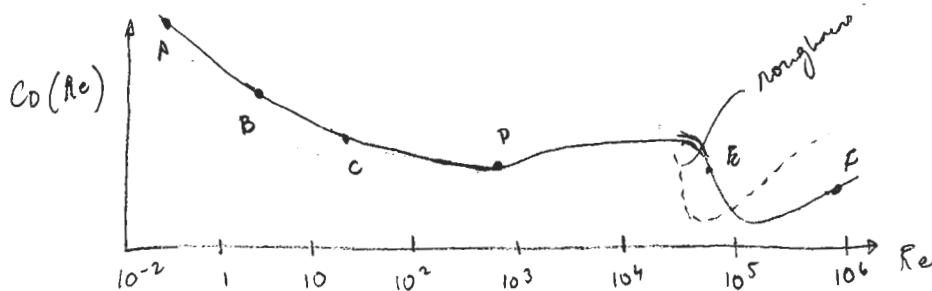
$$\nabla \cdot \vec{u} = 0$$

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\frac{1}{\rho} \nabla p + \frac{1}{Re} \nabla^2 \vec{u} \quad * \text{dropped}$$

B.C depend on geometry, i.e.  $u/L \sim Re^{-\dots}$

Flow regimes as a function of Reynolds #

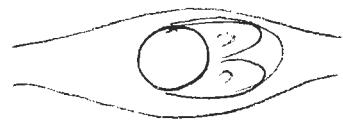
Consider a spherical body



A)  $Re \ll 1$  Stokes flow (3, 4)

B)  $Re < 1$  Oseen flow (3, 4, 2-linearized)

c)  $Re \approx 1 - 100$  - steady, separated flow (2, 3, 4)



c)  $Re \approx 100 - 1000$  - unsteady sep. flow (1, 2, 3, 4) (NS)  
↑ vortex shedding



d)  $Re \approx 200 - 400 \times 10^3$  transition moves onto surface



e)  $Re \approx 500 \times 10^3$  turbulent flow (2, 3, simplified 4)  
↑ TSL

